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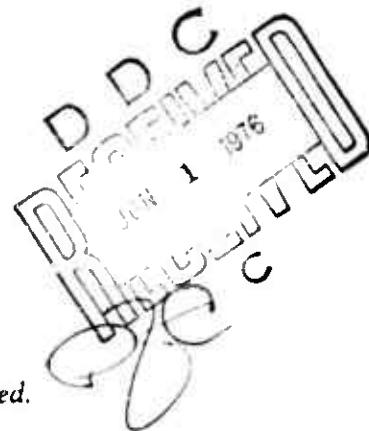
Technical Report RD-76-22

INVESTIGATION OF JET PLUME EFFECTS  
ON THE LONGITUDINAL STABILITY CHARACTERISTICS  
OF A BODY OF REVOLUTION WITH VARIOUS FIN CONFIGURATIONS  
AT MACH NUMBERS FROM 0.2 TO 2.3 (NORMAL JET PLUME SIMULATOR)

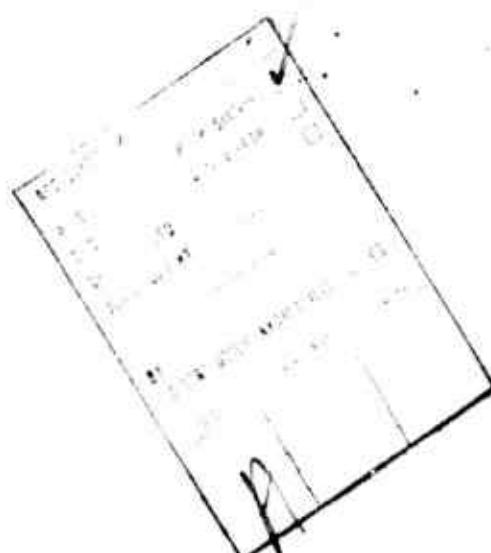
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US Army Missile Research, Development and Engineering Laboratory  
US Army Missile Command  
Redstone Arsenal, Alabama 35809

20 February 1976

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*Redstone Arsenal, Alabama*



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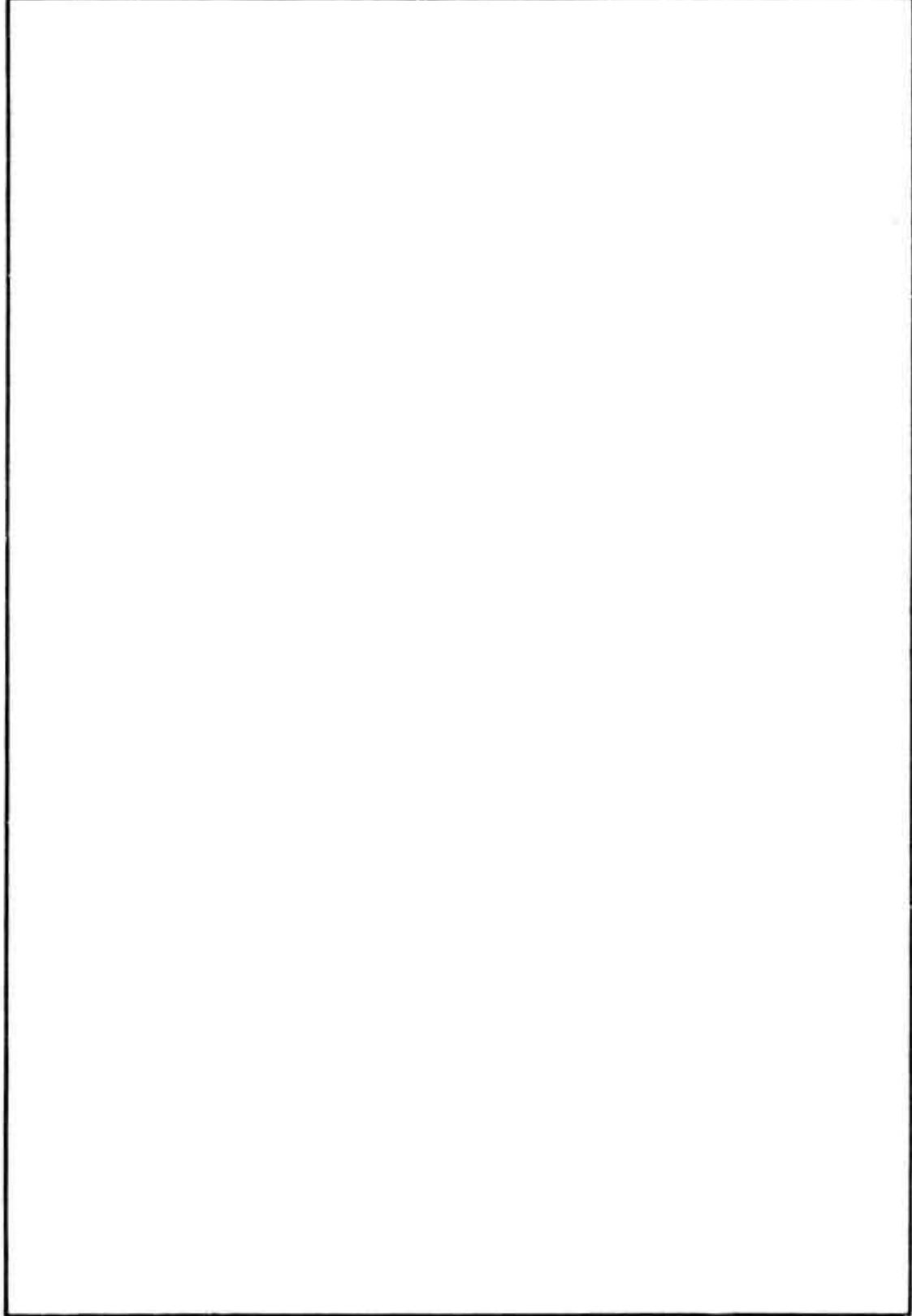
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Transonic wind tunnel tests were conducted on a body of revolution with various fin configurations to investigate jet plume effects on missile longitudinal stability. A series of cold air normal jets located downstream of the base were utilized to simulate the jet plume. Fins of various planform geometry were tested at a forward longitudinal location only. The angle of attack range was -4 to 11 degrees at Mach numbers of from 0.2 to 2.3. The test was run at the Arnold Engineering Development Center Transonic (16T) and Supersonic (16S) wind tunnels and was designated AEDC SF172/TF360.		

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## INTRODUCTION

During the past few years the Army Missile Command has been interested in the adverse effects of the propulsive jet plume on missile aerodynamics. Of particular importance are the effects on missile longitudinal stability. A research program has been established as a means of obtaining the understanding necessary for proper design of future missiles susceptible to this problem (see Reference 1).

It was previously shown that plume induced instability could be avoided by moving the fins forward from the base and using fins of sufficient size. Results also indicated that stability margin might be controlled to a precision where plume effects could be used to advantage as a means of reducing missile wind sensitivity. Later test results appear to substantiate this judgement. Fins can be located in a position to retain most of their effectiveness, while the plume still has a significant destabilizing influence on the missile body. Thus, based on available data, the desired unstable transonic-stable supersonic stability characteristics can be attained.

Previous tests at the CALSPAN transonic tunnel were made at Mach numbers up to 1.25. The present test extended the results up to a Mach number of 2.3. Also, tests were made at Mach numbers of 0.2 and 0.4 and at angles of attack up to 11 degrees to determine launch crosswind effects.

## APPARATUS AND TESTS

The model is a sting mounted body of revolution, 5 inches in diameter and 5½-inches long with a 30 caliber tangent ogive nose. The model was tested in combination with two different sets of cruciform rectangular fins set at zero degrees roll. For the present test the fins were tested in the forward location only (Fin trailing edge 1.5 calibers ahead of the model base). The fin geometry is shown in figure 4.

The geometry of the fins tested is as follows:

<u>Fin</u>	<u>Chord (in)</u>	<u>Semi span (in)</u>
F1	5.0	2.5
F2	3.0	2.5

The plume simulator consisted of 24 sonic jets normal to the sting centerline and arranged circumferentially in two rows with a common air chamber (see figure 3). The simulator was located 0.5 caliber aft of the model base. The combined exit area of the 24 jets represented 6 per cent of the model base (reference) area. The level of plume simulation was established by setting various pressures in the simulator chamber.

Tunnels 16T and 16S are closed-circuit, continuous-flow tunnels that can be currently operated at Mach numbers from 0.20 to 1.6 and 1.5 to 2.4, respectively. The test sections are 16 by 16 ft in cross-section and 40 ft long. Details of each tunnel's capabilities and supporting equipment can be found in reference 5. Photographs of the model installed in the test sections are shown in figures 6 and 7 and sketches of the location of the models in the tunnels are shown in figure 5.

Total model force and moments were measured using a 2.0-inch, 6-component balance, with normal and side force capacities of 1800 pounds and 900 pounds, respectively. The balance was mounted in the model, such that the balance 900-pound capacity side-force gages measured model normal forces, in order to achieve better data resolution in the model pitch plane. Fin forces and moments were measured using 5-component (no axial force) balances, with a nominal normal force capacity of 60 pounds.

A static pressure measurement was made in the balance cavity and was used to calculate the balance cavity axial force. Two static pressure measurements were made at the base of the model and were used to calculate base pressure.

Model angle of attack was measured using a pendulum-type angle sensor, with a backup measurement determined from balance-sting deflections.

Steady-state data were obtained at free-stream Mach numbers from 0.2 to 2.3. The tunnel test conditions were held constant at each Mach number. Plume effects were obtained by setting and maintaining a specific value of chamber pressure while angle of attack was varied.

Model aerodynamic coefficients were tabulated in the body-axes system and referenced to model station 26.5 inches. No correction was made to the data for tunnel flow angularity. Fin moment coefficients were referenced to the fin hinge-line and fin root bending moment coefficients were referenced to the fin-body intersection. The positive orientation of the model and fin forces and moments are shown in figure 2.

## TEST CONDITIONS

The test was conducted in the AEDC Propulsion Wind Tunnels, Supersonic (16S) and Transonic (16T), respectively. Tunnels 16T and 16S are closed-circuit, continuous-flow tunnels that can be currently operated at Mach numbers from 0.20 to 1.6 and 1.5 to 2.4, respectively. The purpose of the test was to determine the Mach number range of adverse jet plume effects on missile longitudinal stability. Similar data were previously obtained at the Calspan Corporation 8-Foot Transonic Wind Tunnel. Three configurations were tested (body with Fins F1, body with Fins F2, and body alone) at various simulated plume shapes, at model angles of attack from -4 to 11 degrees at zero degrees yaw, zero degrees roll, and at free-stream Mach numbers from 0.2 to 2.3. Steady-state data were obtained at these free-stream Mach numbers. The tunnel test conditions were held constant at each Mach number, and the plume shape was generated by setting a specific value of high-pressure air in the plume simulator chamber and discharging the air radially. The Radial Thrust Coefficient (CRT) is a measure of the plume shape and is a function of the free-stream Mach number and the simulator pressure. At specified levels of CRT and Mach number, the model angle of attack was varied from -4 to 11 degrees at the free-stream Mach numbers of 0.2 and 0.4. At all other Mach numbers, the angle-of-attack range was -4 to 4 degrees.

## PLUME SIMULATION

In the past, the Army Missile Command has used base pressure ratio  $p_b/p_\infty$  as an indication of the onset and the severity of plume effects on missile aerodynamics (see reference 1). One of the parameters that can be conveniently used to correlate base pressure is thrust coefficient CT, where CT is axial thrust non-dimensionalized by dynamic pressure and body cross-sectional area, ( $S_{ref}$ ). For the normal jet simulator a similar parameter is radial thrust coefficient, CRT, where

$$CRT = \frac{\text{Radial Thrust}}{qA}$$

Radial thrust is the summation of the thrust of the 24 individual nozzles. For an axial jet, base pressure appears to be primarily influenced by the portion of the jet plume in the vicinity of the jet boundary where it interacts with the freestream flow. Where CT can be considered to represent the axial component of the effective jet, it can be assumed that CRT represents the normal component.

For the plume size of interest in the present investigation a value of CT several times the value of CRT is required for matching base pressures. The exact CT/CRT ratio will depend on a comparison of flight base pressures with base pressure values for the normal jet simulator. Where flight base pressures are unavailable, methods exist which allow simulation of flight rockets with cold air axial jets (see, for example reference 6). An estimate of the CT/CRT ratio (although crude) is valuable for use in preliminary design and insuring that the range of CRT values planned for wind tunnel tests are sufficient.

## RESULTS

Data presented in the plots show radial thrust effects on stability characteristics, fin normal force, fin hinge moment, and fin root bending moment. Radial thrust effect on longitudinal derivatives and hysteresis effects are also plotted.

The transonic portion of the test was run 24-25 January 1975 and was designated TF360. Several runs were made to determine plume effects at high angles of attack and at low Mach numbers. These conditions approximate exit from the launcher for a free rocket configuration. Typical results at these conditions are shown for the body alone (B) configuration on page 2 of the data figures. Significant plume effects are apparent when the thrust level is increased to a CRT value of 12. With a further increase of CRT to 37.5, plume effects are more severe--but only at angles of attack between  $\pm 1.5$  degrees. At higher angles of attack stability characteristics tend to approach the jet-off case. These results suggest that the plume effects at a CRT of 37.5 reach forward to the ogive portion of the body or possibly the nose tip. In this case, the short body tested does not represent the plume effects on a much longer body such as that being considered for the free rocket technology program configuration. Therefore, it is recommended that plume effects on long bodies be investigated for several typical conditions.

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5. Test Facilities Handbook (Tenth Edition). "Propulsion Wind Tunnel Facility, Vol. 4." Arnold Engineering Development Center, May 1974.
6. Korst, H. H., Approximate Determination of Jet Contours Near the Exit of Axially Symmetrical Nozzles as a Basis for Plume Modeling, Technical Report No. RD-72-14, August 1973, U. S. Army Missile Command, Redstone Arsenal, Alabama.

## NOMENCLATURE

<u>SYMBOL</u>	<u>PLOT SYMBOL</u>	<u>DEFINITION</u>
RN/L	RN/L	unit Reynolds number; per ft
V		velocity; ft/sec
$\alpha$	ALPHA	angle of attack, degrees
$\beta$	BETA	angle of sideslip, degrees
$\psi$	PSI	angle of yaw, degrees
$\phi$	PHI	angle of roll, degrees
$\rho$		mass density; slugs/ft <sup>3</sup>
$C_T$	CT	thrust coefficient, axial thrust/qS
$C_T$	CRT	radial thrust coefficient, radial thrust/qS
$P_{bAVG}/P_\infty$	PB/P1	ratio of average base pressure to tunnel freestream static pressure
F.P.	FINPOS	fin position on body:  1. AFT; Fin Hinge line at M.S. 49.750 2. MID; Fin Hinge line at M.S. 46.000 3. FWD; Fin Hinge line at M.S. 42.250
a		speed of sound; ft/sec
$C_p$	CP	pressure coefficient; $(p_1 - p_\infty)/q$
M	MACH	Mach number; V/a
p		pressure; psf
q	Q(NSM) Q(PSF)	dynamic pressure; $1/2\rho V^2$ , psf
$p_b/p_\infty$		base pressure ratio

## NOMENCLATURE (Continued)

### Reference & C.G. Definitions

$A_b$		base area; $\text{m}^2$ , $\text{in}^2$
$b$	BREF	wing span or reference span; m, in
c.g.		center of gravity
$l_{\text{REF}}$ , $\bar{c}$	LREF	reference length or wing mean aerodynamic chord; m, in
$S$ , $S_{\text{ref}}$	SREF	reference area based on body diameter, $\text{in}^2$
	MRP	moment reference point
	XMRP	moment reference point on X axis
	YMRP	moment reference point on Y axis
	ZMRP	moment reference point on Z axis
		<u>Fin Balances</u>
$C_{NFX}$	CNX	fin normal force coefficient, <u>fin normal force</u> $qS_{\text{ref}}$
$C_{mH_X}$	CLMHX	fin hinge moment coefficient, <u>fin hinge moment</u> $qS_{\text{ref}}l_{\text{ref}}$
$C_{mR_X}$	CLMRX	fin root bending moment coefficient, <u>fin root bending moment</u> $qS_{\text{ref}}l_{\text{ref}}$
$x_{CPF_X}$	XCPFX	chordwise center of pressure location relative to fin hinge line, positive toward the leading edge, inches
$C_{NFX_a}$	CNXALFA	fin normal force coefficient derivative with angle, per degree

## NOMENCLATURE (Concluded)

### Body-Axis System (Main Balance)

$C_N$	$C_N$	normal-force coefficient; $\frac{\text{normal force}}{qS}$
$C_A$	$C_A$	axial-force coefficient; $\frac{\text{axial force}}{qS}$
$C_Y$	$C_Y$	side-force coefficient; $\frac{\text{side force}}{qS}$
$C_m$	$CLM$	pitching-moment coefficient; $\frac{\text{pitching moment}}{qS \ell_{REF}}$
$C_n$	$CYN$	yawing-moment coefficient; $\frac{\text{yawing moment}}{qS_b}$
$C_\ell$	$CBL$	rolling-moment coefficient; $\frac{\text{rolling moment}}{qS_b}$
$C_{m\alpha}$	$CLMALF$	pitching moment coefficient derivative with alpha, per degree
$C_{N\alpha}$	$CNALFA$	normal force coefficient derivative with respect to angle of attack, per degree

### SUBSCRIPTS

$b$	base
$l$	local
$s$	static conditions
$t$	total conditions
$\infty$	free stream

TEST : AEDC SF172/TF360  
TABLE 1.  
DATA SET/RUN NUMBER COLLATION SUMMARY

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DATE : 01-20-76

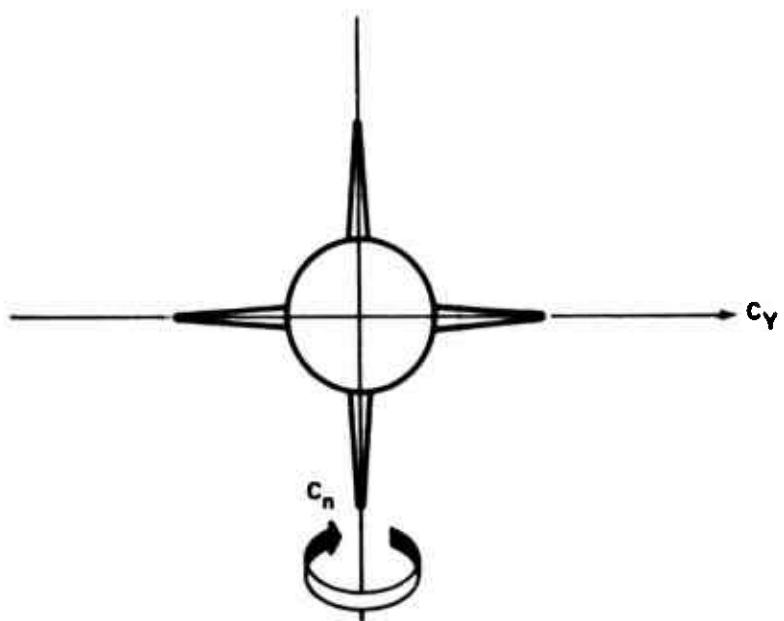
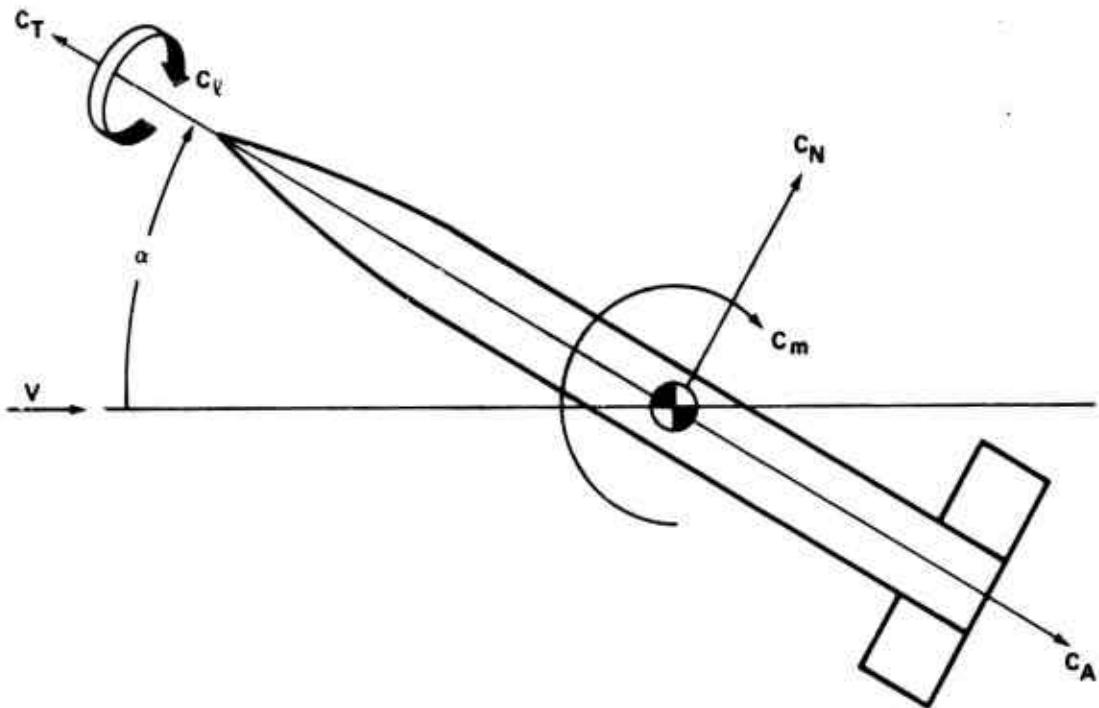
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TABLE 1. (Continued)  
DATA SET/RUN NUMBER COLLATION SUMMARY

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			$\alpha$	$\beta$	$\phi$	F.P.	MACH	0.01	1	2	3	4	6	6.5	12	25	37.5	50
RXE A*02	B	A 0 0 - 0.2	128															
03		A T T T 0.4	134															
04		B T T T 1.0	137															
05		T T T 1.25	139															
06		T T 1.5	144															
07		T 1.7	45*															
08		2.0	56*															
09	BF1	A 3 0.2	103															
11		A T 0.4	109															
12		B T 1.0	112															
13		T 1.25	114															
14		T 1.50	119															
15		T 1.7	18*															
16		2.0	30*															
17		A 2.3	36*															
18	BF2	A 0.2	172															
19	BF2	B 0.4	168															
$\Delta=0$ DATA, CN		C LM	C Y	C YN	C BL	C A	PB/P I		CRT		ALPHA	7						
$\Delta=1$ DATA, CNF1		C NF2	C NF3	C NF4	X C P F1	X C P F2	X C P F3	X C P F4		C RT	ALPHA	8						
$\Delta=2$ DATA, CLMH1		CL MH2	CL MH3	CL MH4	CL MR1	CL MR2	CL MR3	CL MR4		C RT	ALPHA	8						
TYPE OF DATA $\alpha$ OR $\beta$ SCHEDULES		$\alpha$ (A) = -4,-3,-2,-1.5,-1,-0.5,0,0.5,1,1.5,2,3,4,5,7,9,11								IO VAR (1)	IO VAR (2)	NOV						
$\alpha$ (B) = -4,-3,-2,-1.5,-1,-0.5,0,0.5,1,1.5,2,3,4																	*SF172	

TABLE 1. (Concluded)

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DATE : 01-20-76



(VIEW LOOKING FORWARD)

Figure 1 - Axis System Sign Convention for Main Balance

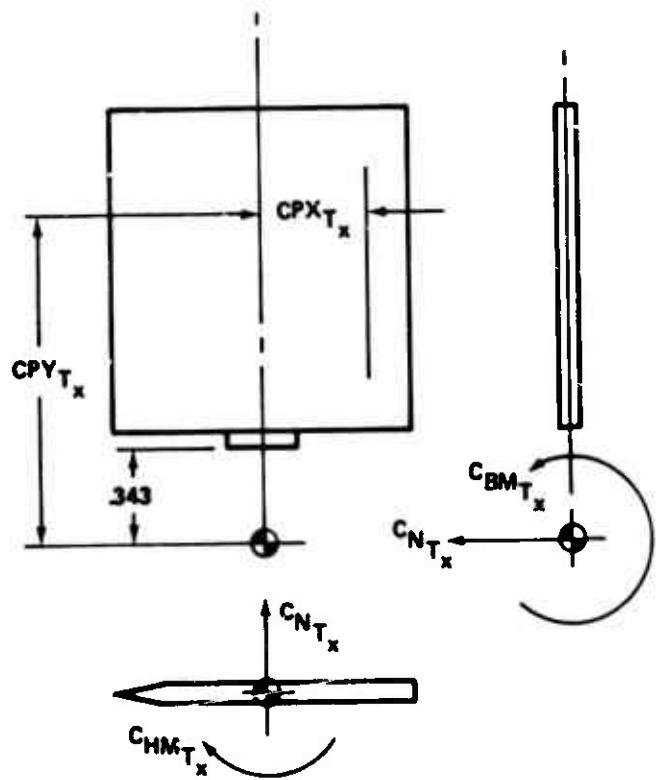
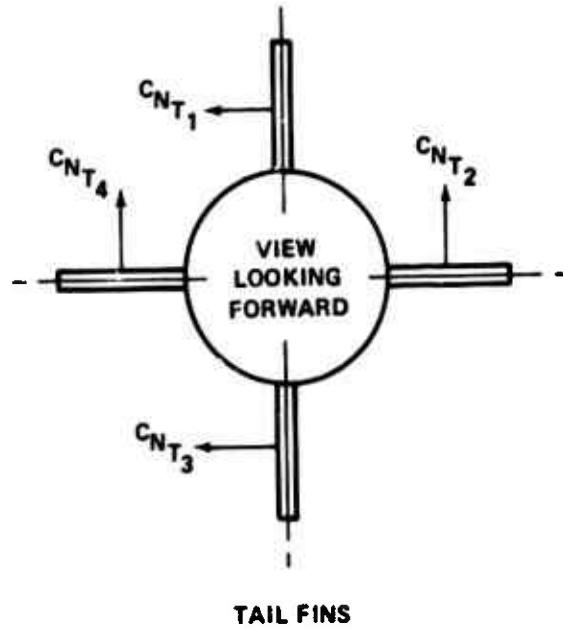


Figure 2 - Axis System and Positive Sign Convention for Fins

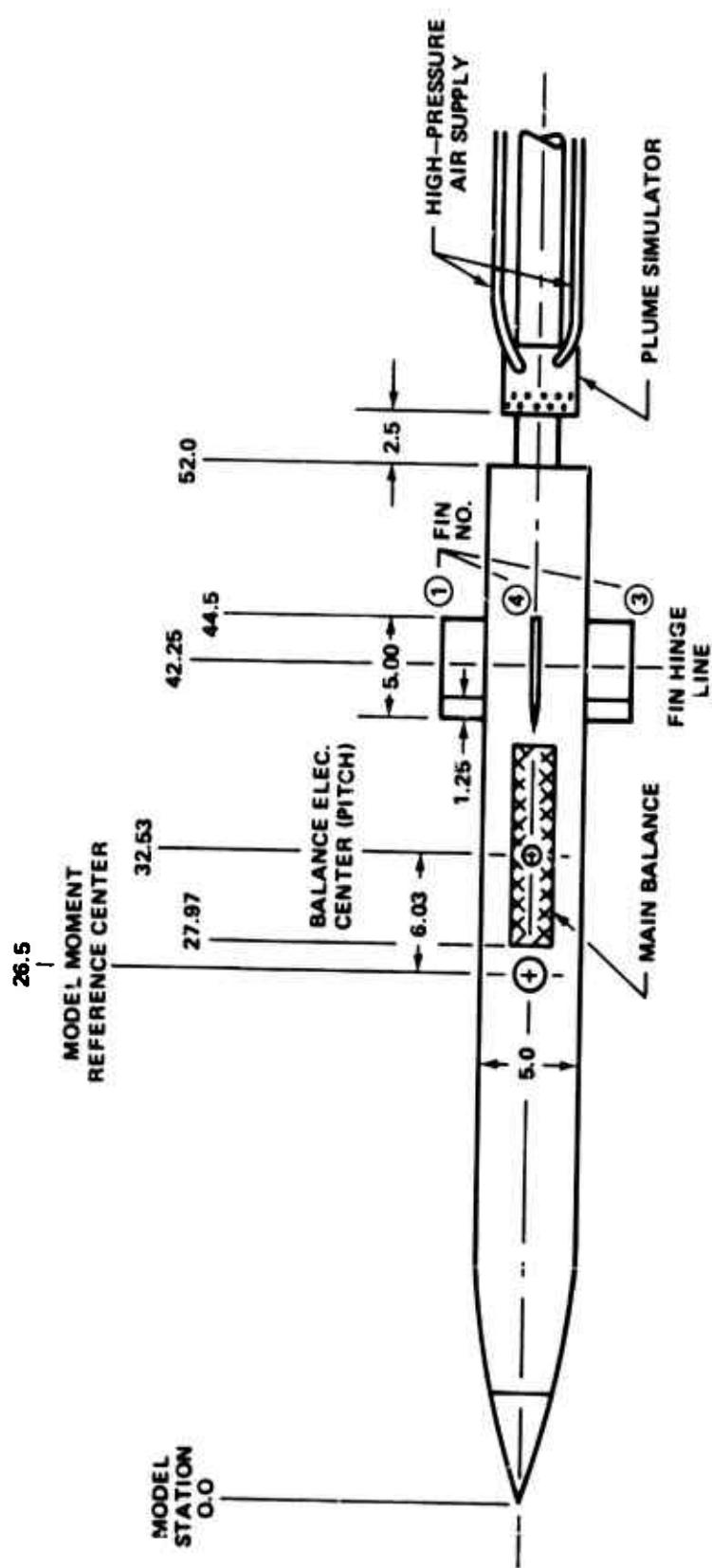


Figure 3 - AMC Model Drawing

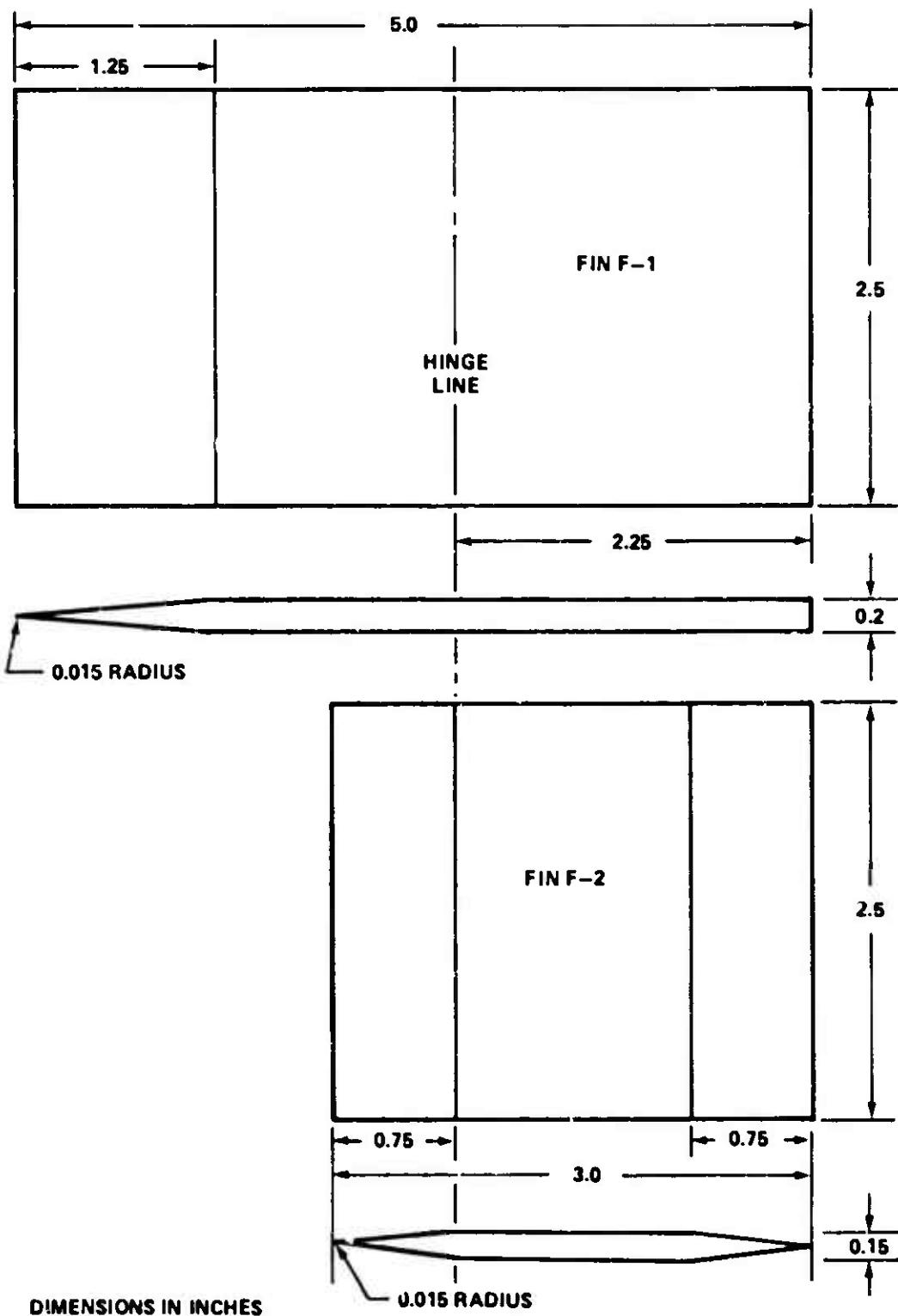
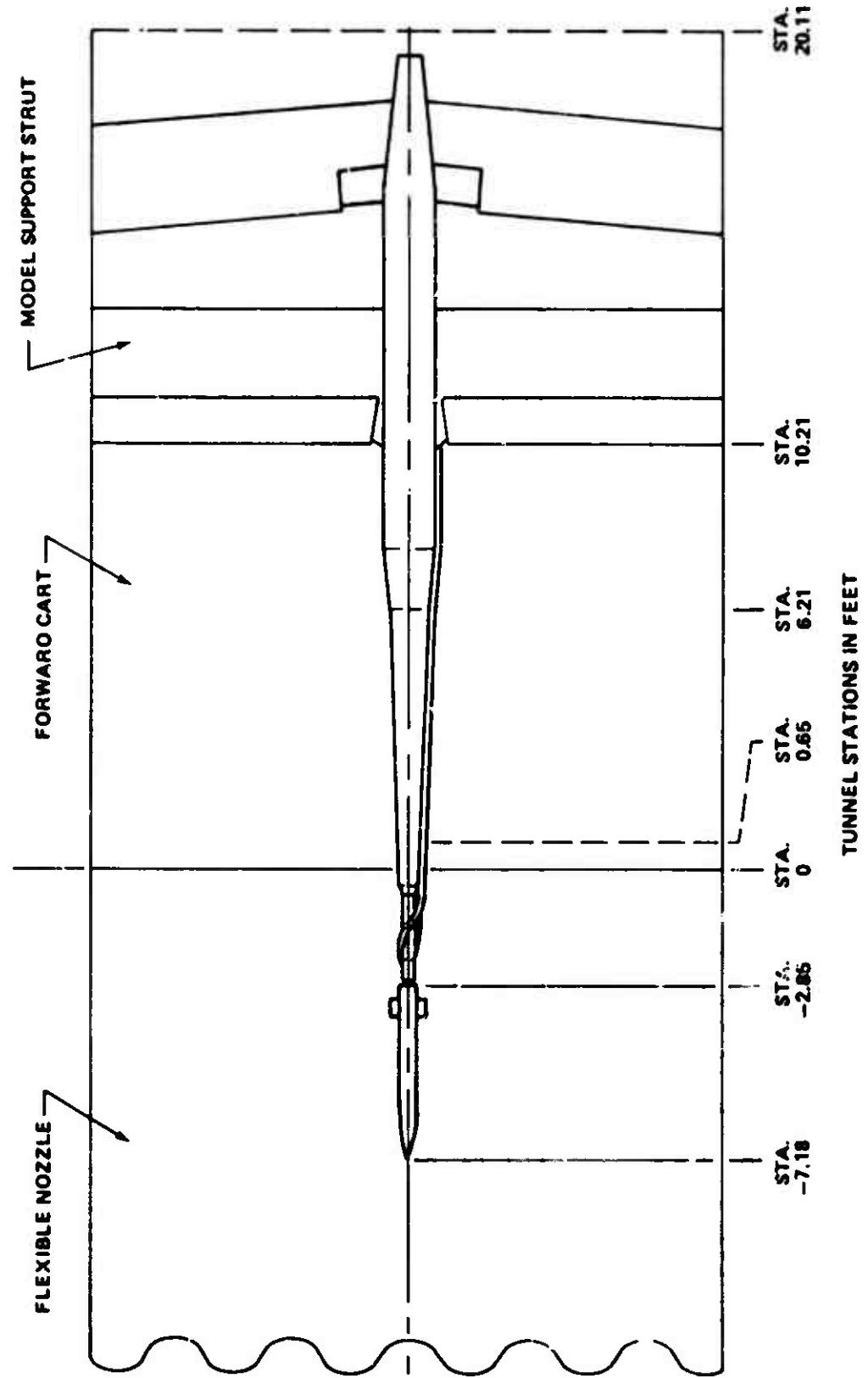
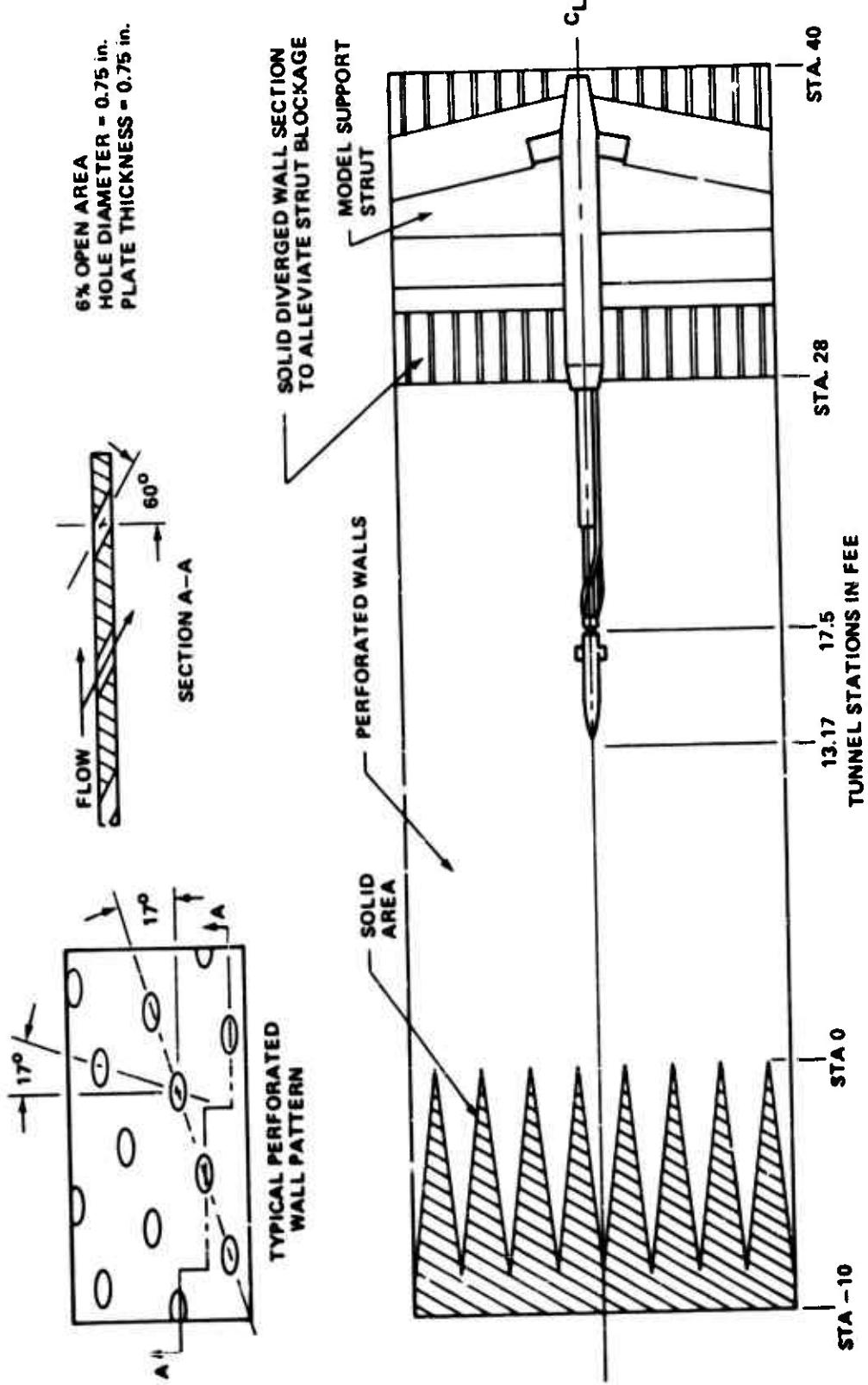


Figure 4 - Sketch of Fins F1 and F4



a. Tunnel 165  
Figure 5 - Sketch of Model Installation



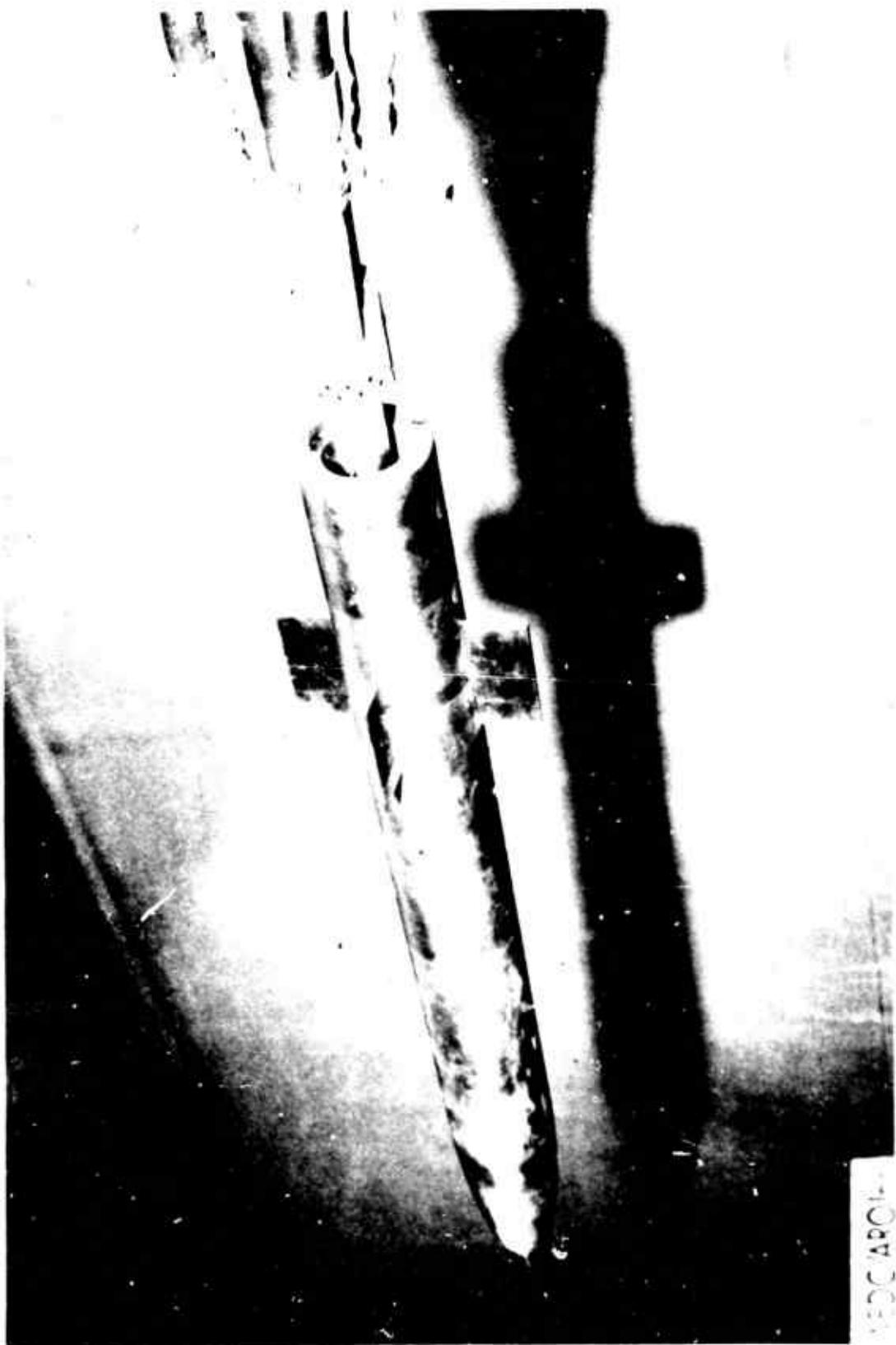
b. Tunnel 16T  
Figure 5. Concluded

Figure 6 - Photograph of Model (BF2) in PWT (16T)



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Figure 7. - Photograph of Model (BF1) in PWT (16S)



## PLOTTED DATA

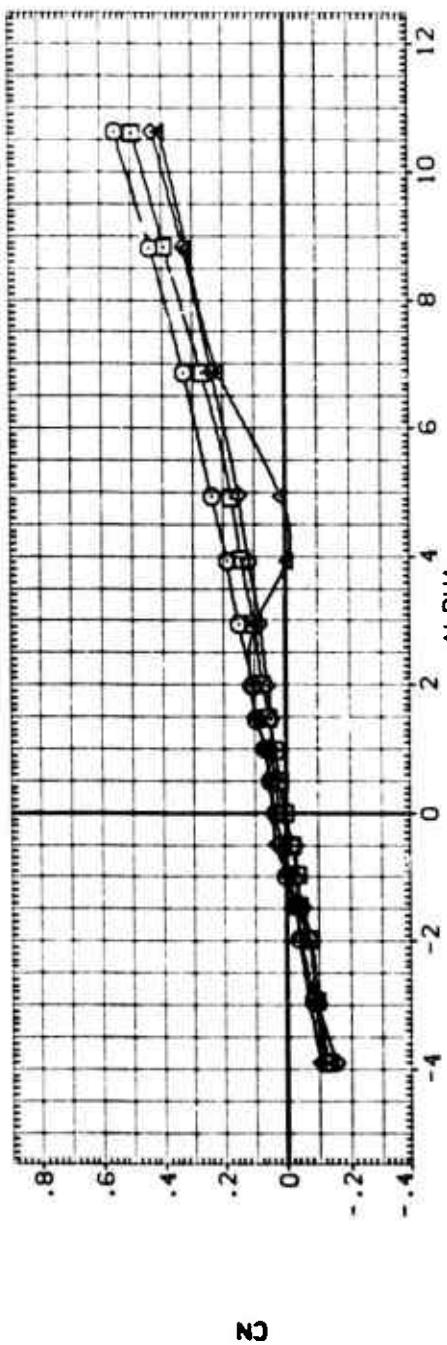
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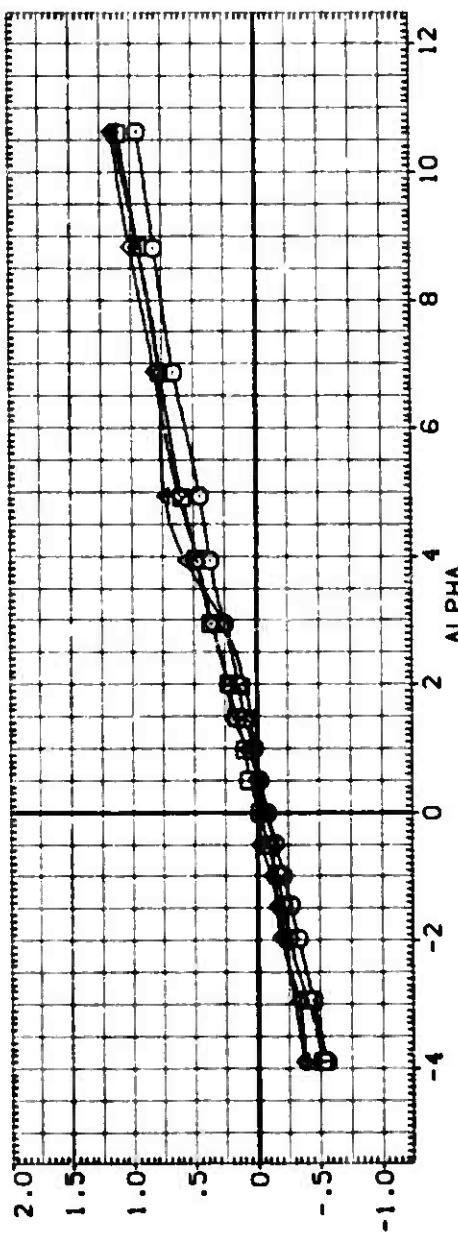
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 25.602 MACH .200  
 50.611  
 101.026

(RXE002)

REFERENCE INFORMATION  
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 THP .0000 IN.  
 ZHP .0000 IN.  
 SCALE .0000



Cn



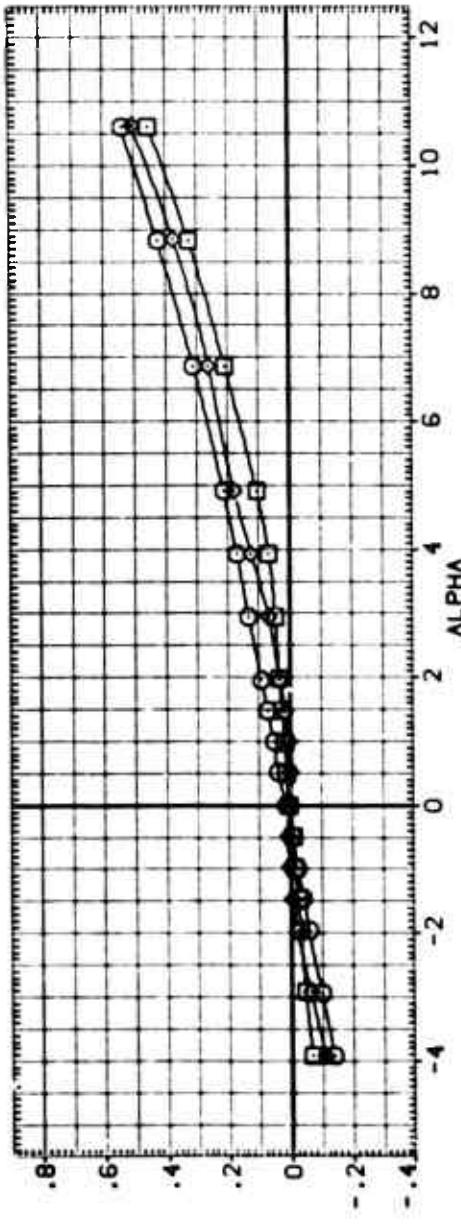
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### THRUST EFFECTS ON STABILITY CHARACTERISTICS

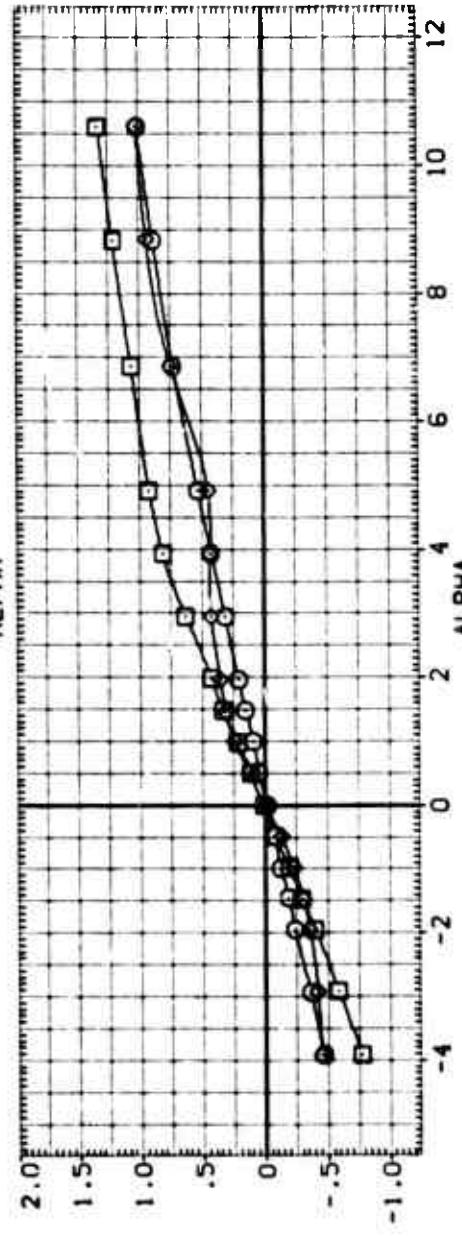
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 CRIT = 12.013, CLM = 37.191

(RXED03)

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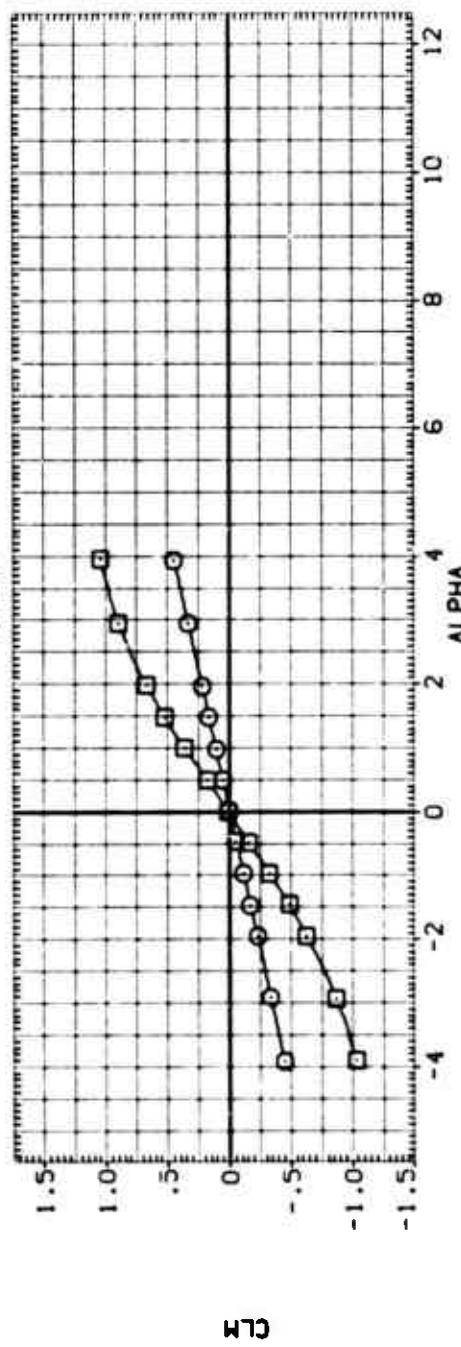
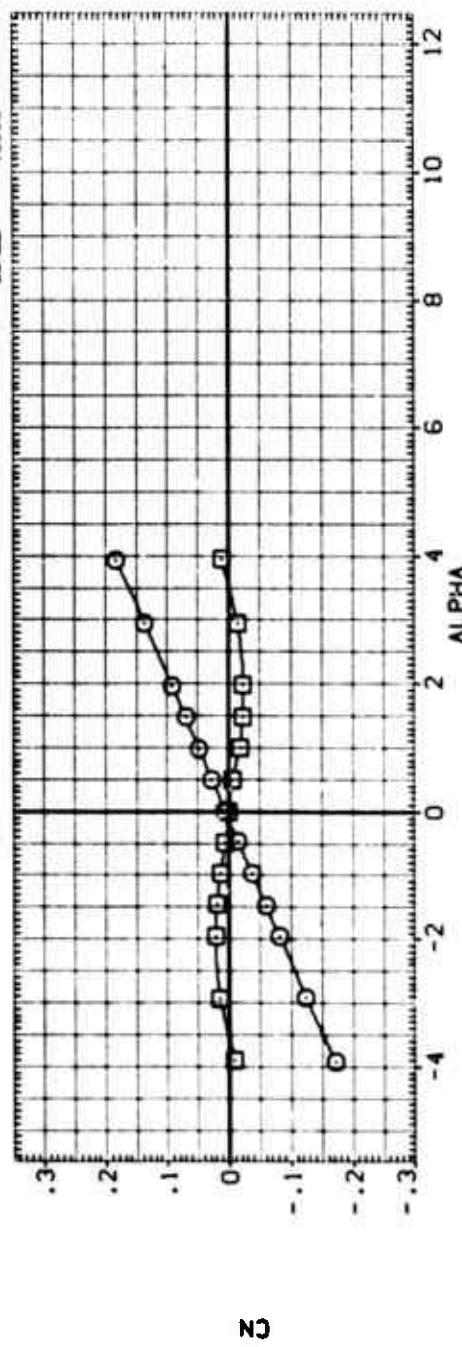
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### THRUST EFFECTS ON STABILITY CHARACTERISTICS

PAGE 2

AEDC TF360 BODY ALONE, B  
 PARAMETRIC VALUES  
 CRIT Q21 MTA MACH .000 PMI 1.000

REFERENCE INFORMATION  
 SPEED 19,6350 SD. IN.  
 LREF 5.0000  
 BREF 5.0000  
 AREF 26.5000  
 TREF .0000  
 ZHDP .0000  
 SCALE .0000



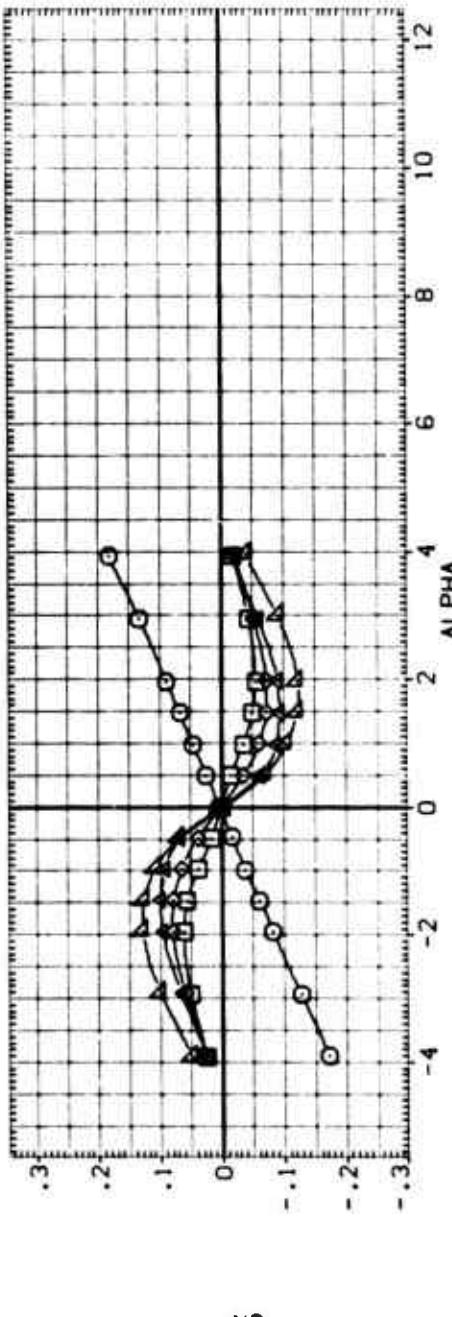
### THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY ALONE, B  
 PARAMETRIC VALUES  
 CRIT .010 BETA .000 PHI .000  
 1.015 MACH 1.250  
 4.013  
 5.976  
 11.995

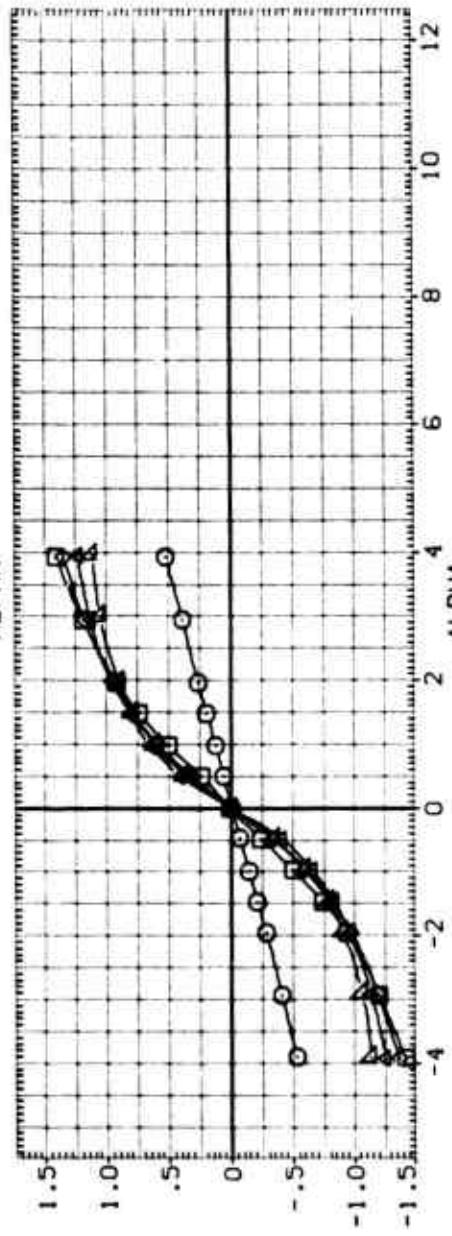
SYM  
 O □ ◇ △

(RXE005)

REFERENCE INFORMATION  
 SREF 19.6750 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 ARGP 26.5000 IN.  
 THRP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



CN



CLM

#### THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY ALONE, B

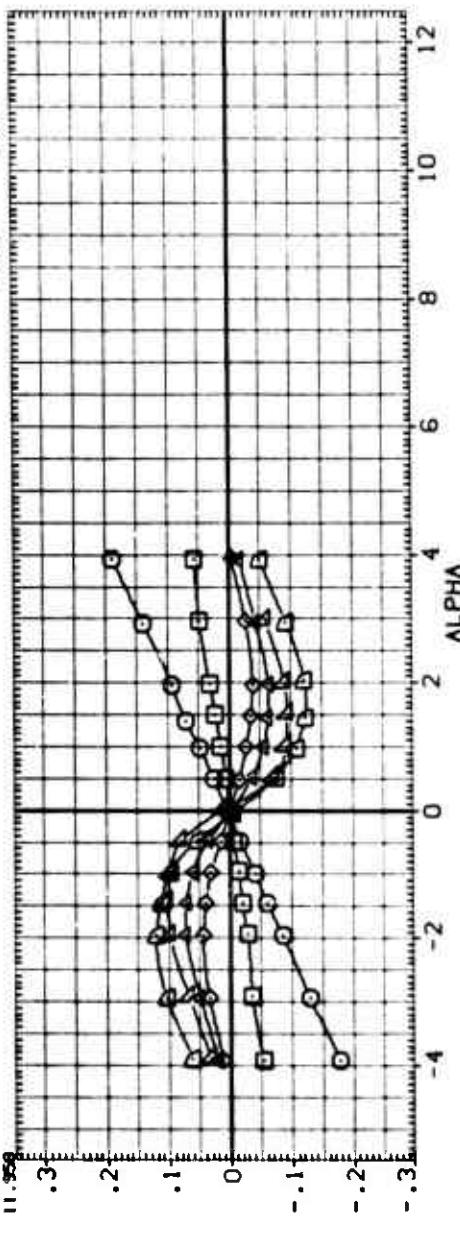
PARAMETRIC VALUES  
.000 PHI  
1.500 MACH

REFERENCE INFORMATION  
SREF 19.6250 SQ. IN.  
LREF 5.0000 IN.  
XREF 5.0000 IN.  
YREF .0000 IN.  
ZREF .0000 IN.

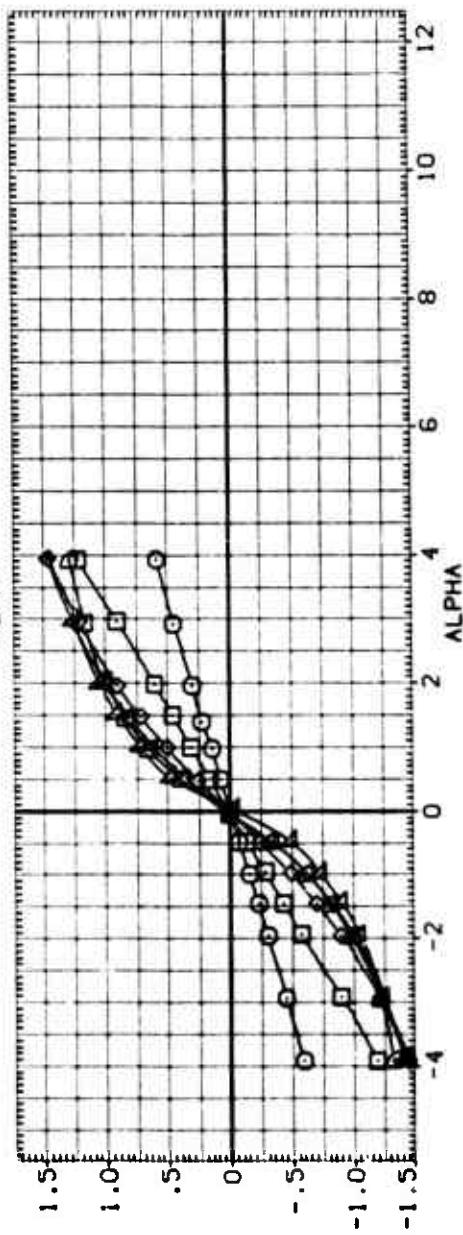
SCALE .0000

(RXE006)

SYMBOL  
O □ △ ▲ ▽



$C_n$



$C_{lm}$

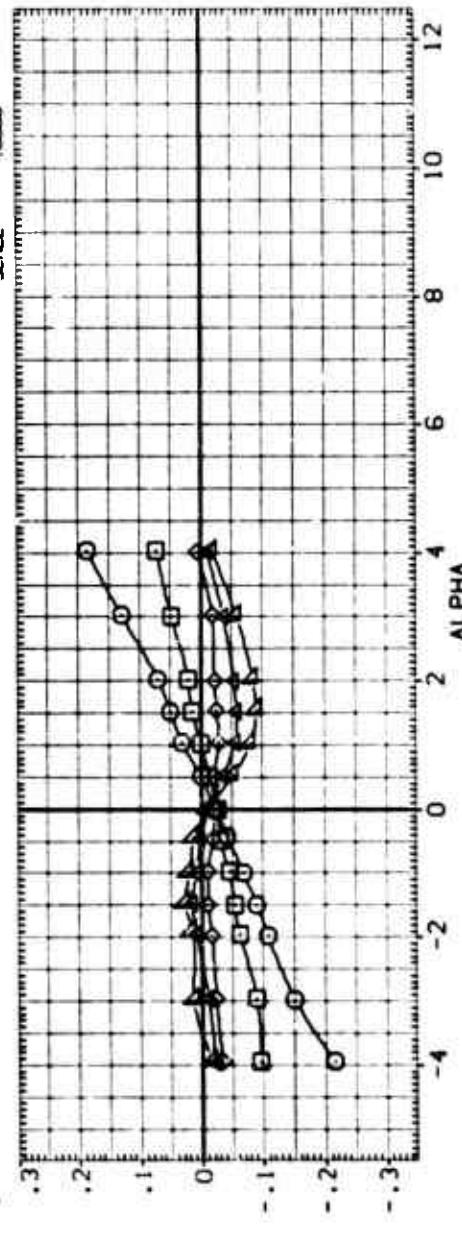
THRUST EFFECTS ON STABILITY CHARACTERISTICS

PAGE 5

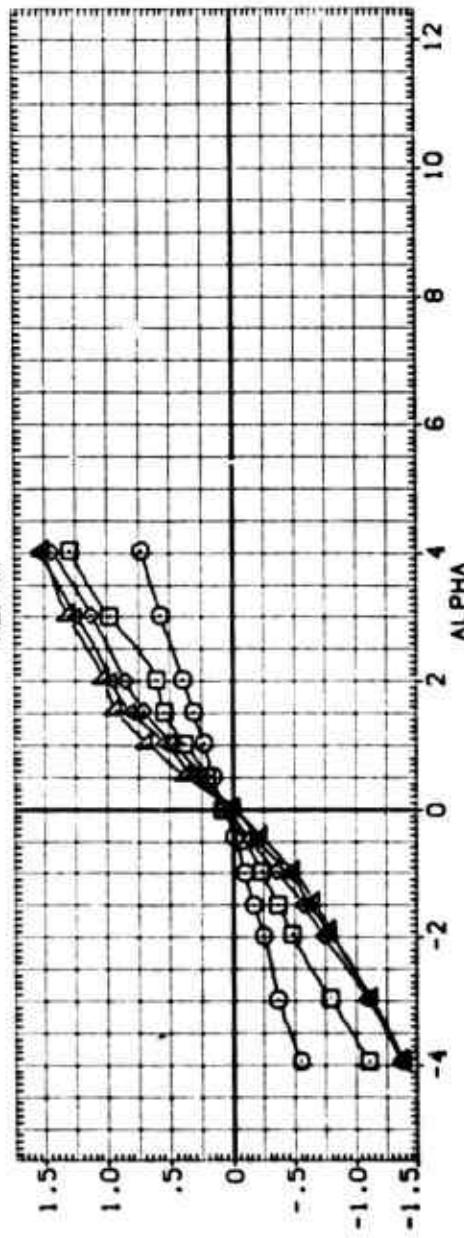
AEDC SF172 BODY ALONE, B  
 PARAMETRIC VALUES  
 CRIT .018      BETA .000      PHI .000  
 2.046      MACH 1.700  
 3.009  
 4.001  
 6.000

(RXE007)

REFERENCE INFORMATION  
 SPEC 19.6250 SD. IN.  
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 ZHSP 0.0000 IN.  
 SCALE .0000



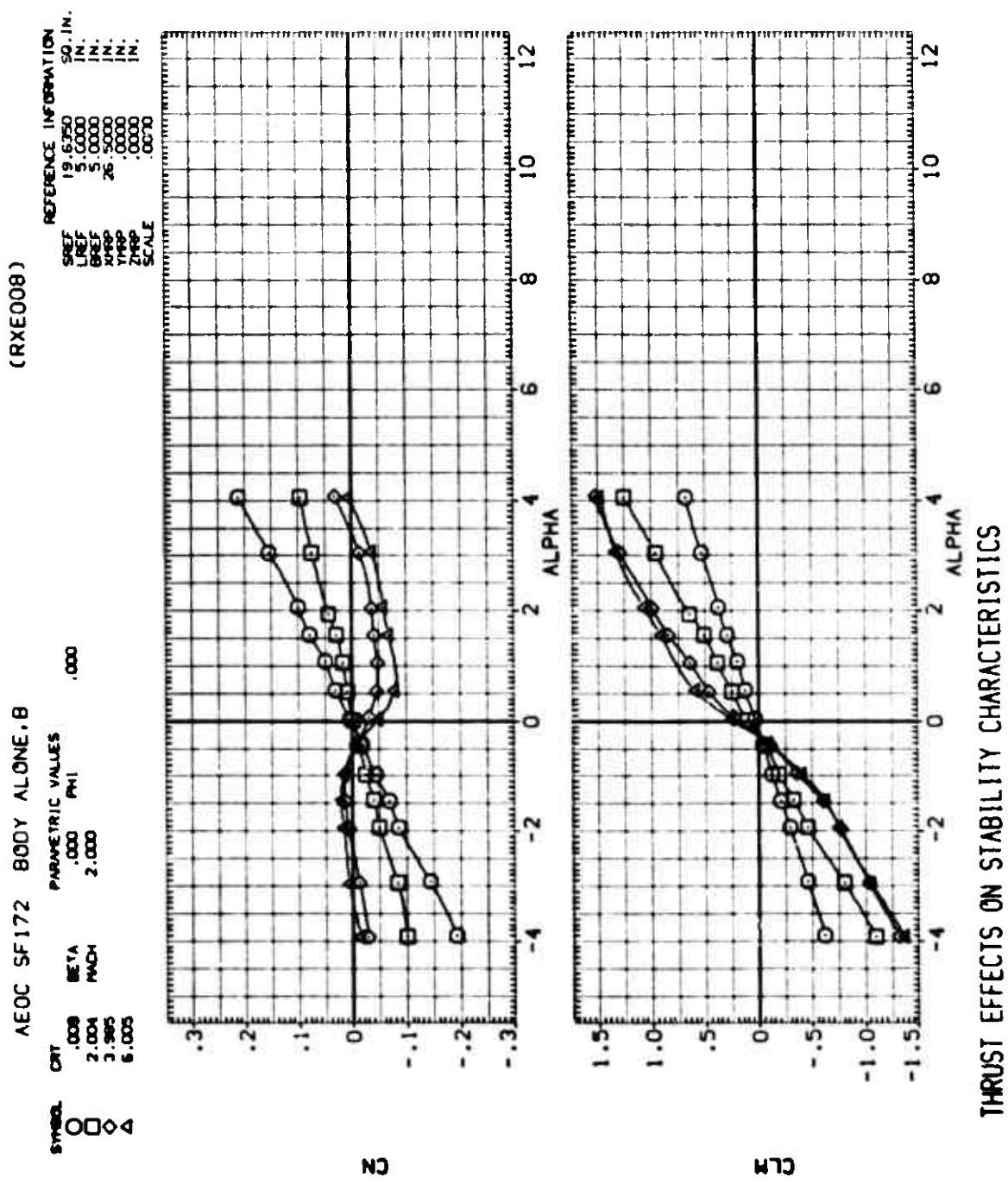
$C_n$



$C_{lm}$

THRUST EFFECTS ON STABILITY CHARACTERISTICS

PAGE 6



THRUST EFFECTS ON STABILITY CHARACTERISTICS

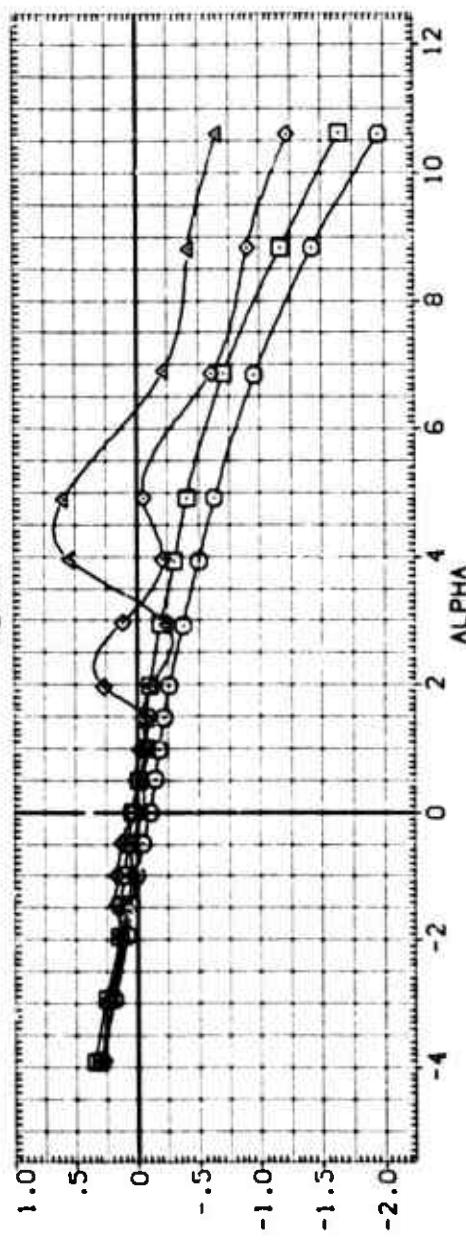
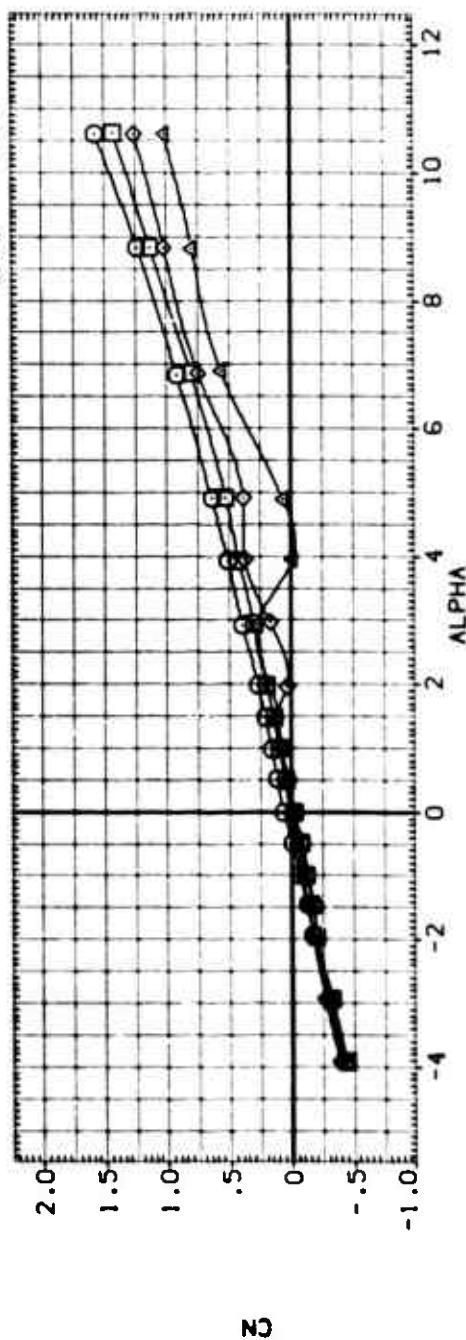
AEOC TF560 BODY FIN. BF1

Symbol	ON	BETA	PARAMETRIC VALUES
○	.575	.000	PHI .000
□	26.074	.3.000	MACH .200
◊	50.138		
△	100.918		

(RXE009)

REFERENCE INFORMATION

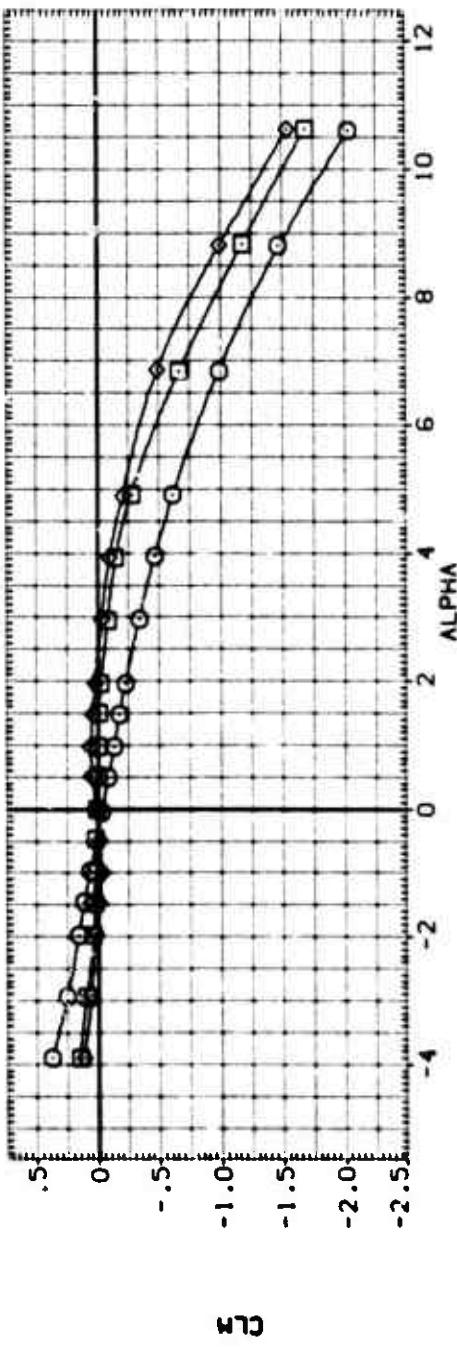
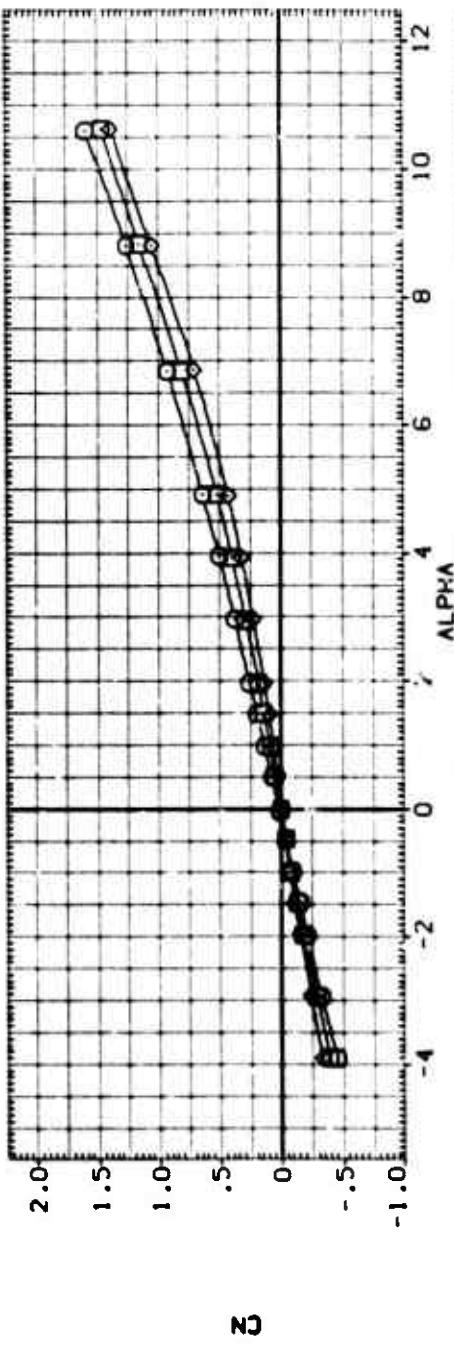
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BREF	.5.0000	IN.
XHBP	26.5000	IN.
YHBP	.0000	IN.
ZHBP	.0000	IN.
SCALE	.0000	



### THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY FIN. BFI  
 CRIT .1322      META .000      PHI .000  
 11.977      FINPOS 3.000      MACH .400  
 37.520

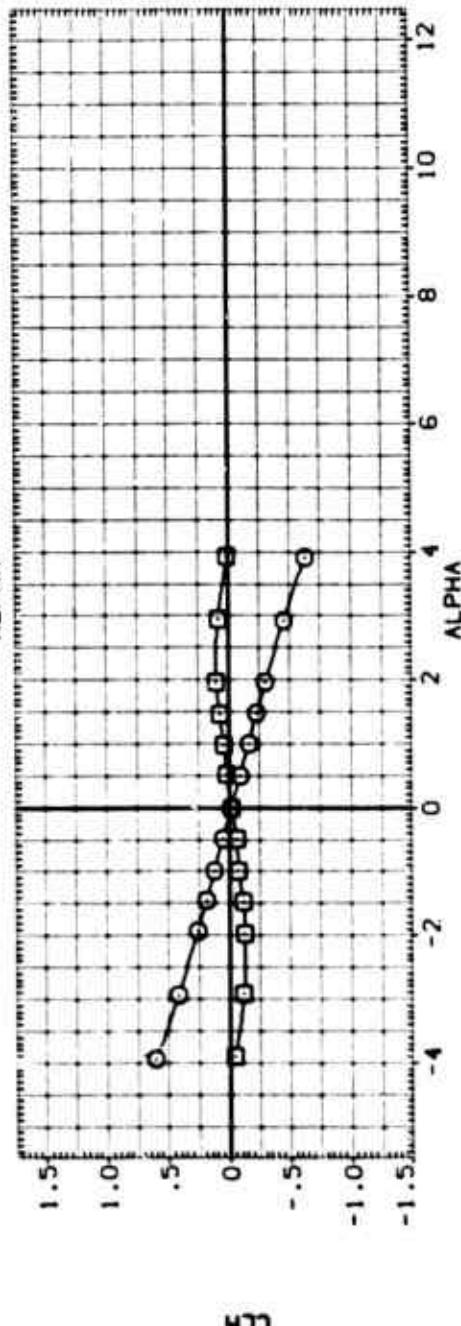
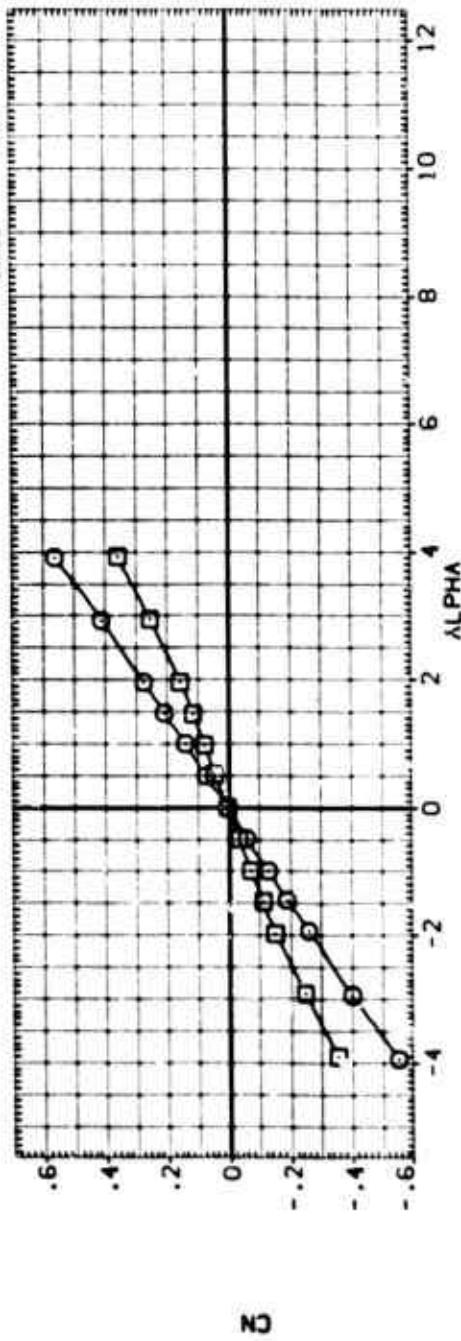
SYMBOLS  
 ○      □      ◊  
 REFERENCE INFORMATION  
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 LREF 5.0000      IN.  
 BREF 5.0000      IN.  
 XHPP 26.5000      IN.  
 YHPP .0000      IN.  
 ZHPP .0000      IN.  
 SCALE .0000



### THRUST EFFECTS ON STABILITY CHARACTERISTICS

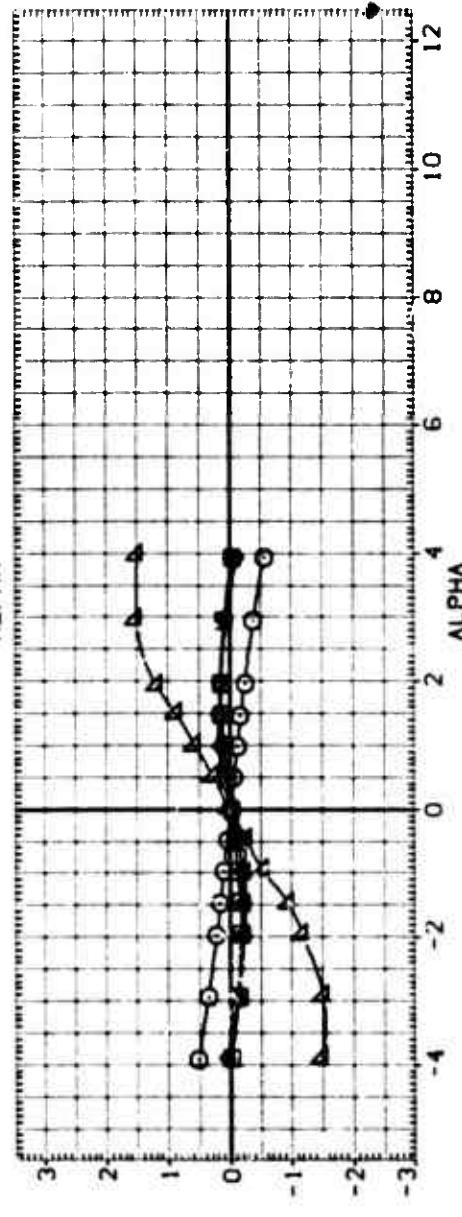
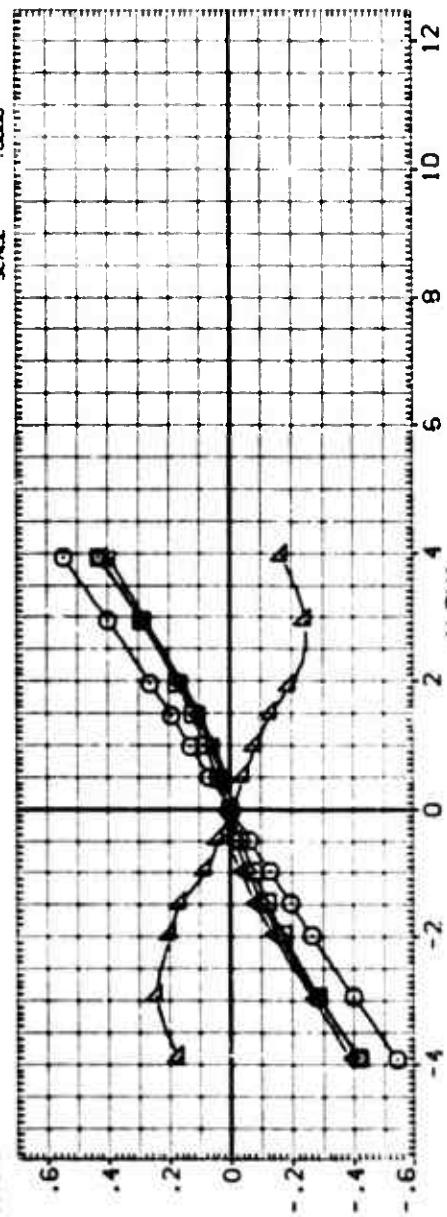
AEDC TF360 BODY FIN, BF1  
 SYMBOL COT .012 META .000 PHI .000  
 5.000 FINPOS 3.000 MACH 1.000

(RXE012)  
 REFERENCE INFORMATION  
 SHEF 19.6250 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 AREF 26.5000 IN.  
 VREF .0000 IN.  
 ZREF .0000 IN.



## THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY FIN. BF1  
 PHASED VALUES  
 CHF .010 META .000 PNL .000  
 3.042 FINPOS 3.000 PAON 1.250  
 4.014  
 6.006  
 11.875



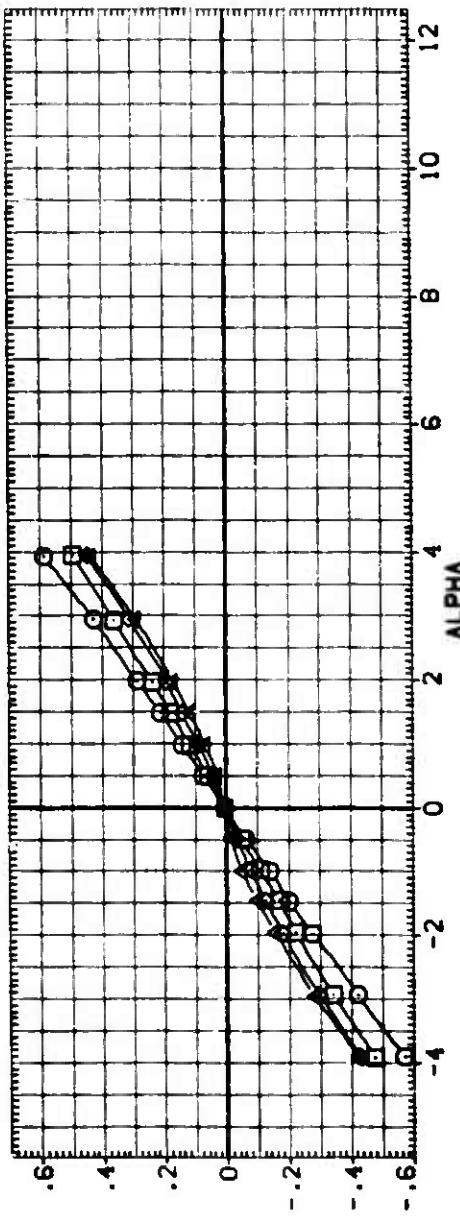
### THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY FIN, BF1

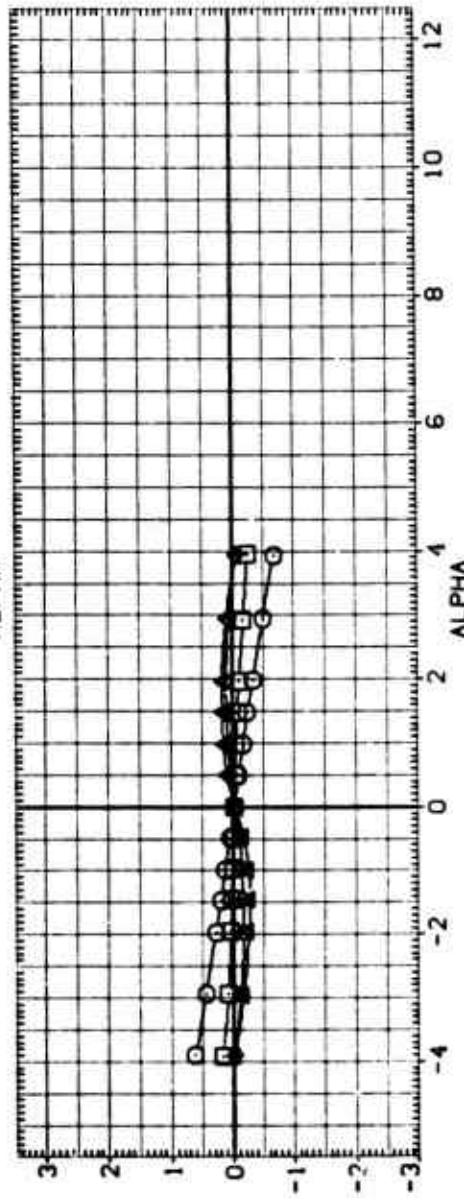
STRAU	CHT	META	PARAMETRIC VALUES	
○	.010	.000	PHI	.000
□	2.011	3.000	MACH	1.300
◊	3.012			
△	4.017			

(RXE014)

REFERENCE INFORMATION  
 SREF 19.6350 SO. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 YHPP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



$C_n$



$C_{lm}$

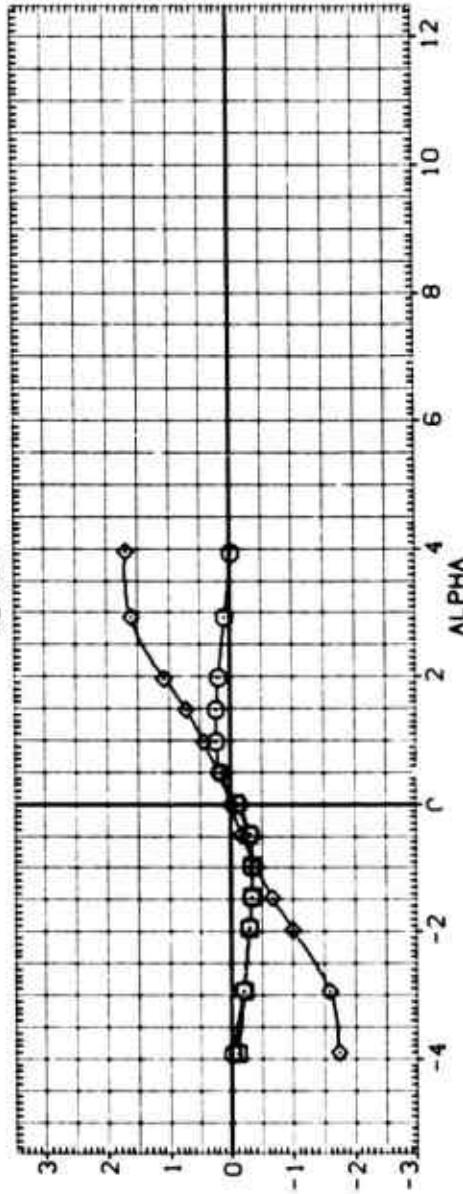
THRUST EFFECTS ON STABILITY CHARACTERISTICS

PAGE 12

AEDC TF360 BODY FIN. BF1  
 PARAMETRIC VALUES  
 CCR .000 PHI .000  
 BETA 5.989 FINPOS 3.000 MADL 1.500



Cn

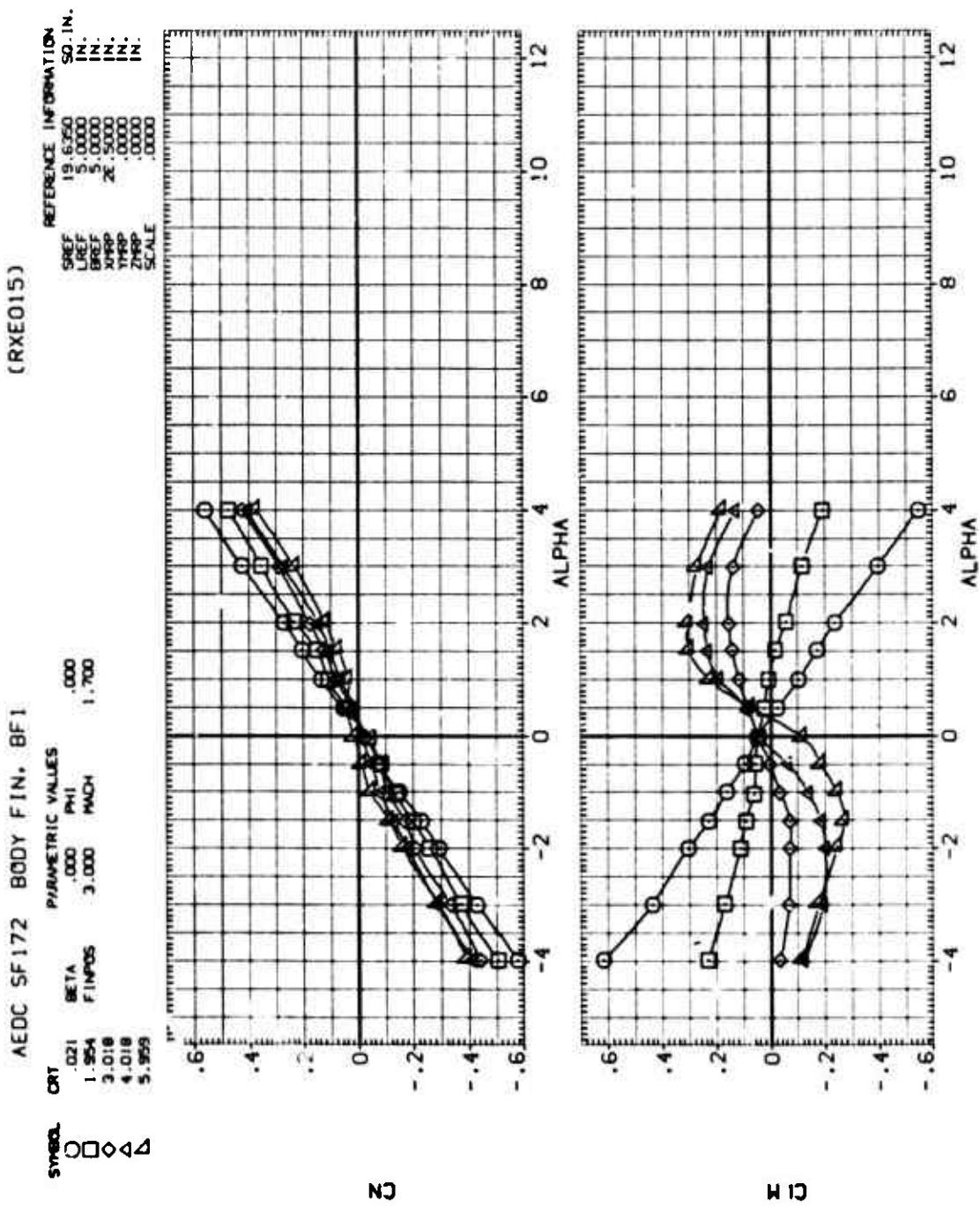


CLM

### THRUST EFFECTS ON STABILITY CHARACTERISTICS

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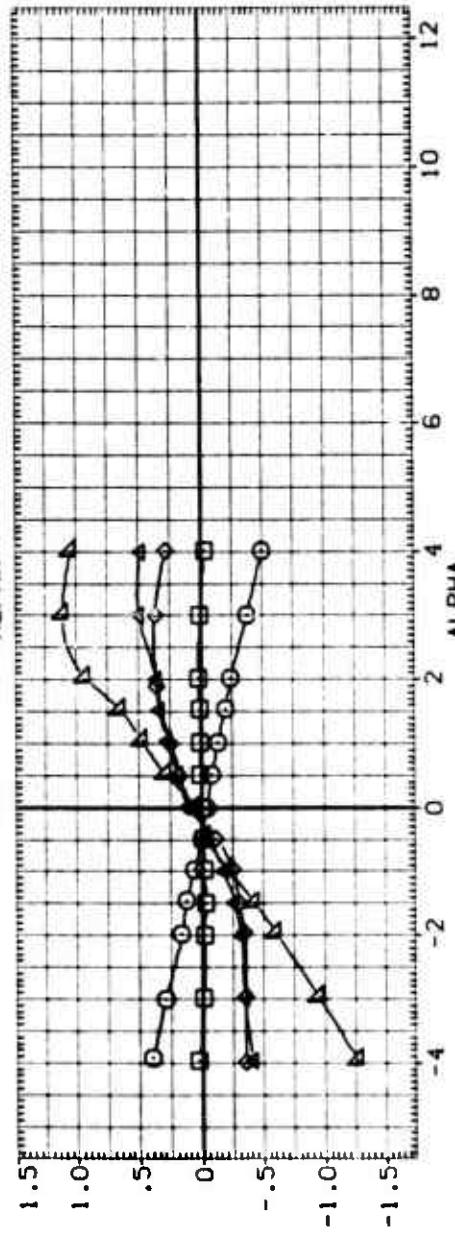
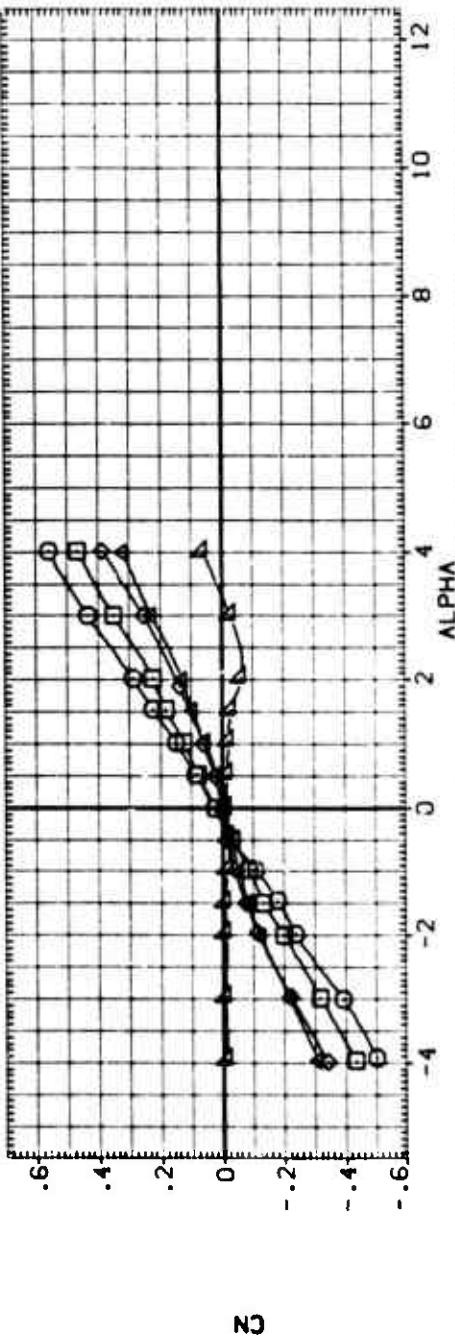
## THRUST EFFECTS ON STABILITY CHARACTERISTICS



AEDC SF172 BODY FIN. BFI  
 SYMBOLS DAT BETA .000 PHI .000  
 F1POS 2.011 MACH 2.000  
 3.999 6.009 11.932

(RXE016)

REFERENCE INFORMATION  
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 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 YHPP .00000 IN.  
 ZHPP .00000 IN.  
 SCALE .00000



### THRUST EFFECTS ON STABILITY CHARACTERISTICS

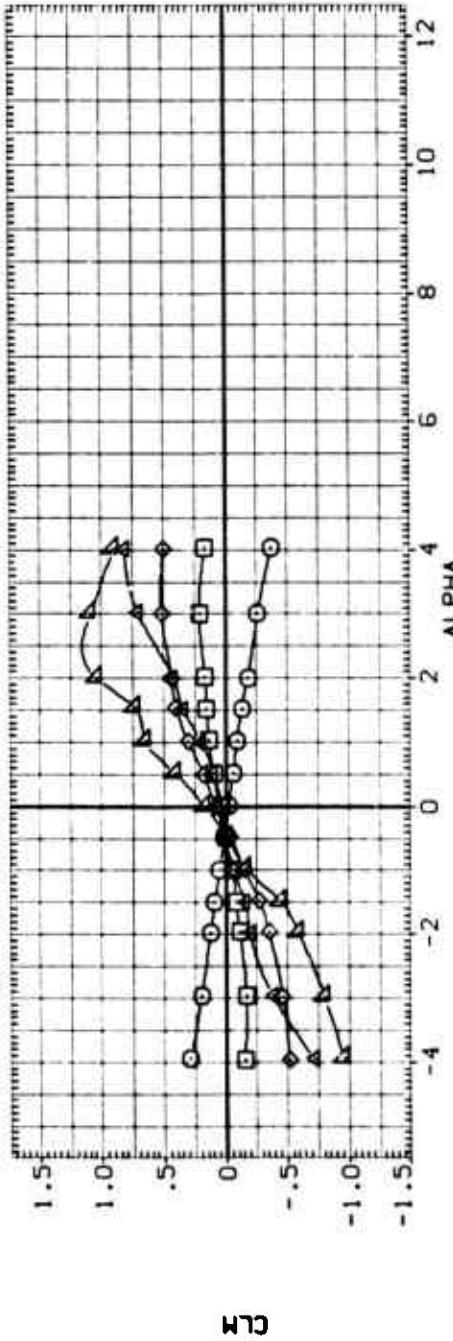
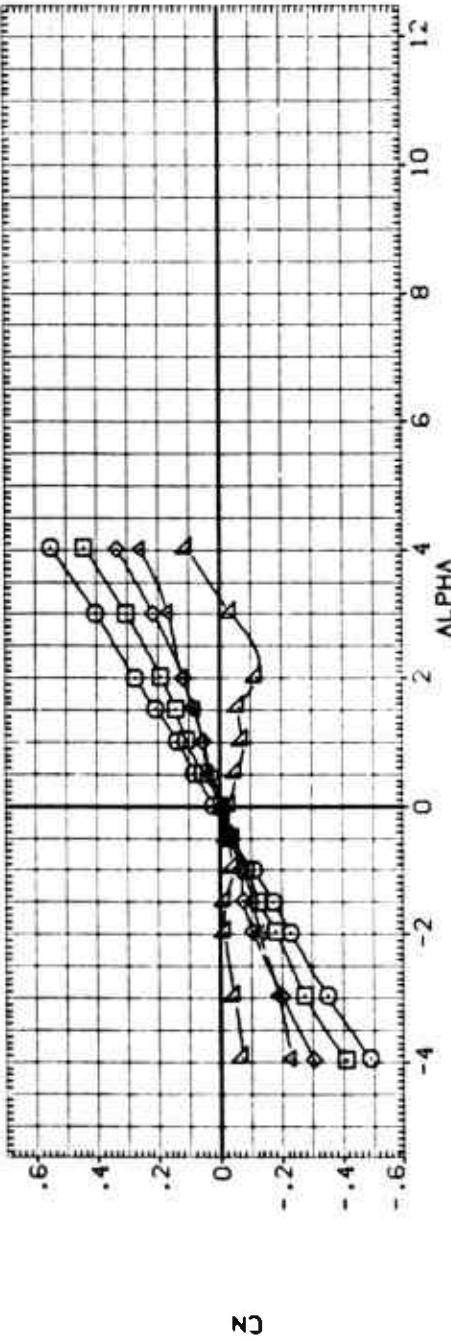
AEDC SF172 BODY FIN. BF1

Symbol	CRT	BETA	FINPOS	PHI	MACH
○	.021	.000	3.000	.000	2.300
□	.024				
△	.021				
◆	.052				
▲	.011				

(RXE017)

REFERENCE INFORMATION

REF	19.6750 IN.	50. IN.
LREF	5.0000	IN.
BREF	5.0000	IN.
XHPP	26.5000	IN.
YHPP	1.0000	IN.
ZHPP	1.0000	IN.
SCALE	1.0000	IN.



### THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY FIN, BF2

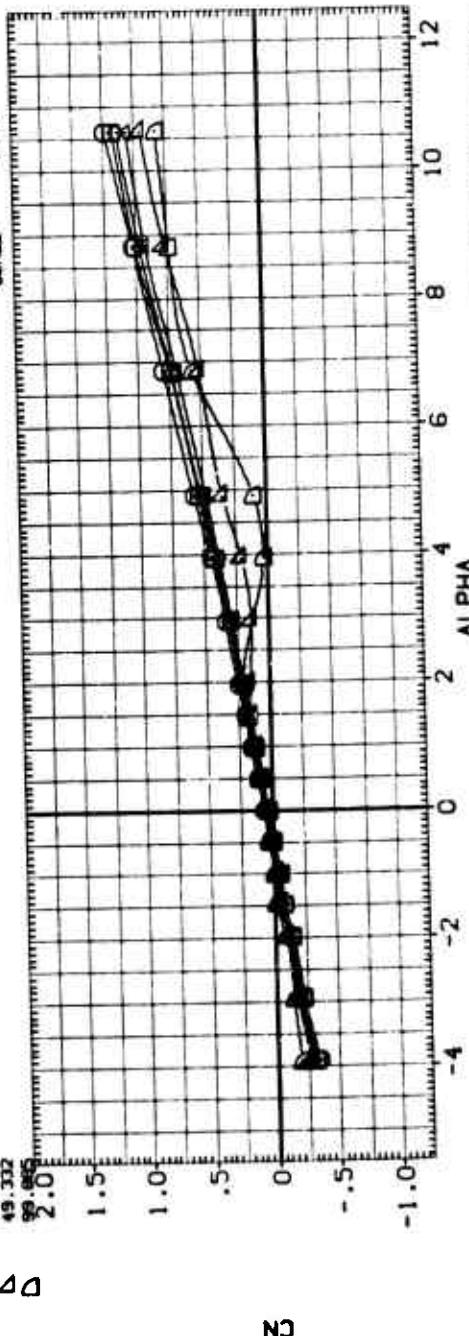
PARAMETRIC VALUES

CNT	BETA	PHI
.542	.000	.000
5.253	3.000	MACH
12.314		.200
25.314		
49.332		
98.865		

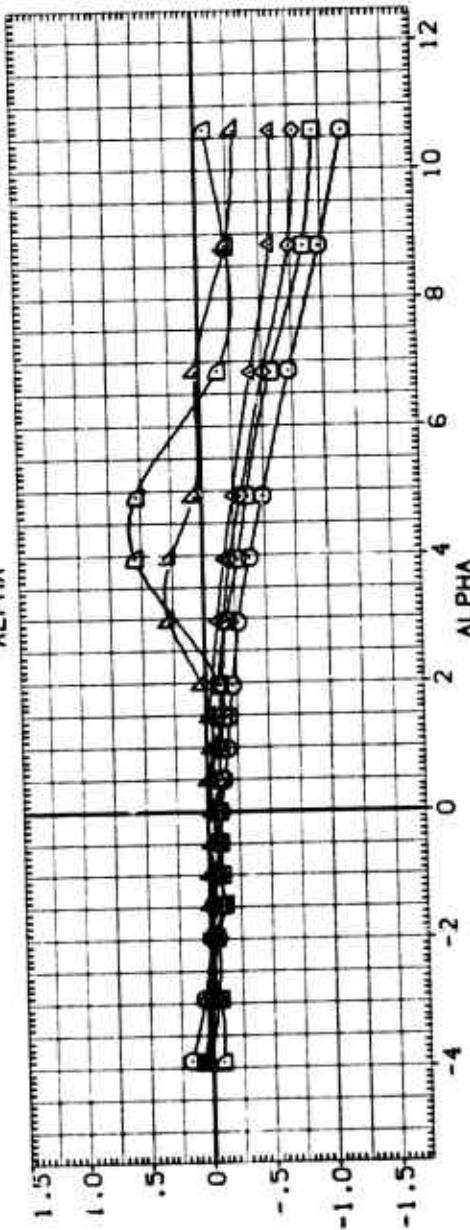
SYMBOLS  
 ○ □ △ ◇ ▲ ▾ ▶ ▷

(RXE018)

REFERENCE INFORMATION  
 SHEF 19.6350 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHBP .26.0000 IN.  
 YHBP .000000 IN.  
 ZHBP .000000 IN.  
 SCALE .0000



CN



CL<sub>x</sub>

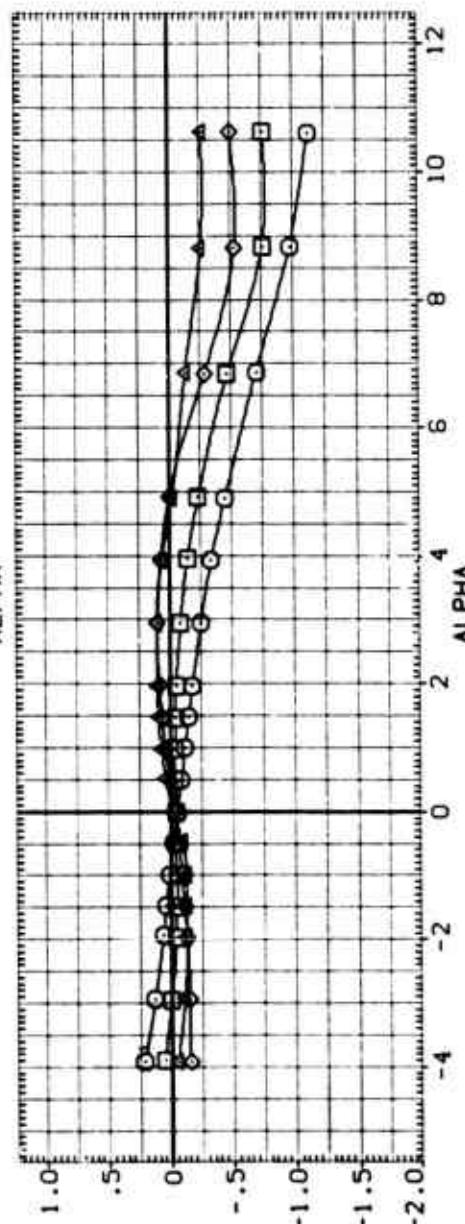
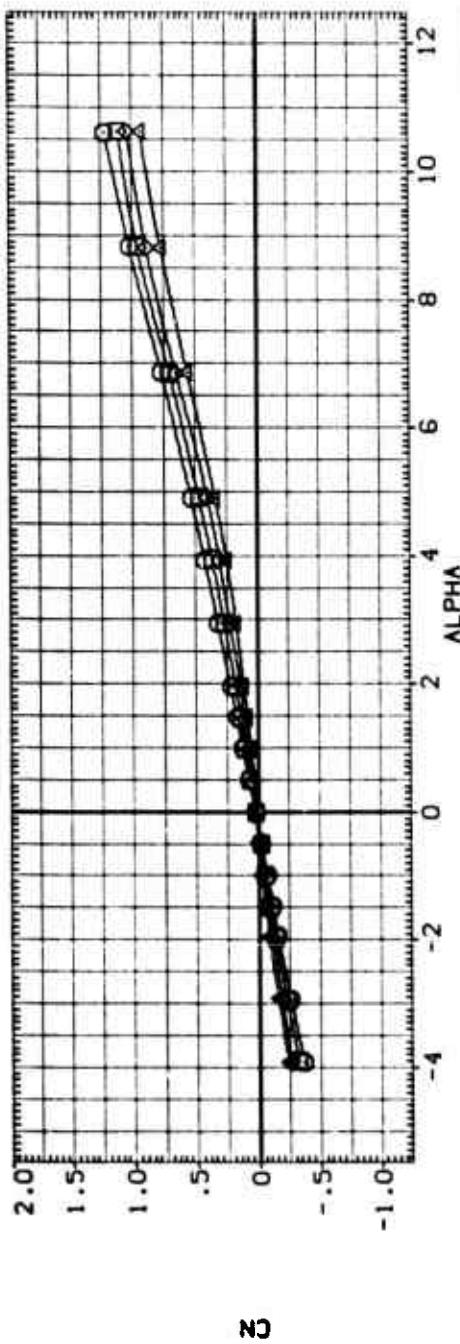
THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY FIN, BF2

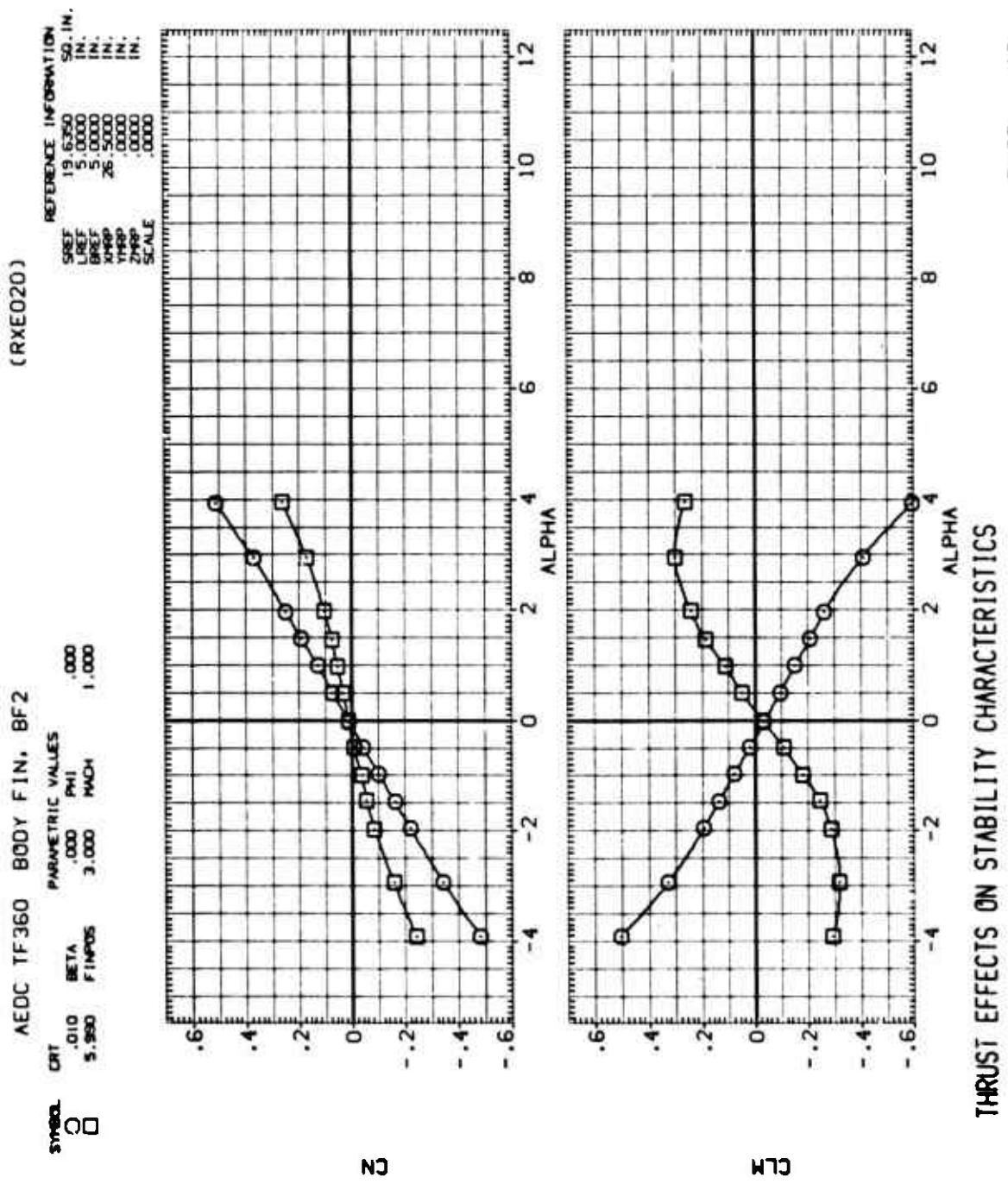
	PARAMETRIC VALUES
CRIT	.120
BETA	5.713
FINPOS	3.000
PHI	.000
MACH	.400

(RXE019)

REFERENCE INFORMATION  
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 SCALE .0000



### THRUST EFFECTS ON STABILITY CHARACTERISTICS



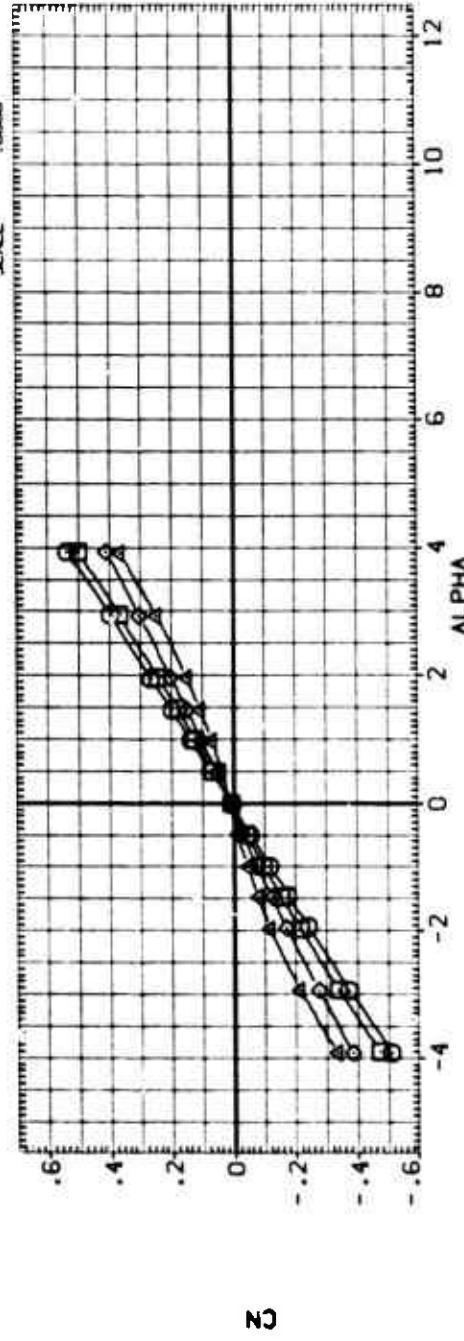
### THRUST EFFECTS ON STABILITY CHARACTERISTICS

AEDC TF360 BODY FIN, BF2

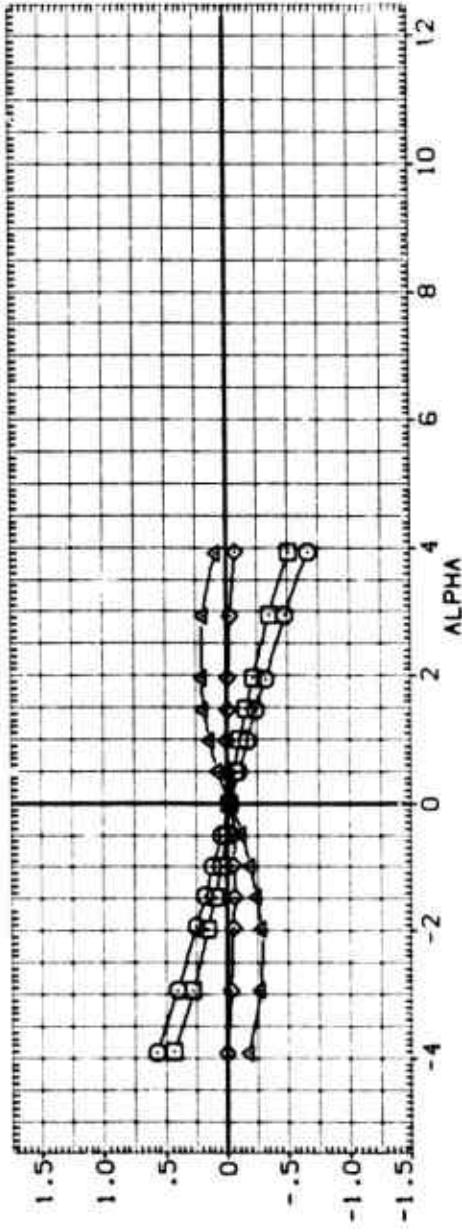
PARAMETRIC VALUES	PHI	MACH
0.000	.000	1.250
.694	FINPOS	
2.016		
3.015		

(RXE021)

REFERENCE INFORMATION  
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 YHPP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



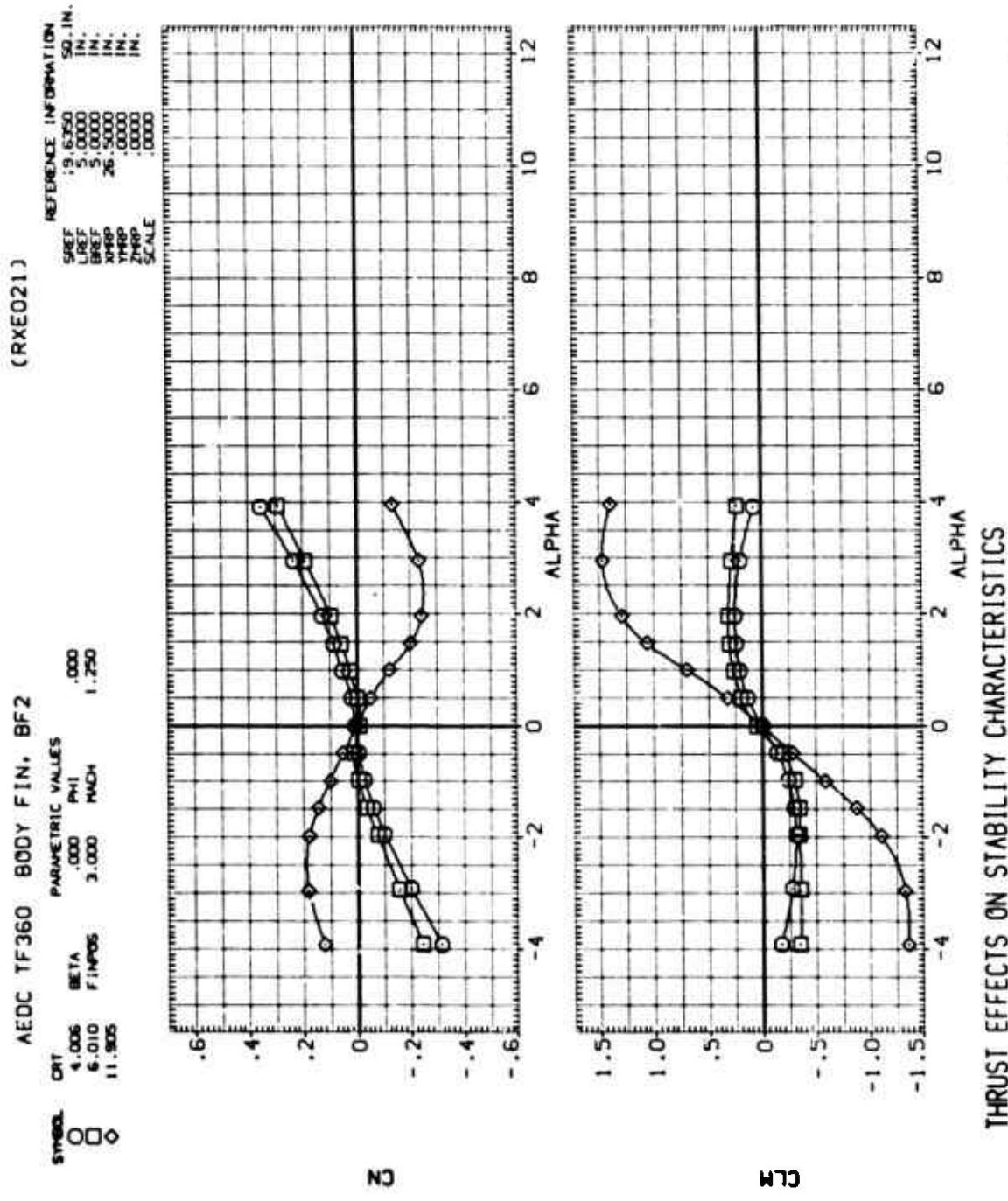
$C_n$



$C_{lh}$

### THRUST EFFECTS ON STABILITY CHARACTERISTICS

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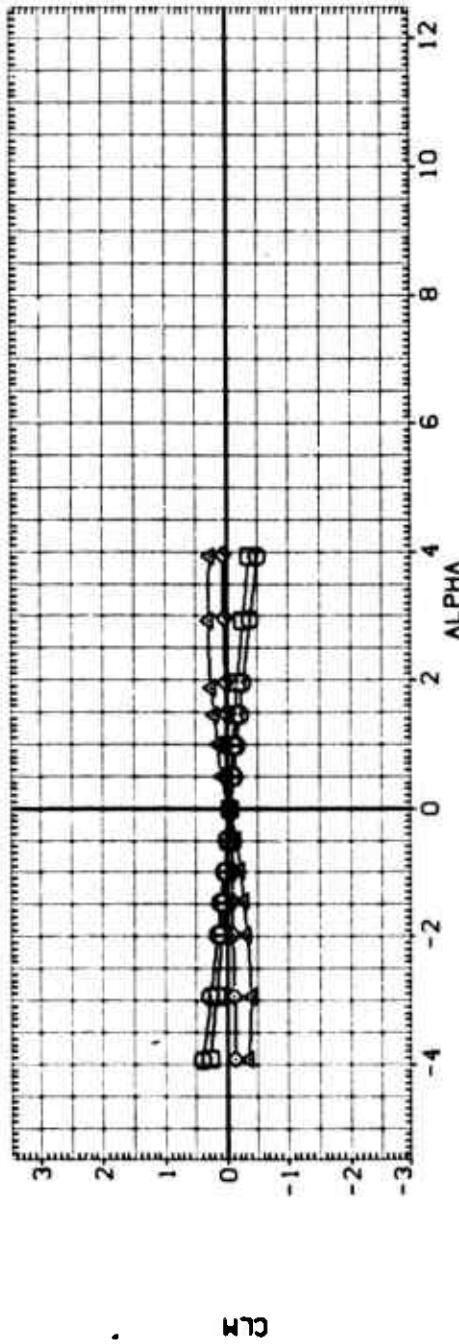
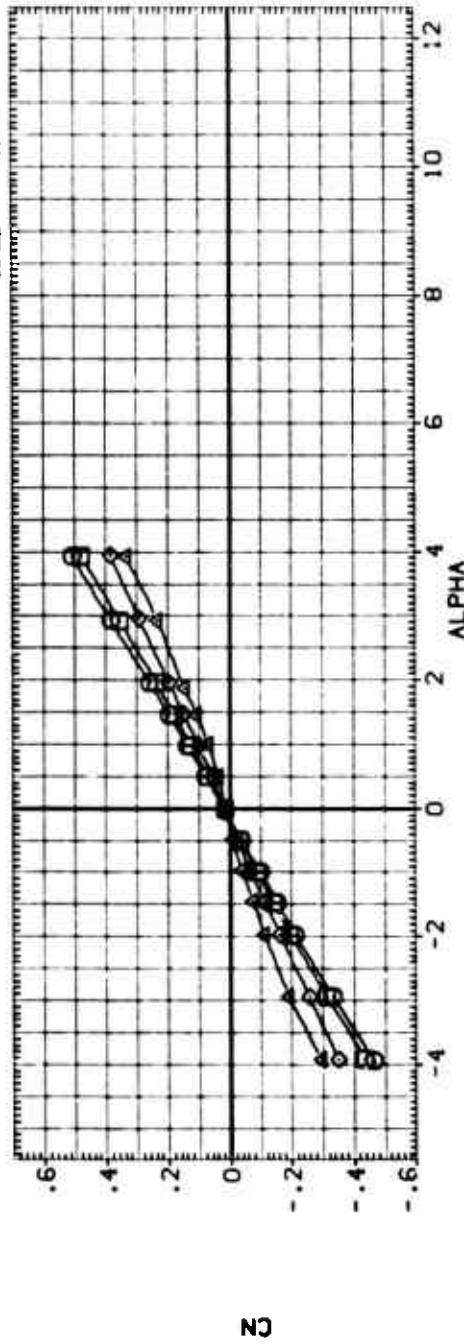


### THRUST EFFECTS ON STABILITY CHARACTERISTICS

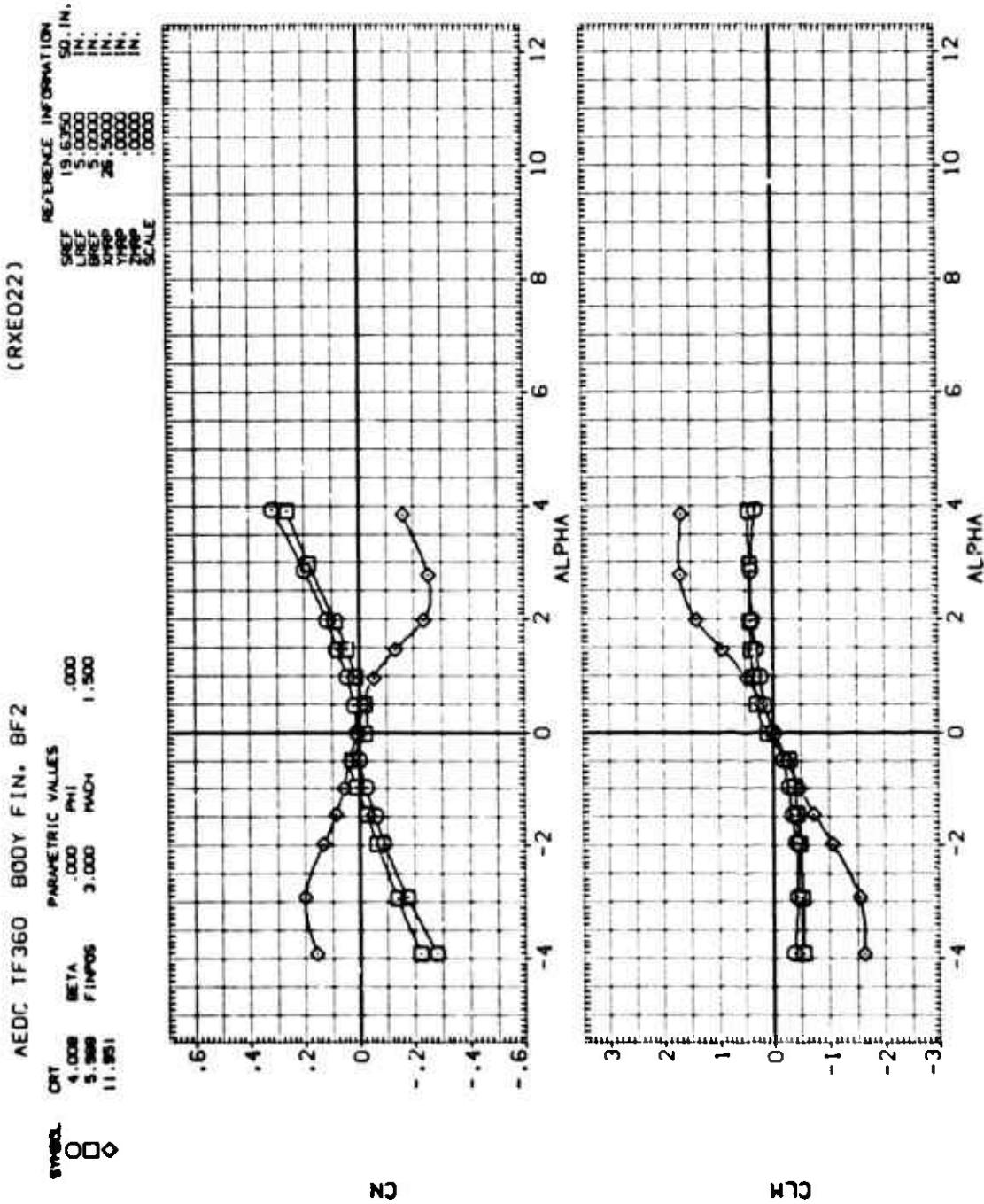
SYMBOL	OPT.	PARAMETRIC VALUES			BF2
		BETA	F1POS	PHI	
AEDC	.010			.000	
TF360	.993			3.000	MACH

(RXE022)

REFERENCE INFORMATION		SO. IN.
SREF	19-6360	
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BREF	5.0000	
PRM	25.5000	
PRMX	.000000	
SPR	.000000	
SPRP	.000000	
SPRF	.000000	



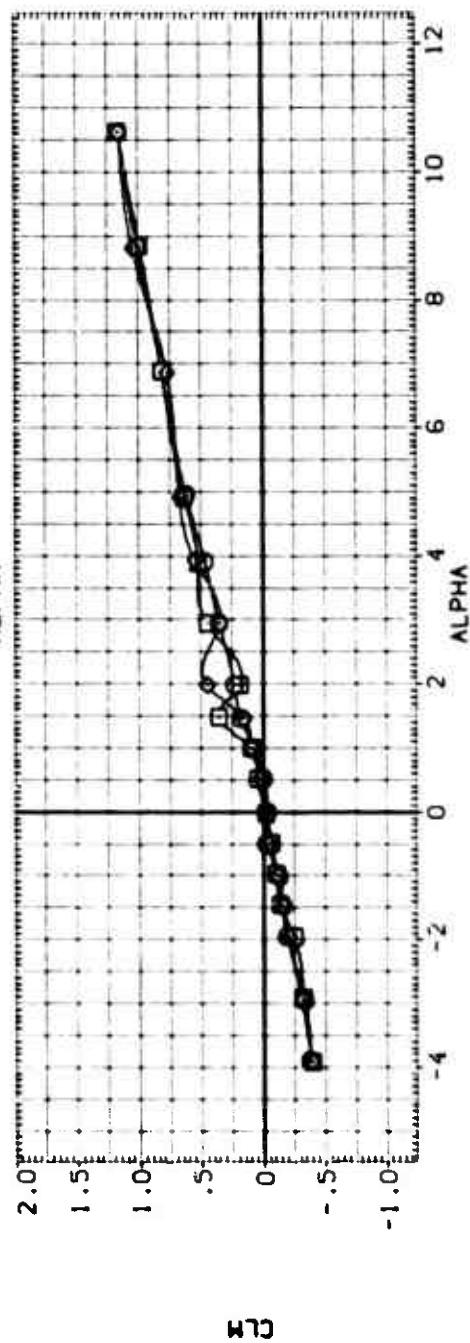
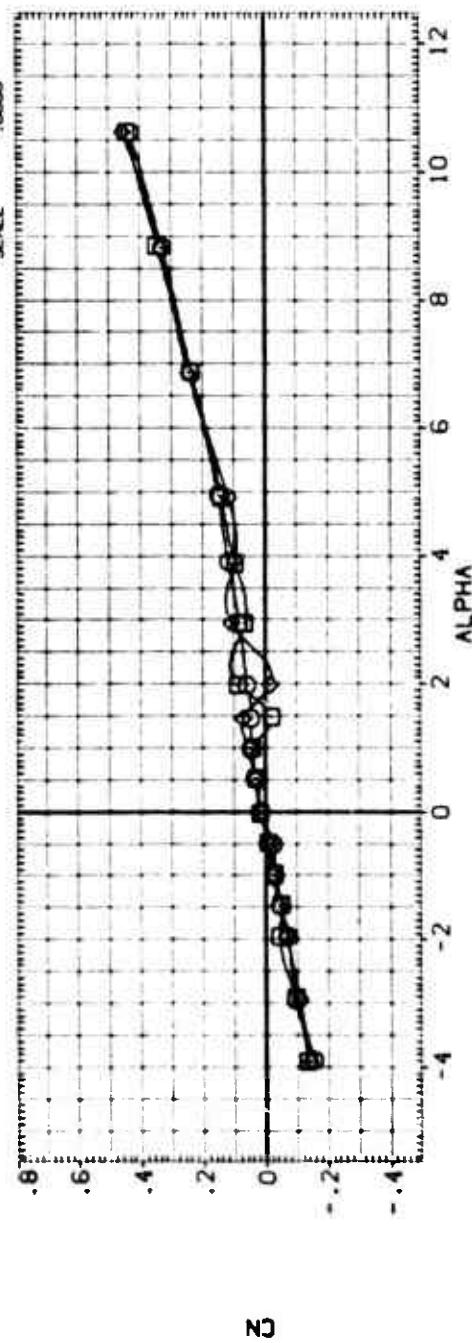
## THRUST EFFECTS ON STABILITY CHARACTERISTICS



### THRUST EFFECTS ON STABILITY CHARACTERISTICS

DATA SET SYMBOL CONFIGURATION DESCRIPTION  
 BAC0021 AEDC T-380 BODY ALONE, BI INCREASING ALPHA  
 BAC0022 AEDC T-380 BODY ALONE, BI DECREASING ALPHA  
 BAC0023 AEDC T-380 BODY ALONE, BI INCREASING ALPHA  
 BAC0024 AEDC T-380 BODY ALONE, BI DECREASING ALPHA

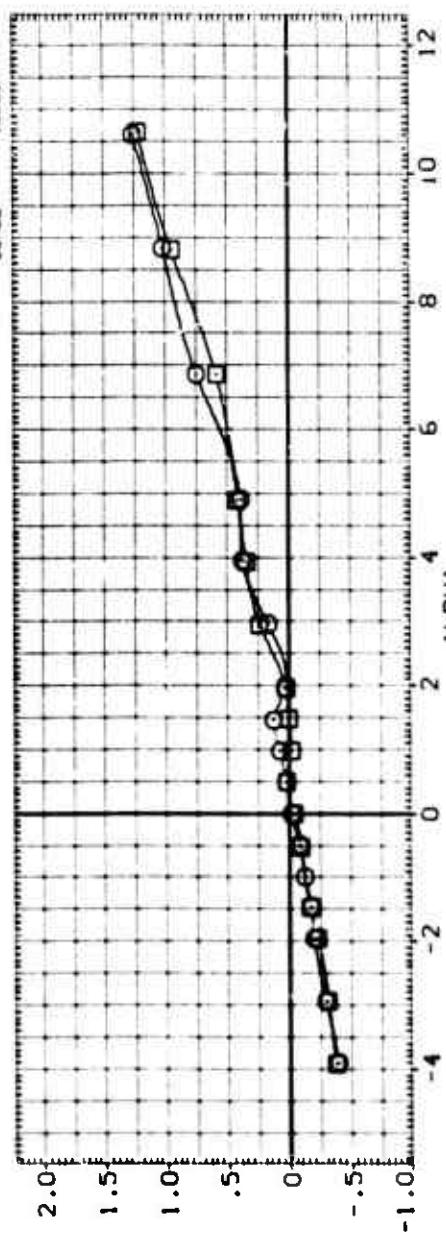
BETA .0000 .0000 .0000 .0000  
 PHI .0000 .0000 .0000 .0000  
 MACH .200 .200 .200 .200  
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 SREF 19.6250 SQ. IN.  
 LREF 5.0000 IN.  
 SREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 YHPP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



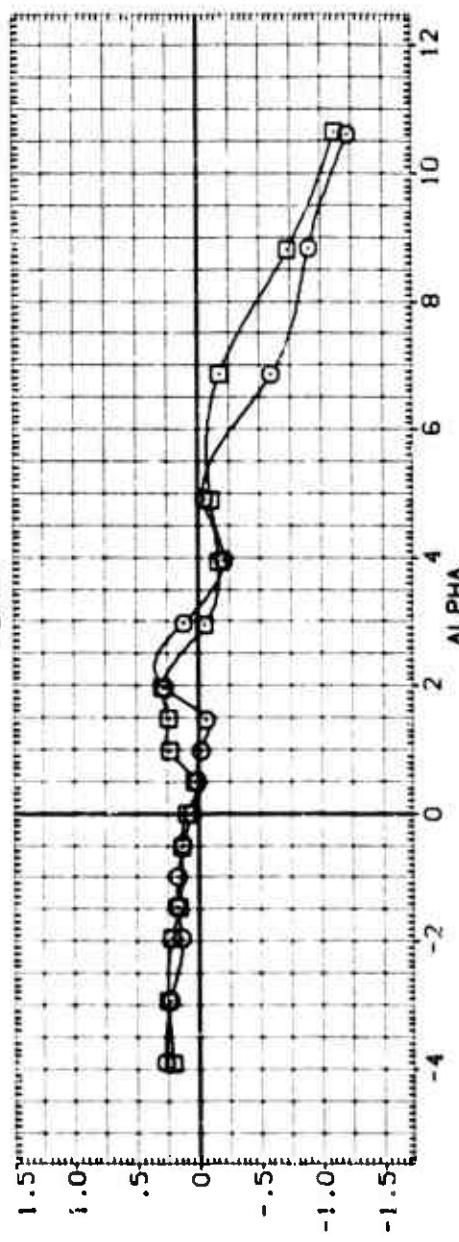
HYSTeresis Effects  
 $(\Delta)_{CRT} = 50.61$

DATA SET SYMBOL      CONFIGURATION DESCRIPTION  
 (BNE009)      AEDC TF360 BODY FIN, B (I) INCREASING ALPHA  
 (BNE023)      AEDC TF360 BODY FIN, B (I) DECREASING ALPHA

BETA .000 PHI .000 FIN05 MACH .200  
 BETA .000 PHI .000 FIN05 MACH .200  
 REF 19.6350 SC. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 RREF 26.5000 IN.  
 TREF .0000 IN.  
 ZREF .0000 IN.  
 SCALE .0000



CN

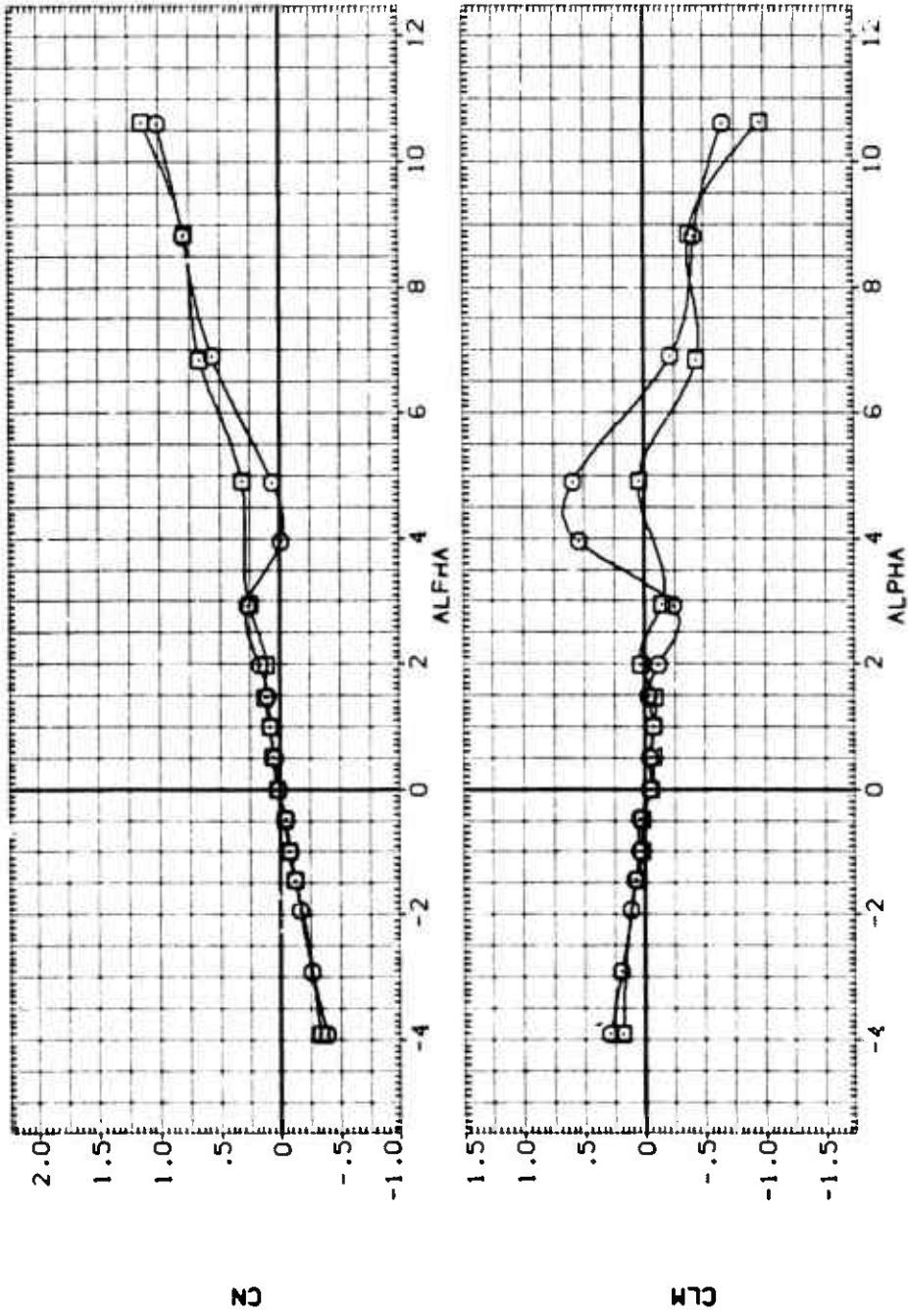


CL<sub>A</sub>

HYSERESIS EFFECTS  
 $(\Delta)_{CRT} = 50.14$

DATA SET SYMBOL: CONFIGURATION DESCRIPTION  
 (B)E009 AEDC TF360 BODY FIN, BF1 (INCREASING ALPHA)  
 (B)E025 AEDC TF360 BODY FIN, BF1 (DECREASING ALPHA)

BETA .000 PHI .000 FINPOS 3.000 MACH .200 SPEC 19.6350 50. IN.  
 .000 .000 3.000 .200 LINEF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 YHPP -.0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



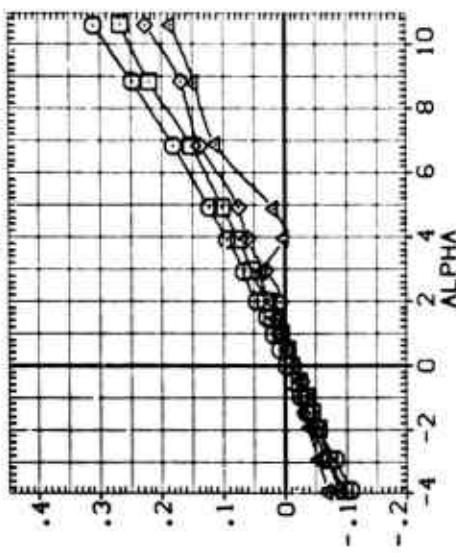
HYSTERESIS EFFECTS  
 (B)CRT = 100.92

AEDC TF360 BODY F1N. BF1

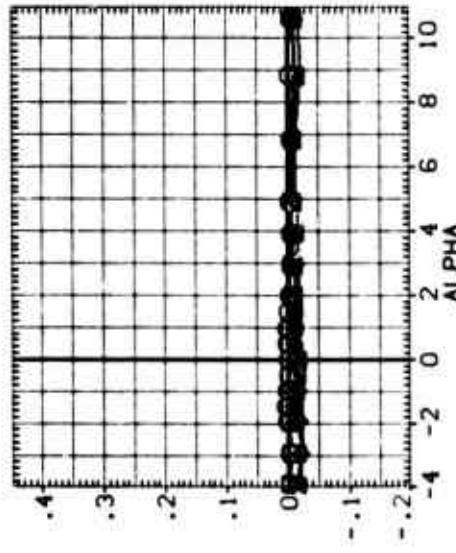
	CRT	BETA	Psi	MACH	.000
SIGMA	.575				.000
Symbol	○	□	△	◊	
FINPS	26.074	5.000	100.132	50.132	
MACH	.200				

(RXE109)

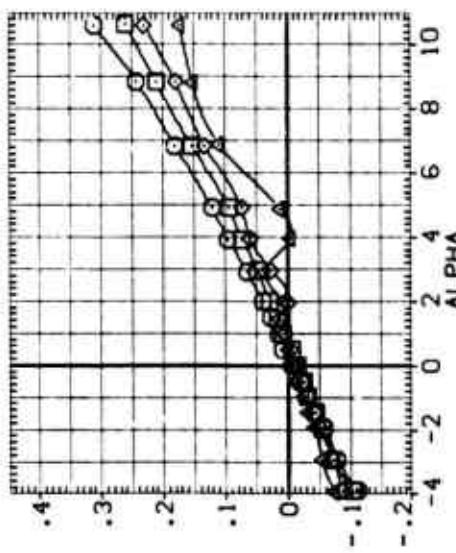
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 SCALE .00000



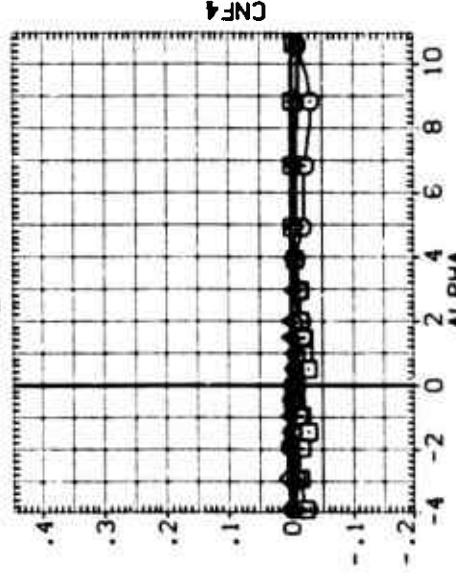
CNF1



CNF2



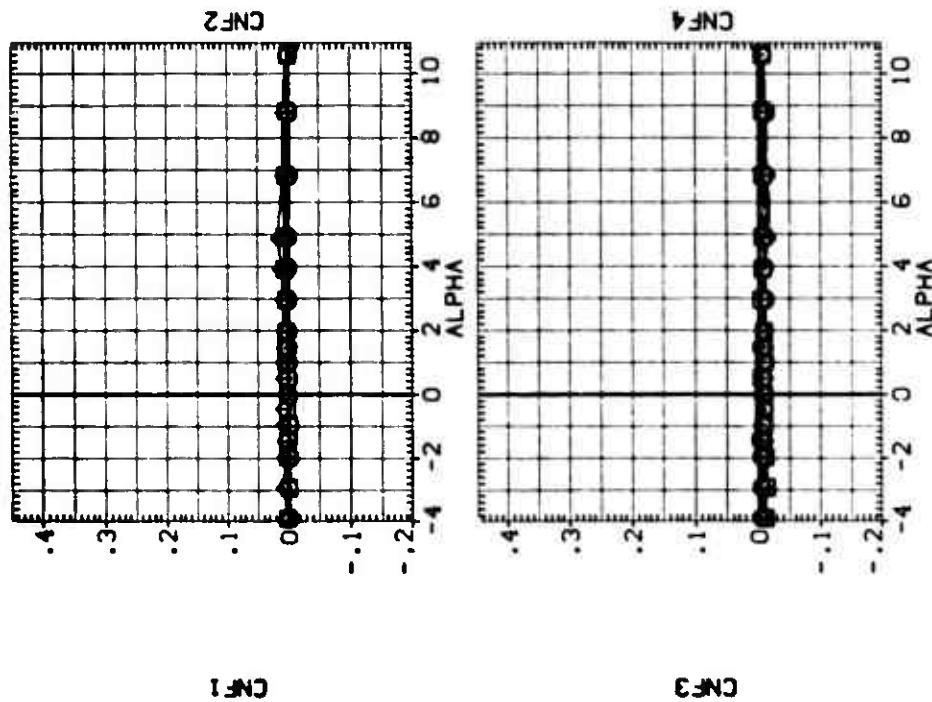
CNF3



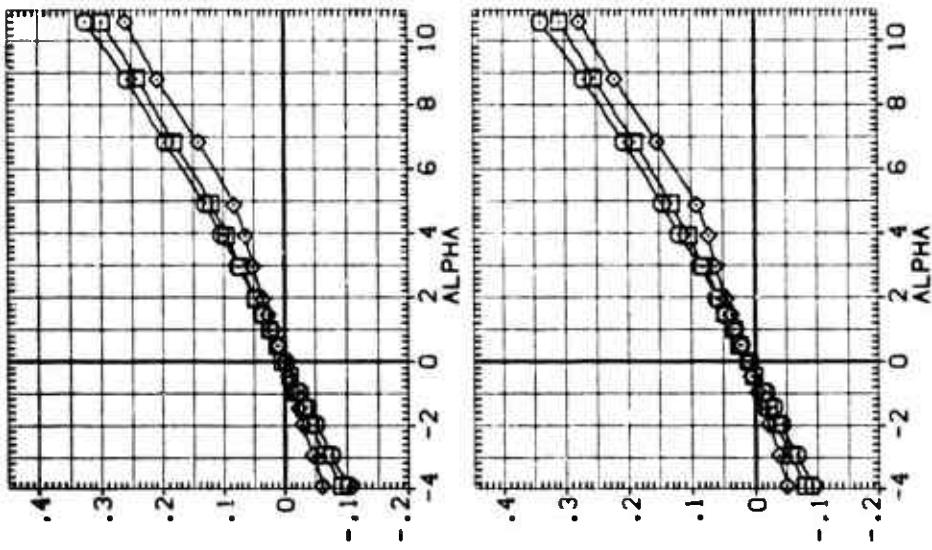
CNF4

THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 BODY FIN. BF1			
PARAMETRIC VALUES			
ORT	.132	BETA	.000
11.877		FIN05	PHI
			MACH
SMALL	37.800		



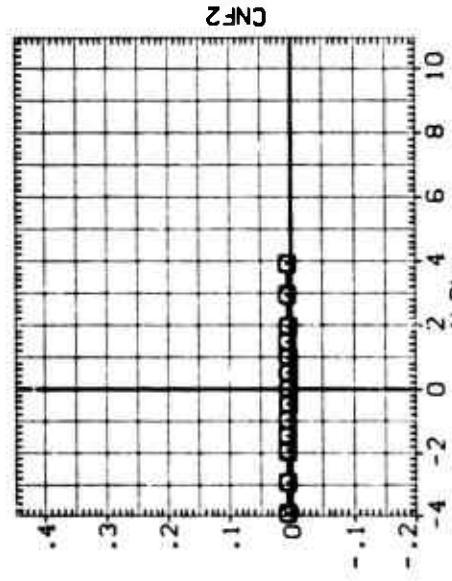
(RxE111)



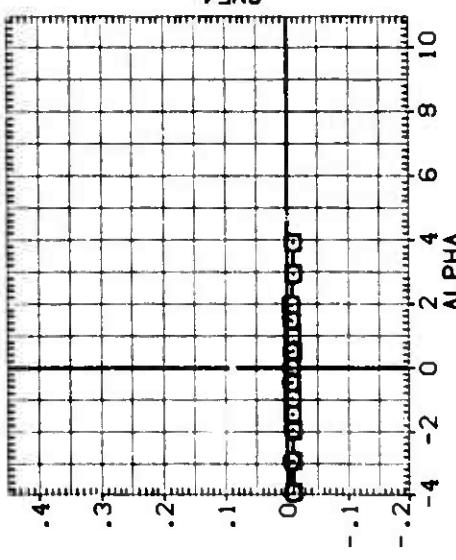
AEDC TF360 BODY FIN. BF1  
 CRT .012 PH1 .000 MACH 1.000  
 5.885 FINPOS .000

(RXE112)

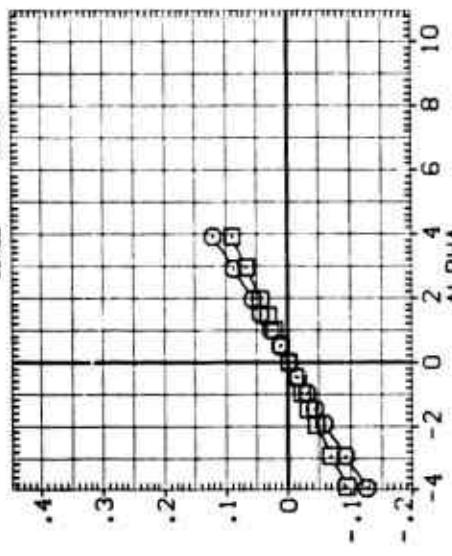
REFERENCE INFORMATION  
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 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 YHPP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



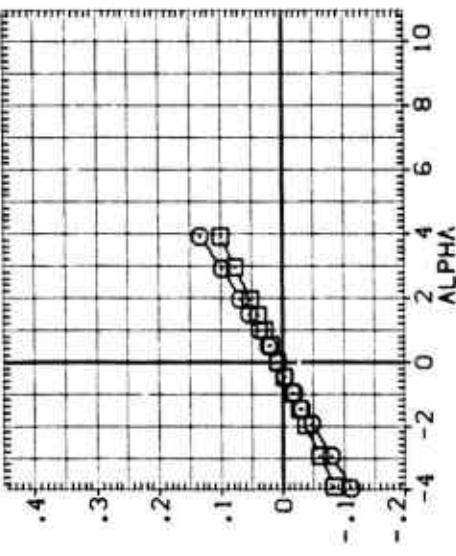
CNF1



CNF3



CNF2



CNF4

THRUST EFFECTS ON FIN NORMAL FORCE

AEOC TF360 BODY FIN, BF1

PARAMETRIC VALUES			
CRT	BETA	PHI	MACH
.010	.000	.000	.000
3.042	FINPOS	3.000	1.250
4.014			
6.006			
11.526			

SYMBOLS

- CREF
- LREF
- ◊ BREF
- △ AREF
- ▲ TREF
- ◆ ZREF

(RXE113)

REFERENCE INFORMATION

SREF 19.6250 SQ. IN.

LREF .0000 IN.

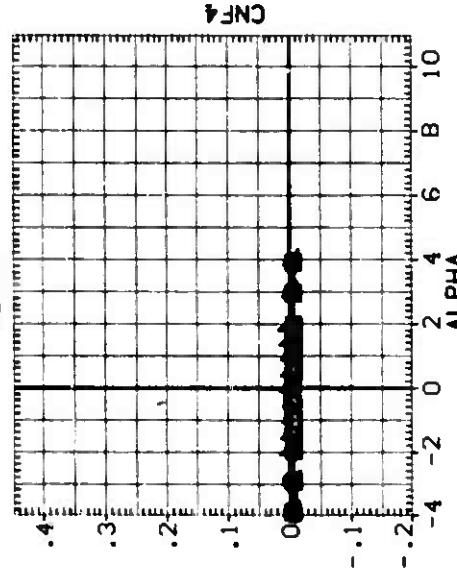
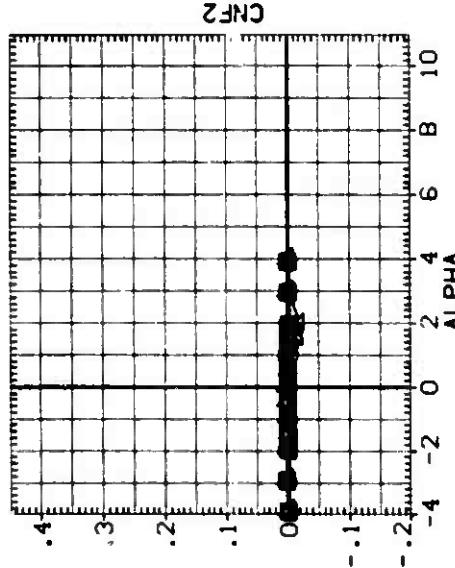
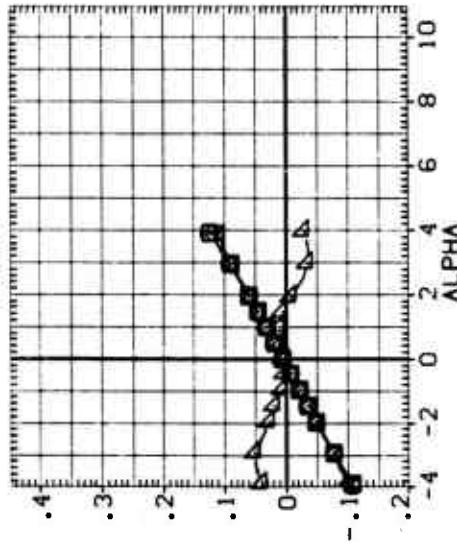
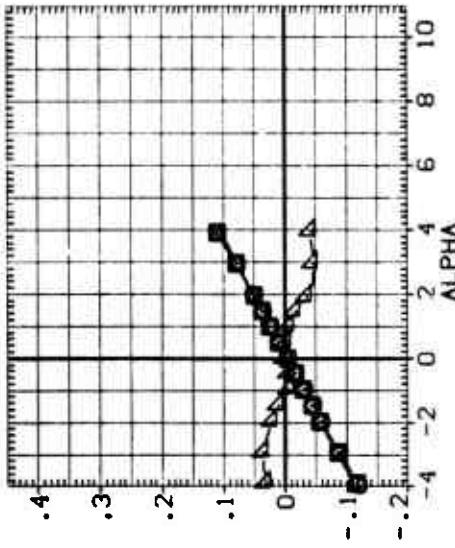
BREF .0000 IN.

AREF .0000 IN.

TREF .0000 IN.

ZREF .0000 IN.

SCALE .0000



THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 BODY FIN. BF1

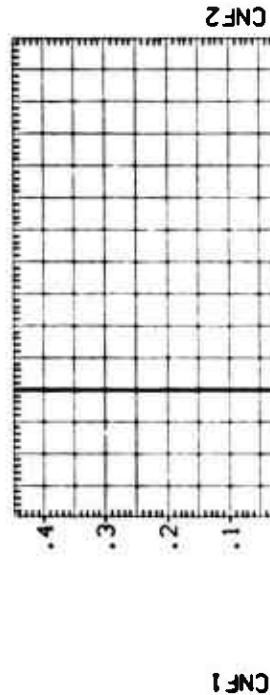
	CRT	BETA	PARAMETRIC VALUES	PHI	.000
SMALL	2.010	FINPOS	3.000	MACH	.500
	2.011				
	3.012				
	4.017				

SMALL  
○ □ ◇ △

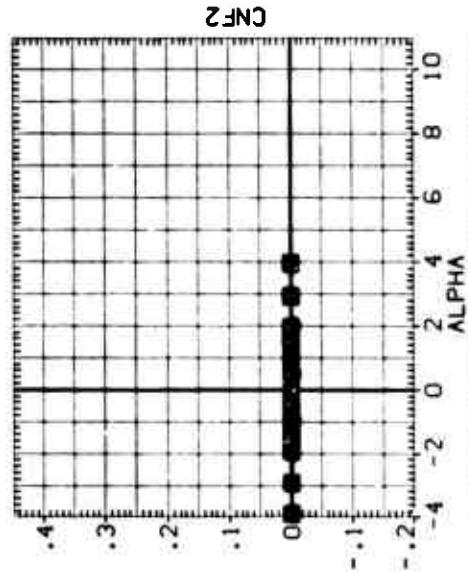
(RXE114)

REFERENCE INFORMATION

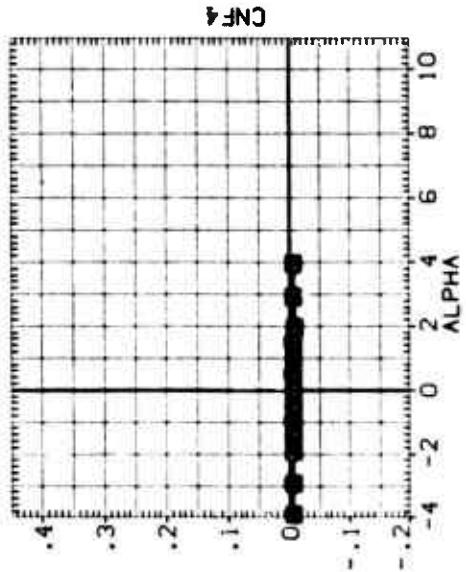
SREF	19.6300	SD, IN.
LREF	5.0000	IN.
BREF	5.0000	IN.
XHBP	26.5000	IN.
YHBP	-0.0000	IN.
ZHBP	-0.0000	IN.
SCALE	.0000	



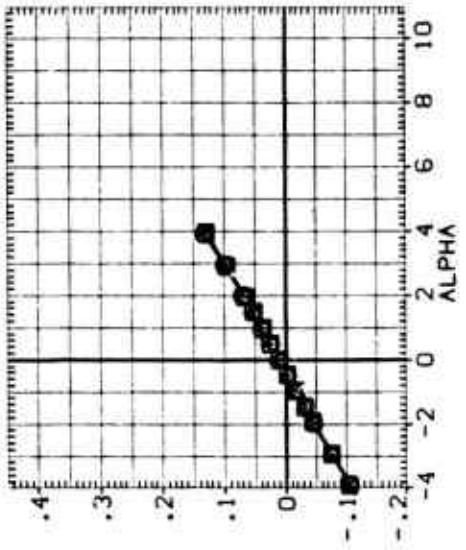
CNF1



CNF2



CNF3



CNF4

THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 BODY FIN. BF1

	PARAMETRIC VALUES
$\alpha$	.000
$\beta$	.000
$\gamma$	3.000
$M_{\infty}$	.500

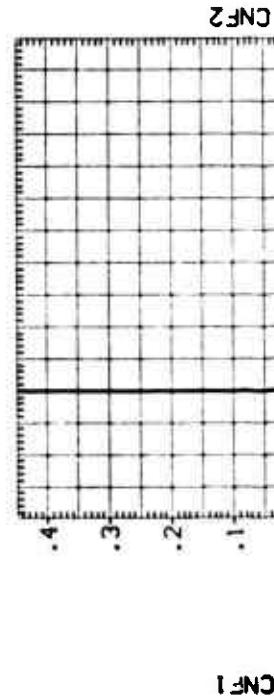
SYMBOLS

- 
- 
- ◊

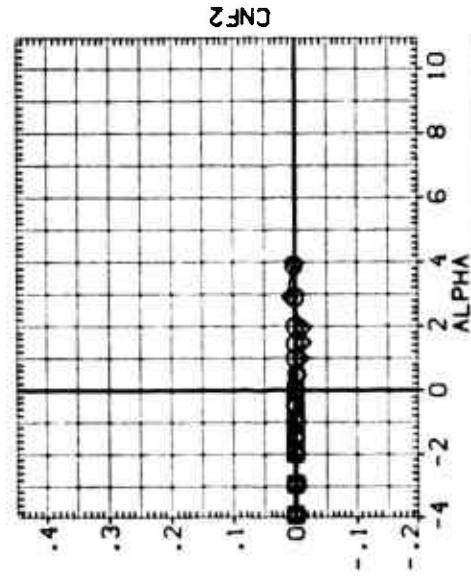
(RXE114)

REFERENCE INFORMATION  
SO. IN.

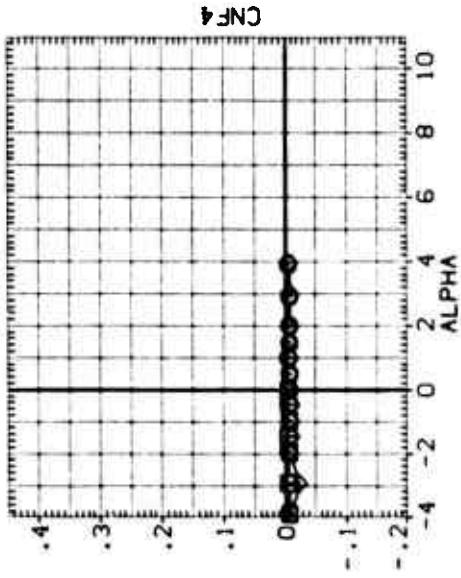
	REF
SREF	19.6350
LREF	5.0000
BREF	5.0000
XHDP	26.5000
YHDP	0.0000
ZHDP	0.0000
SCALE	-0.0000



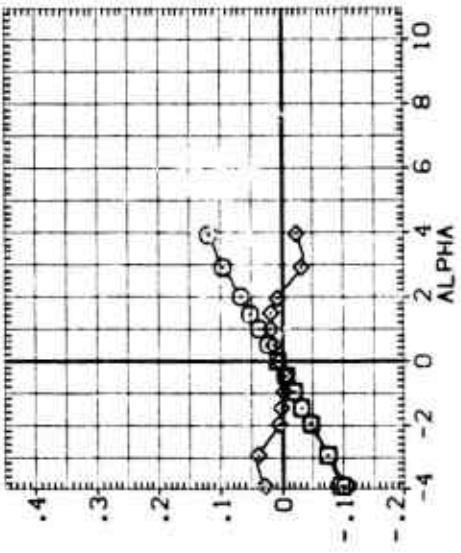
CNF1



CNF2



CNF3



CNF4

THRUST EFFECTS ON FIN NORMAL FORCE

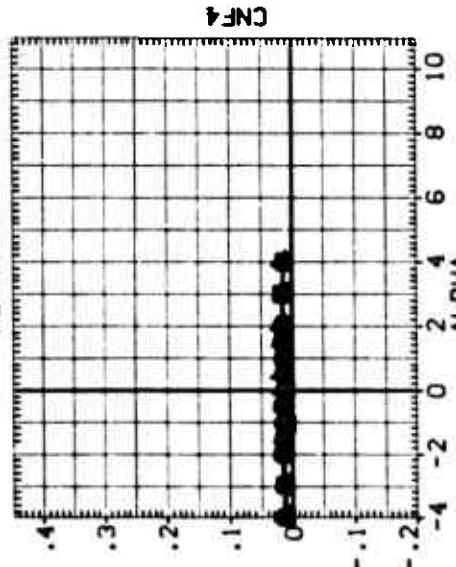
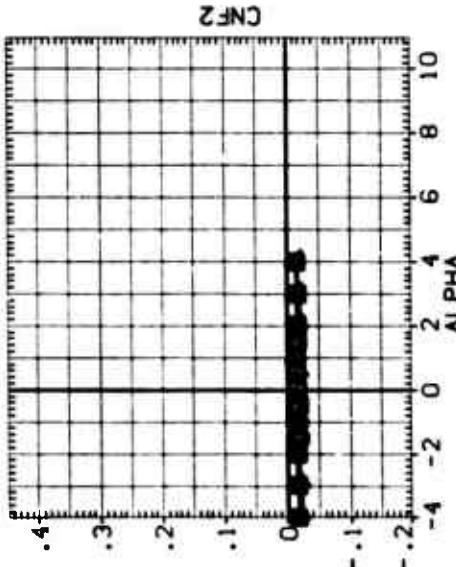
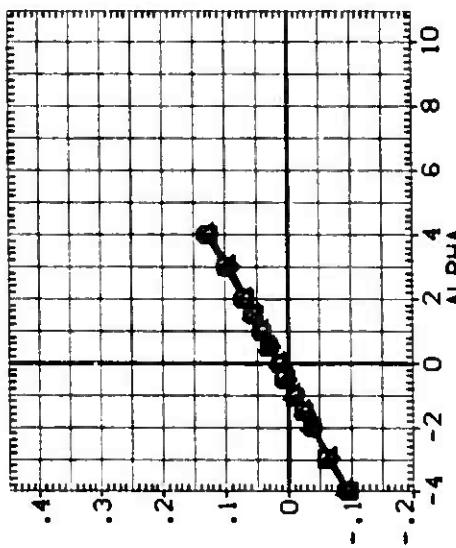
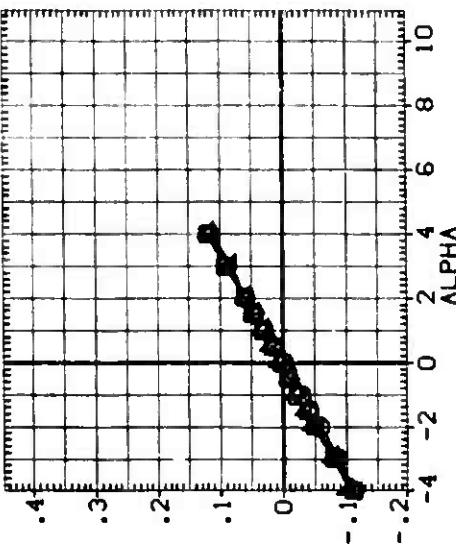
AEDC SF172 BODY FIN. BF1

PARAMETRIC VALUES			
CRF	BETA	PHI	.000
0.021	3.000	MACH	1.700
1.954	FINPOS		
3.018			
4.018			
5.959			

SYMOL: O □ ◇ △

(RXE115)

REFERENCE INFORMATION  
 SREF 19.6350 SD. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XTRP 26.5000 IN.  
 YTRP .0000 IN.  
 ZTRP .0000 IN.  
 SCALE .0000



THRUST EFFECTS ON FIN NORMAL FORCE

AEDC SF172 BODY FIN, BF1

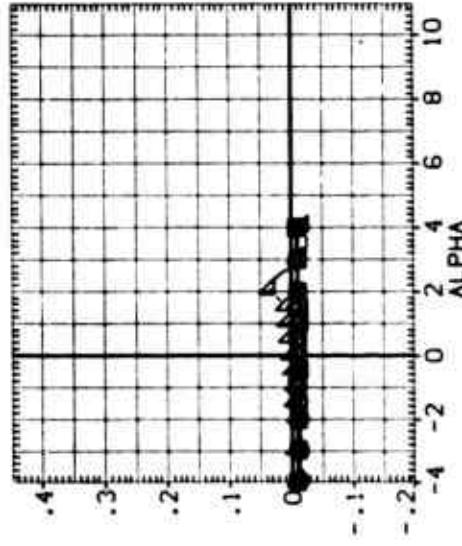
	0	PARAMETRIC VALUES
BETA	-.000	.000
FINPOS	2.011	.PHI .000
	3.989	MACH 2.000
	6.009	
	11.932	

SYMBOLS  
 O  $\square$   $\diamond$   $\triangle$   $\Delta$

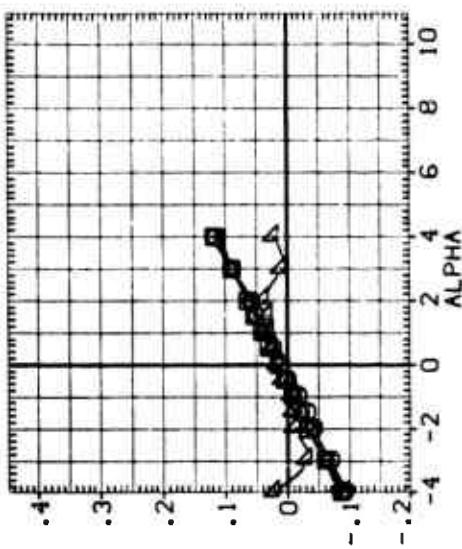
(RXE116)

REFERENCE INFORMATION  
 SREF 19.6350 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 AREF 26.5000 IN.  
 TREF .0000 IN.  
 ZREF .0000 IN.  
 SCALE .0000

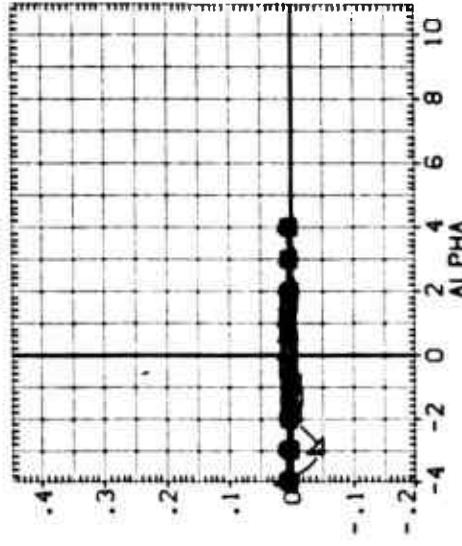
CNF2



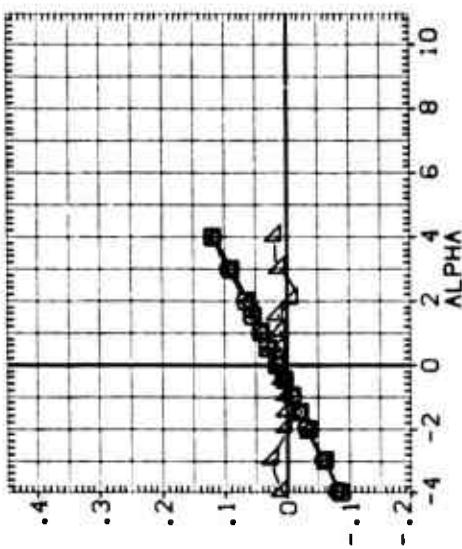
CNF1



CNF4



CNF3



THRUST EFFECTS ON FIN NORMAL FORCE

PAGE 34

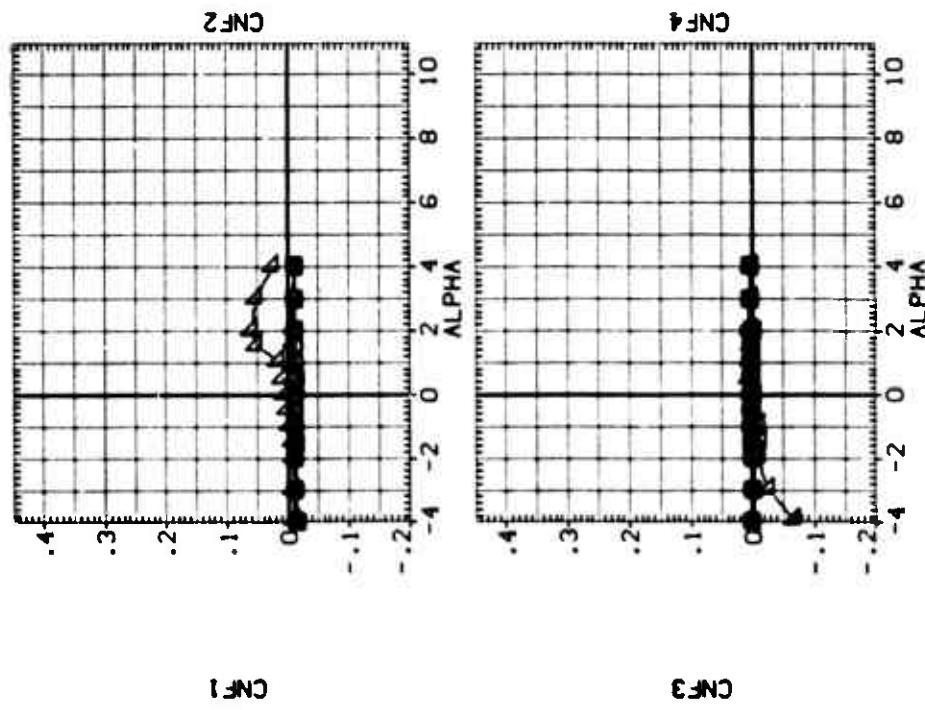
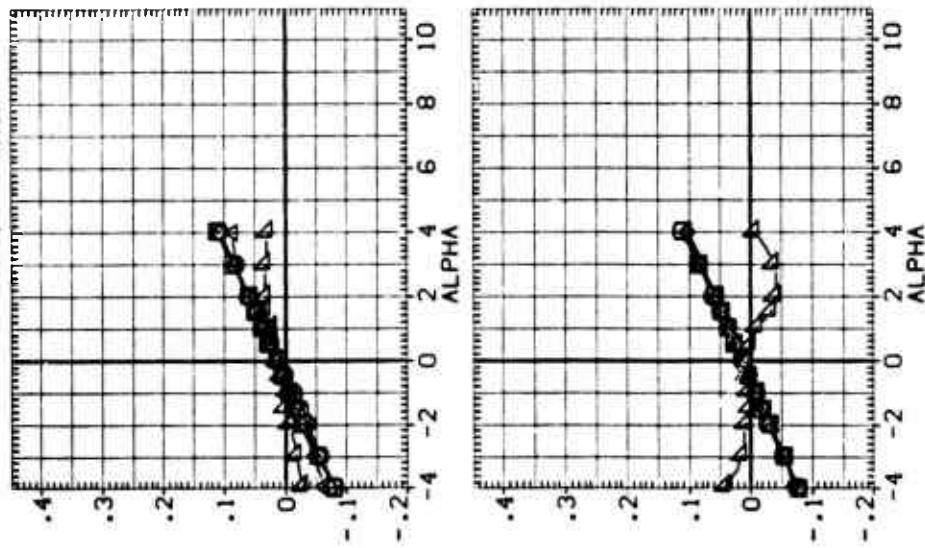
AEDC SF172 BODY FIN, BF1

	CNT	BETA	PARAMETRIC VALUES
○	.021	000	PHI .000
□	2.024	FINPOS 3.000	MACH 2.000
△	4.021		
◆	6.052		
▲	12.011		

SYMBOLOGY

(RXE117)

REFERENCE INFORMATION  
 SREF 19.6350 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XREF 26.5000 IN.  
 YREF .0000 IN.  
 ZREF .0000 IN.  
 SCALE



THRUST EFFECTS ON FIN NORMAL FORCE

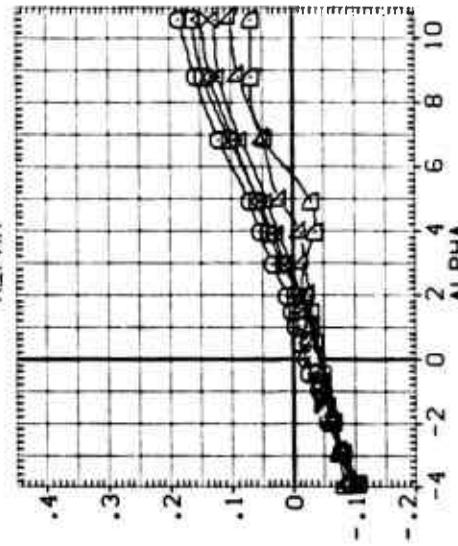
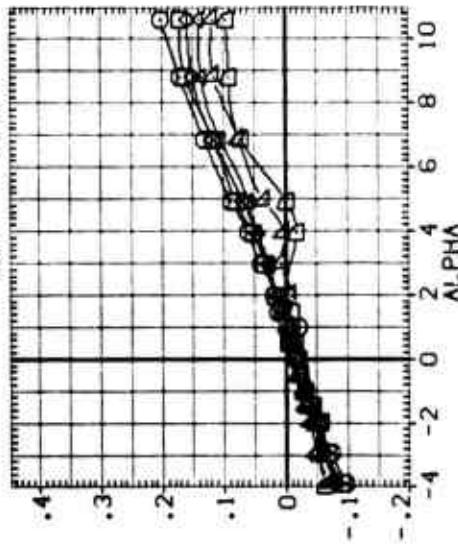
AEDC TF360 BODY FIN. BF2

	CRT	BETA	PARAMETRIC VALUES	
STRENS.	.542	.000	$\rho_{\infty}$	.000
	5.253	3.000	MACH	.200
	12.314			
	25.314			
	49.332			
	53.885			

(RXE11B)

REFERENCE INFORMATION

SREF	19.6750	SD. IN.
LREF	5.0000	IN.
BREF	5.0000	IN.
XHPP	26.5000	IN.
YHPP	.0000	IN.
ZHPP	.0000	IN.
SCALE	.0000	



THRUST EFFECTS ON FIN NORMAL FORCE

CNF2

CNF1

CNF4

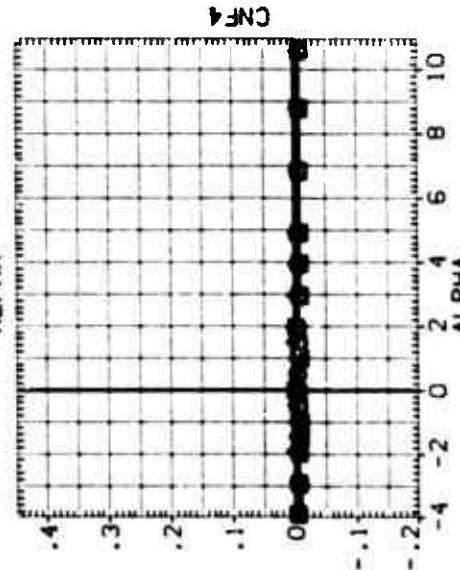
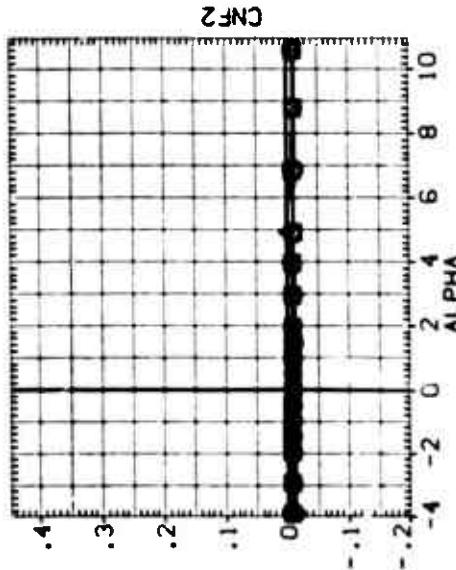
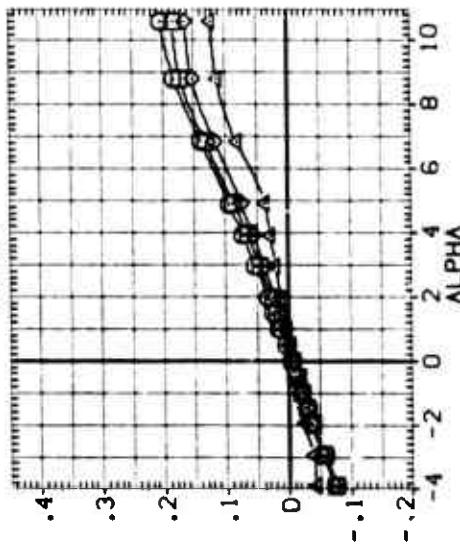
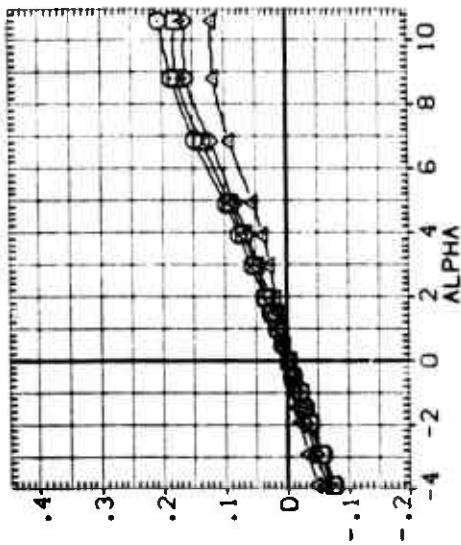
CNF3

AEDC TF360 BODY FIN, BF2

	CONST.	BETA	FINPOS	PHI	MACH
SYNTH.	.120	.000	3.000	.000	.400
□	5.713				
◊	12.135				
△	37.274				

(CXE119)

REFERENCE INFORMATION  
SREF 19.6350 SQ. IN.  
LREF 5.0000 IN.  
BREF 5.0000 IN.  
XHPP 26.5000 IN.  
YHPP .0000 IN.  
ZHPP .0000 IN.  
SCALE .0000

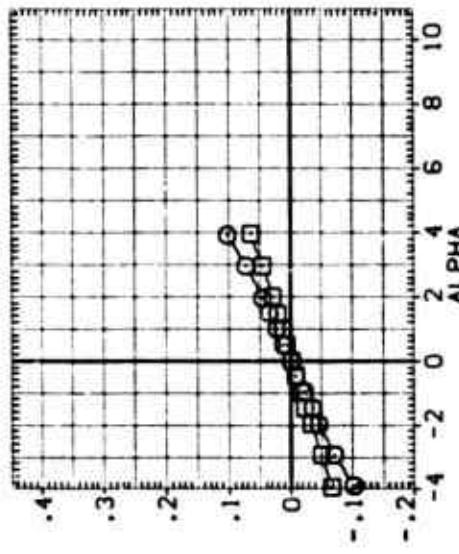
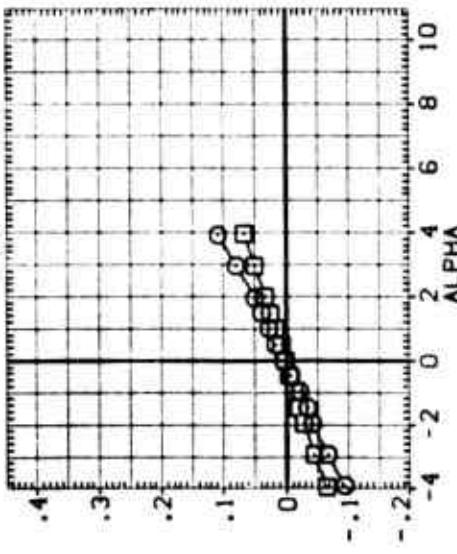


THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 800Y FIN. BF2  
 SYMBOLS: CDF .010 .000 1.000  
 PARAMETRIC VALUES: MACH 3.000 FINPOS 5.950

(RXE120)

REFERENCE INFORMATION  
 CDF 19.6350 SD. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHBP 26.5000 IN.  
 YHBP 0.0000 IN.  
 ZHBP 0.0000 IN.  
 SCALE 0.0001



CNF2

CNF1

CNF4

CNF3

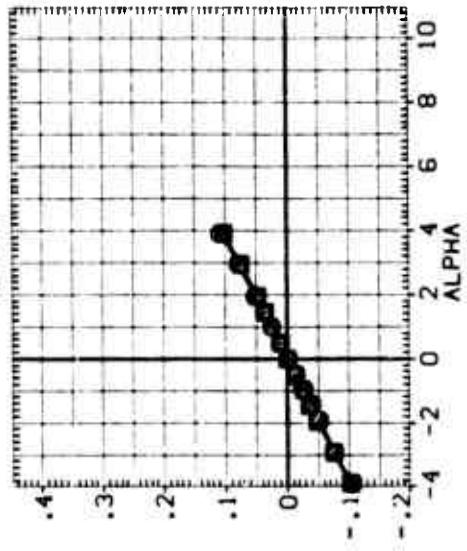
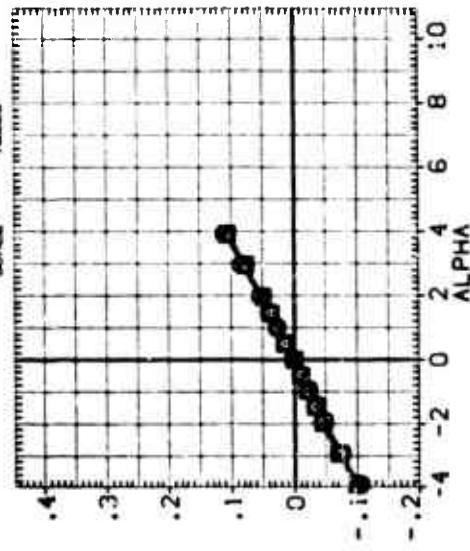
THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 BODY FIN, BF2

	PARAMETRIC VALUES
$\alpha$	.000
$\beta$	.000
$\gamma$	.000
$\delta$	.000
$\epsilon$	.000
$\phi$	.000
$\theta$	.000
$\psi$	.000
MACH	1.250

(CXE121)

REFERENCE INFORMATION  
 SREF 19.6250 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XREF 26.5000 IN.  
 YREF .0000 IN.  
 ZREF .0000 IN.  
 SCALE .0000



CNF2

CNF4

CNF1

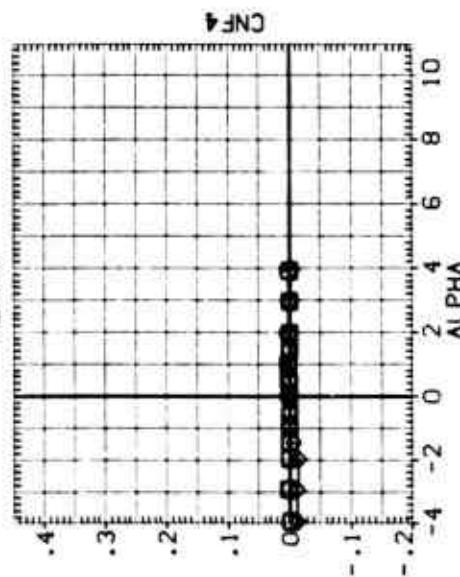
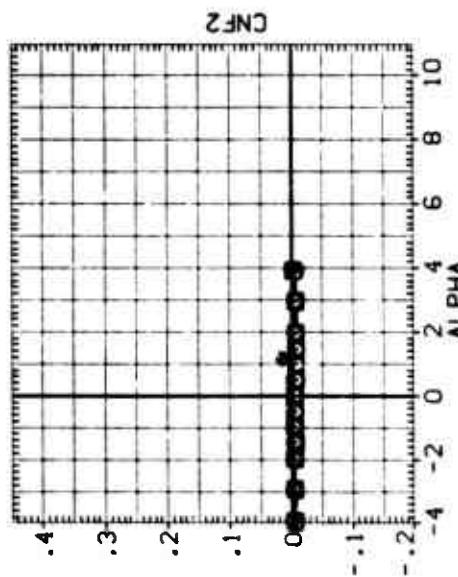
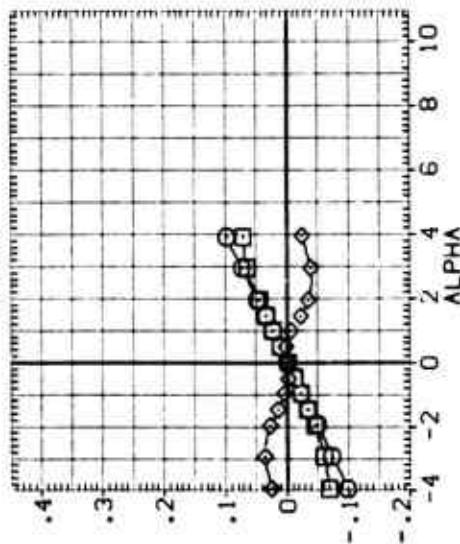
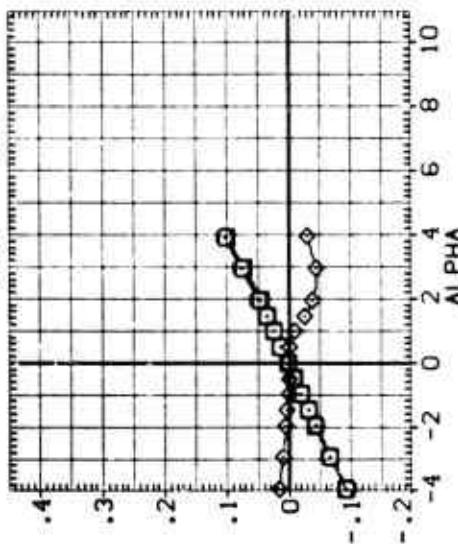
CNF3

THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 BODY FIN. BF2  
 SYMBOL CRI 4.005 BETA .000 FINPOS 3.000 MACH 1.250  
 6.010 11.905

(CXE121)

REFERENCE INFORMATION  
 SREF 19.6750 SD. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XTRP 26.5000 IN.  
 YTRP .0000 IN.  
 ZTRP .0000 IN.  
 SF ALE .0000



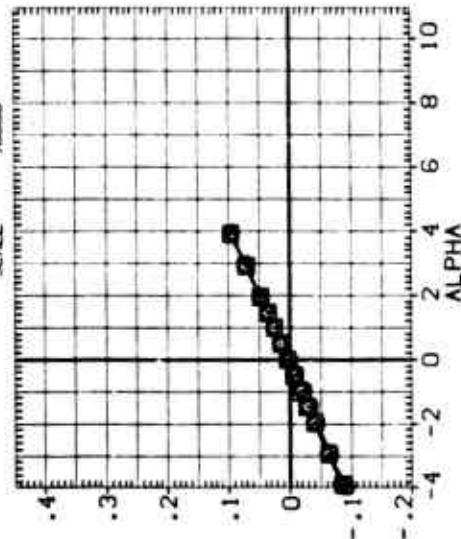
THRUST EFFECTS ON FIN NORMAL FORCE

AEDC TF360 BODY FIN, BF2

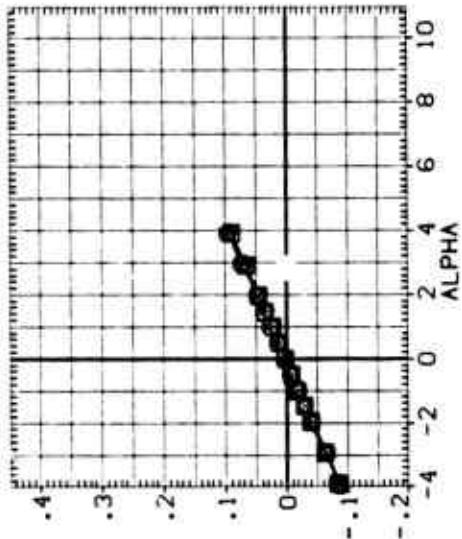
Symbol	DRY	BETA	PARAMETRIC VALUES	
O	.010	.000	$\phi_{\text{N}}$	.000
□	.989	.000	MACH	.500
△	2.008	.000		
△	3.060	.000		

(RXE122)

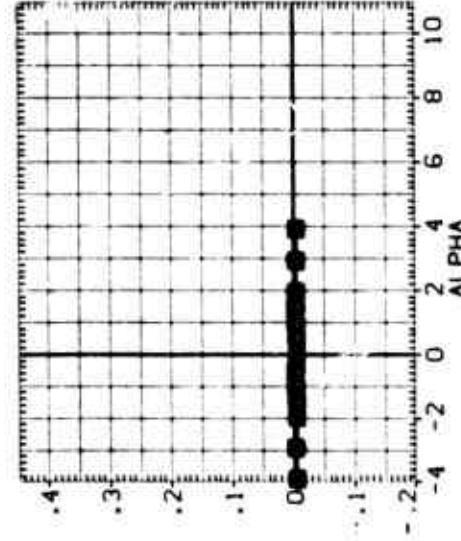
REFERENCE INFORMATION  
 SHEF 19.6350 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHBP 26.5000 IN.  
 YHBP .0000 IN.  
 ZHBP .0000 IN.  
 SCALE .00000



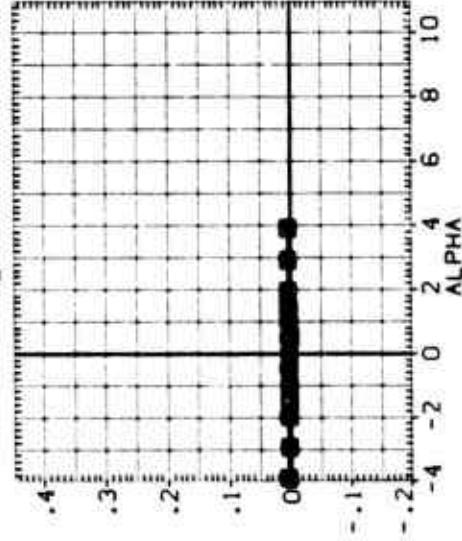
CNF1



CNF2



CNF3



CNF4

THRUST EFFECTS ON FIN NORMAL FORCE

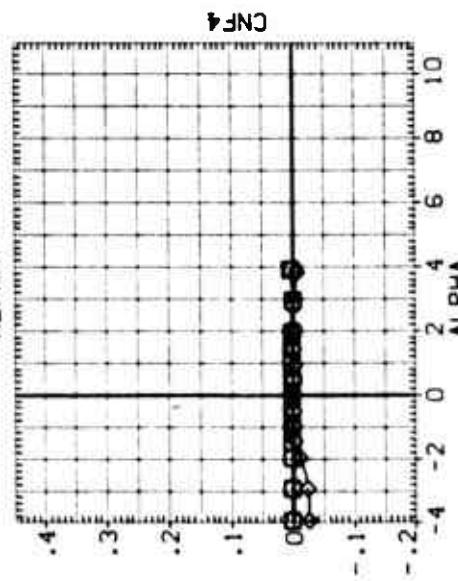
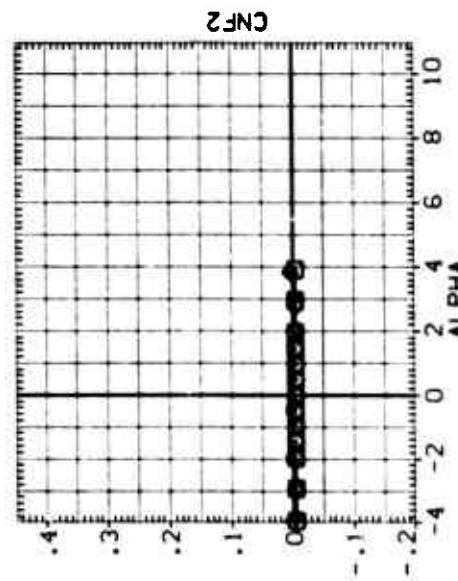
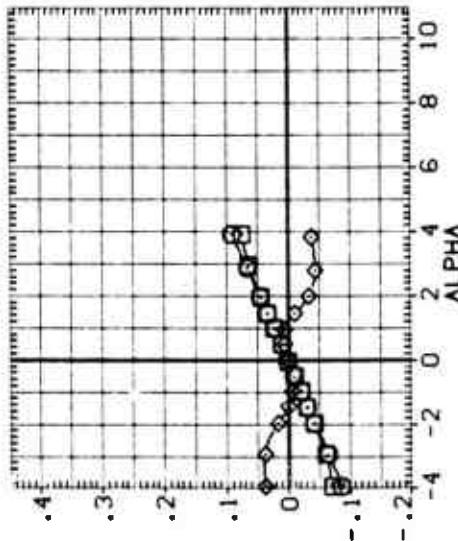
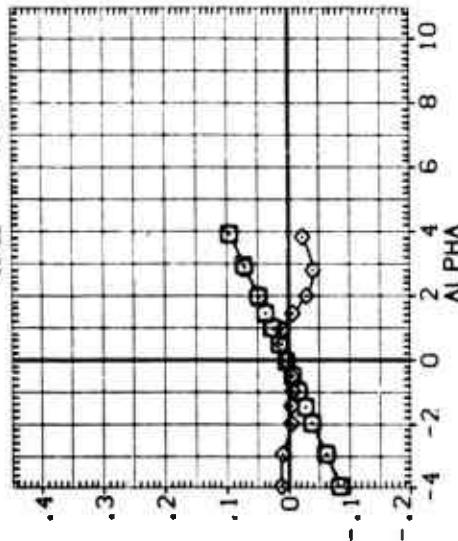
AEOC TF360 BODY FIN, BF2

Sym.	CRT	BETA	PARAMETRIC VALUES
○	.000	.000	PHI .000
□	5.988	FINPOS 3.000	MACH 1.500
◊	11.951		

(RXE122)

REFERENCE INFORMATION

SREF	19.6350	50. IN.
LREF	5.0000	IN.
BREF	5.0000	IN.
XHSP	26.5000	IN.
YHSP	.0000	IN.
ZHSP	.0000	IN.
SCALE	.0000	



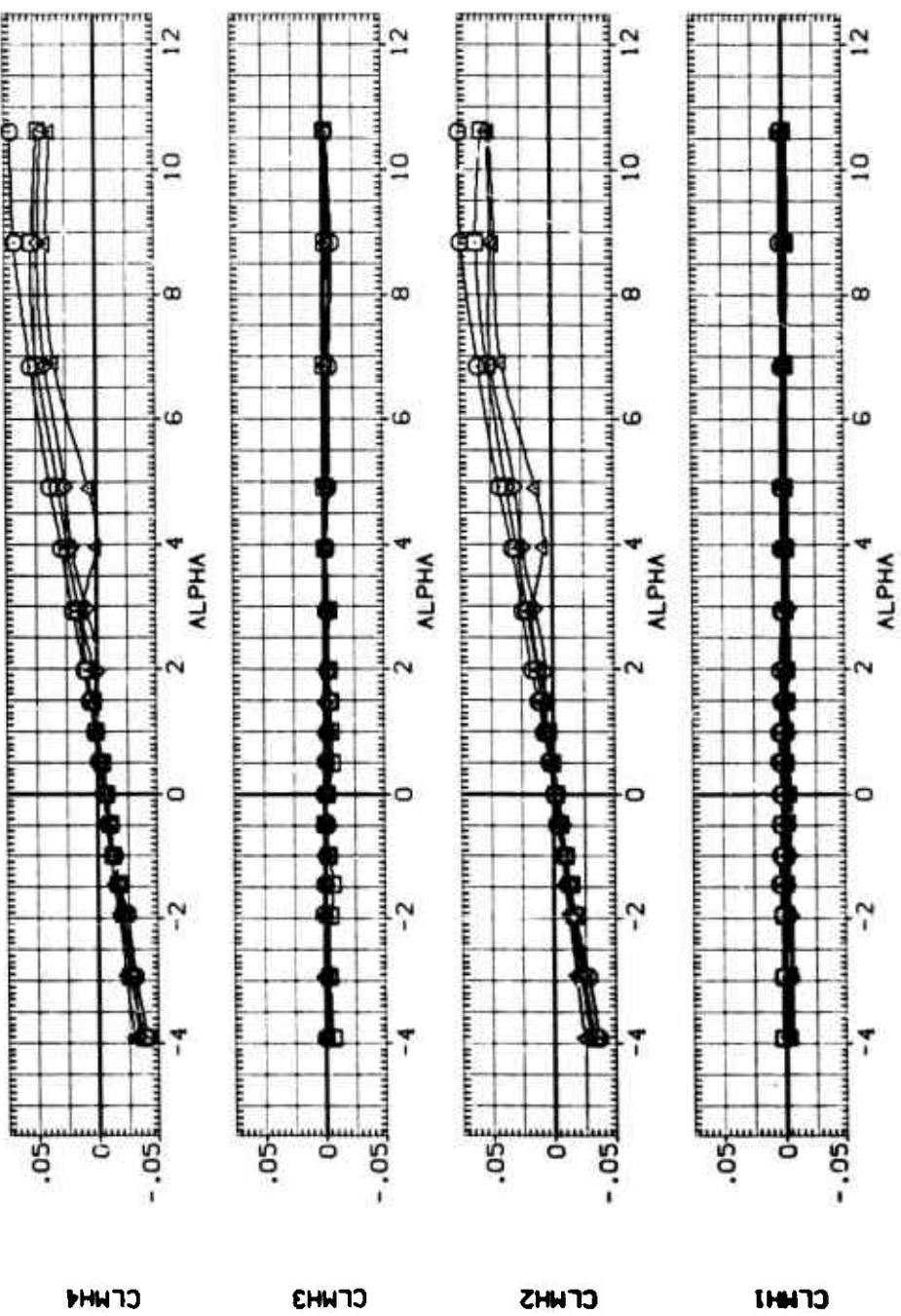
THRUST EFFECTS ON FIN NORMAL FORCE

PAGE 42

AEDC TF360 BODY FIN, BF1  
 SYMBOL CRT .575 BETA .000 PHI .000  
 O 26.074 FINPOS 3.000 MACH .200  
 □ 50.139  
 ▲ 100.918

(RXE209)

PARAMETRIC VALUES  
 REFERENCE INFORMATION  
 SEEF 19.5250 50.1N.  
 LINEF 5.0000 N.  
 BREF 5.0000 N.  
 XHFP 26.5000 N.  
 YHFP .0000 N.  
 ZHFP .0000 N.  
 SCALE .00000

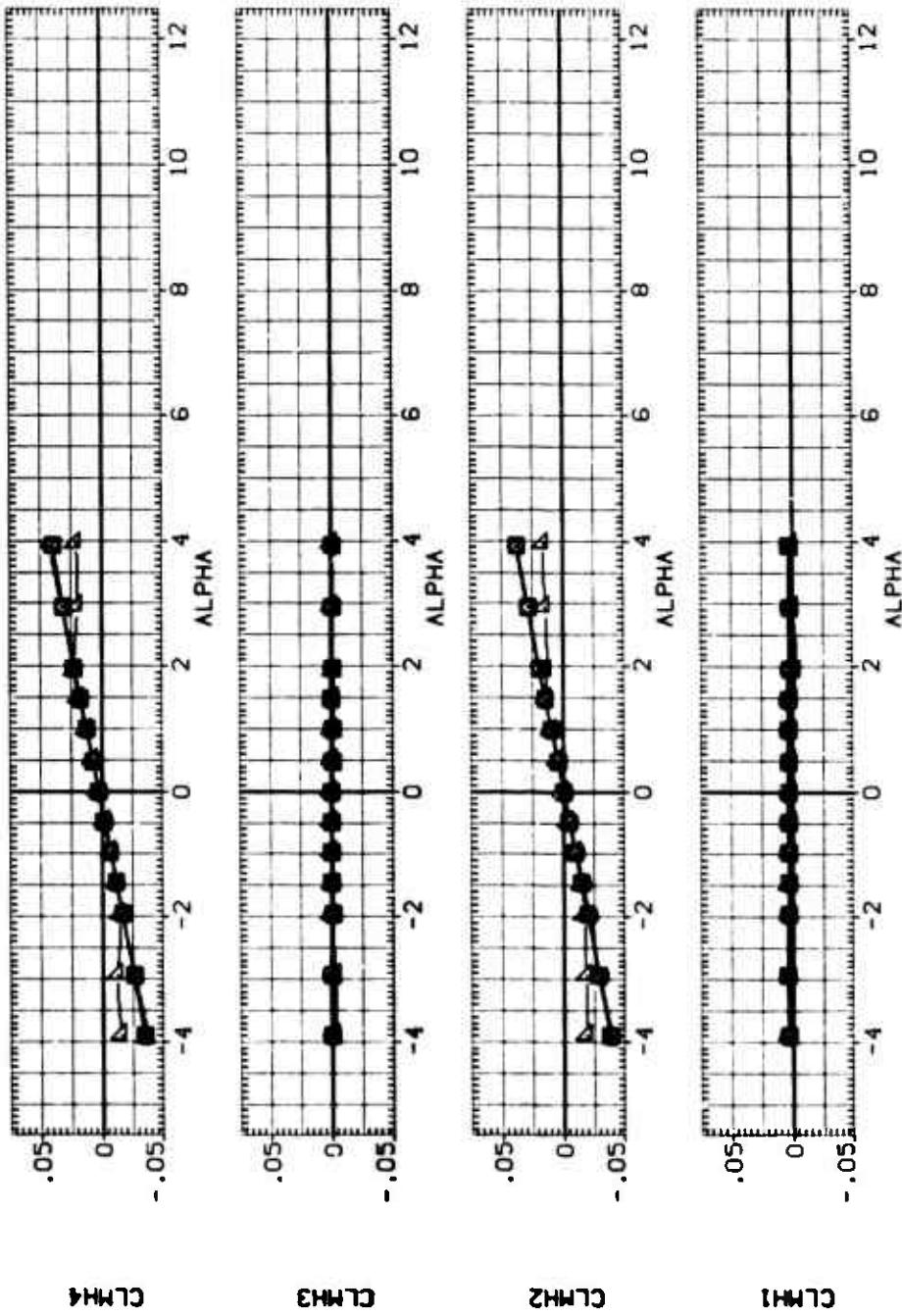


TYPICAL THRUST EFFECT ON FIN HINGE MOMENT

AEDC TF360 BODY FIN. BF1  
 smma. CNT. 010 042 014 006 926  
 .010 0.000 3.000 4.014 6.006 11.926  
 □○△△△

(RXE213)

PARAMETRIC VALUES  
 CNT. 010 042 014 006 926  
 .010 0.000 3.000 4.014 6.006 11.926  
 □○△△△  
 REFERENCE INFORMATION  
 SREF 19.6250 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 26.5000 IN.  
 XHPP .0000 IN.  
 YHPP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000

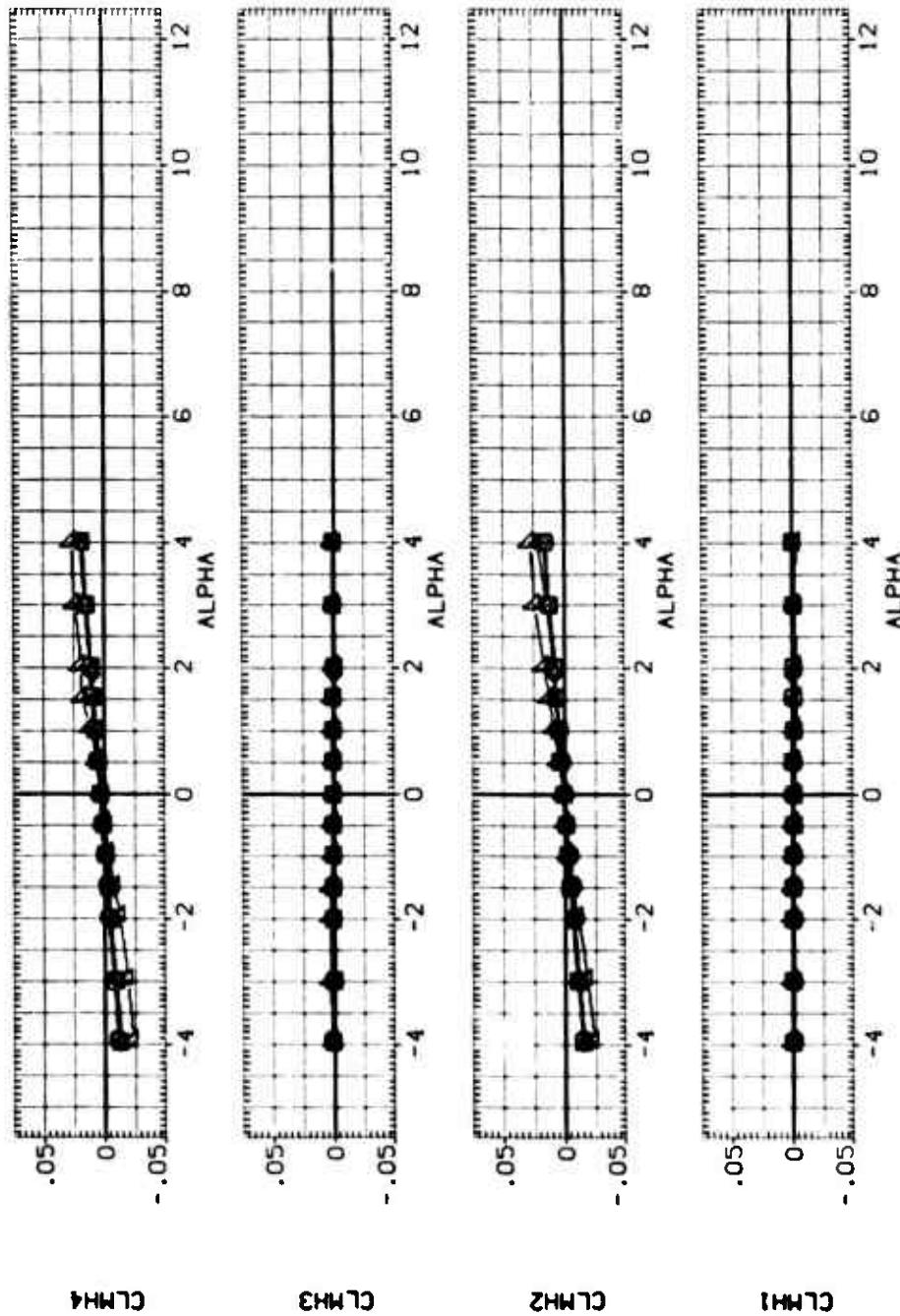


TYPICAL THRUST EFFECT ON FIN HINGE MOMENT

AEDC SF172 BODY FIN. BF1  
 SPHERICAL  
 CDT .000     $\text{BETA}$  .000     $\text{PHI}$  .000  
 2.011    FINPOS 3.000    MACH 2.000  
 3.969  
 6.009  
 11.932

(RXE216)

PARAMETRIC VALUES  
 REFERENCE INFORMATION  
 SREF 19.6350 SQ. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 YHPP .0000 IN.  
 ZHPP .0000 IN.  
 SCALE .0000



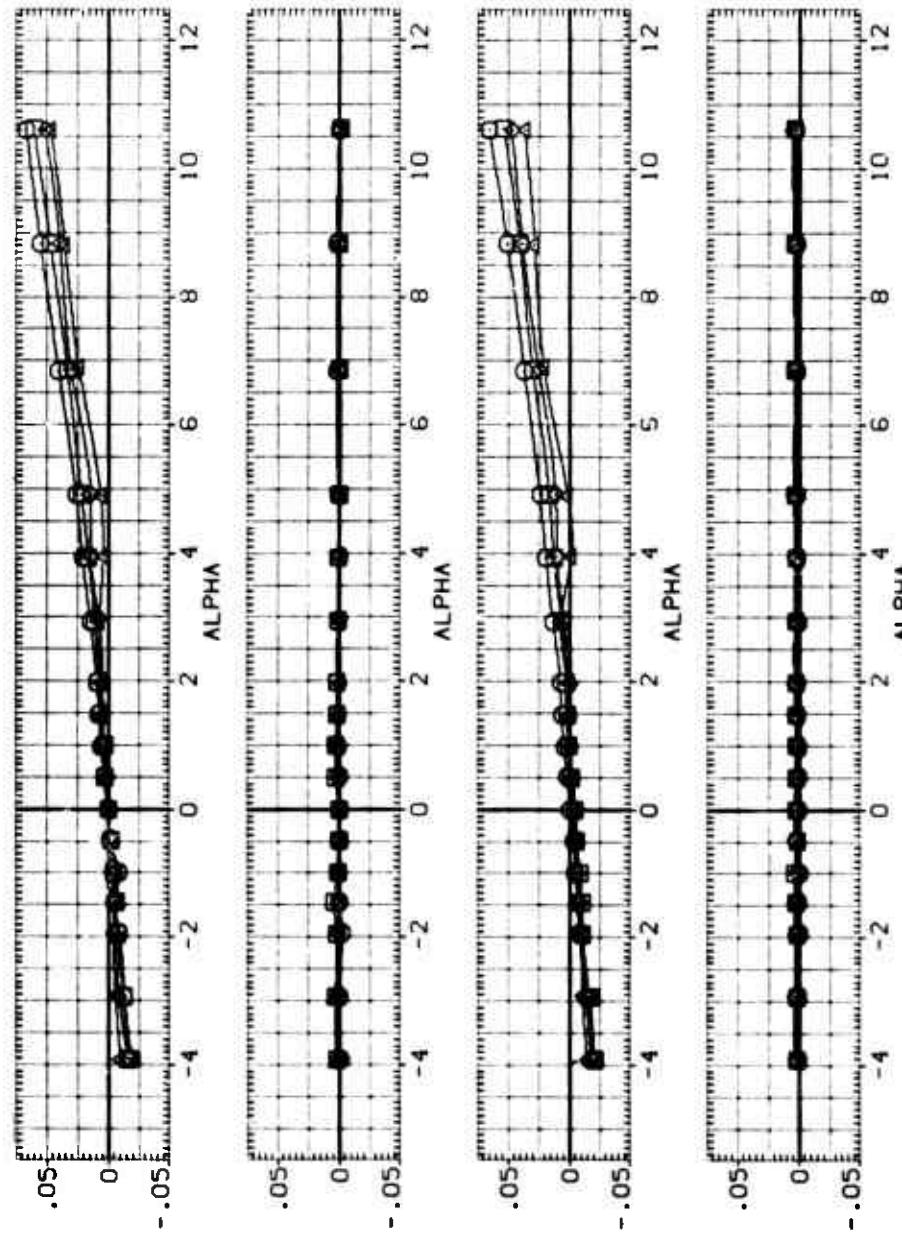
TYPICAL THRUST EFFECT ON FIN HINGE MOMENT

AEOC TR 360 BODY FIN, BF1

SYMBOL	CRT	BETA	PARAMETRIC VALUES
O	.575	.000	PHI .000
□	26.074	.000	MACH .200
◇	50.139		
△	100.918		

(RXE209)

REFERENCE INFORMATION  
 SREF 19.6350 50. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XMRP 26.5000 IN.  
 YMRP .0000 IN.  
 ZMRP .0000 IN.  
 SCALE .0000

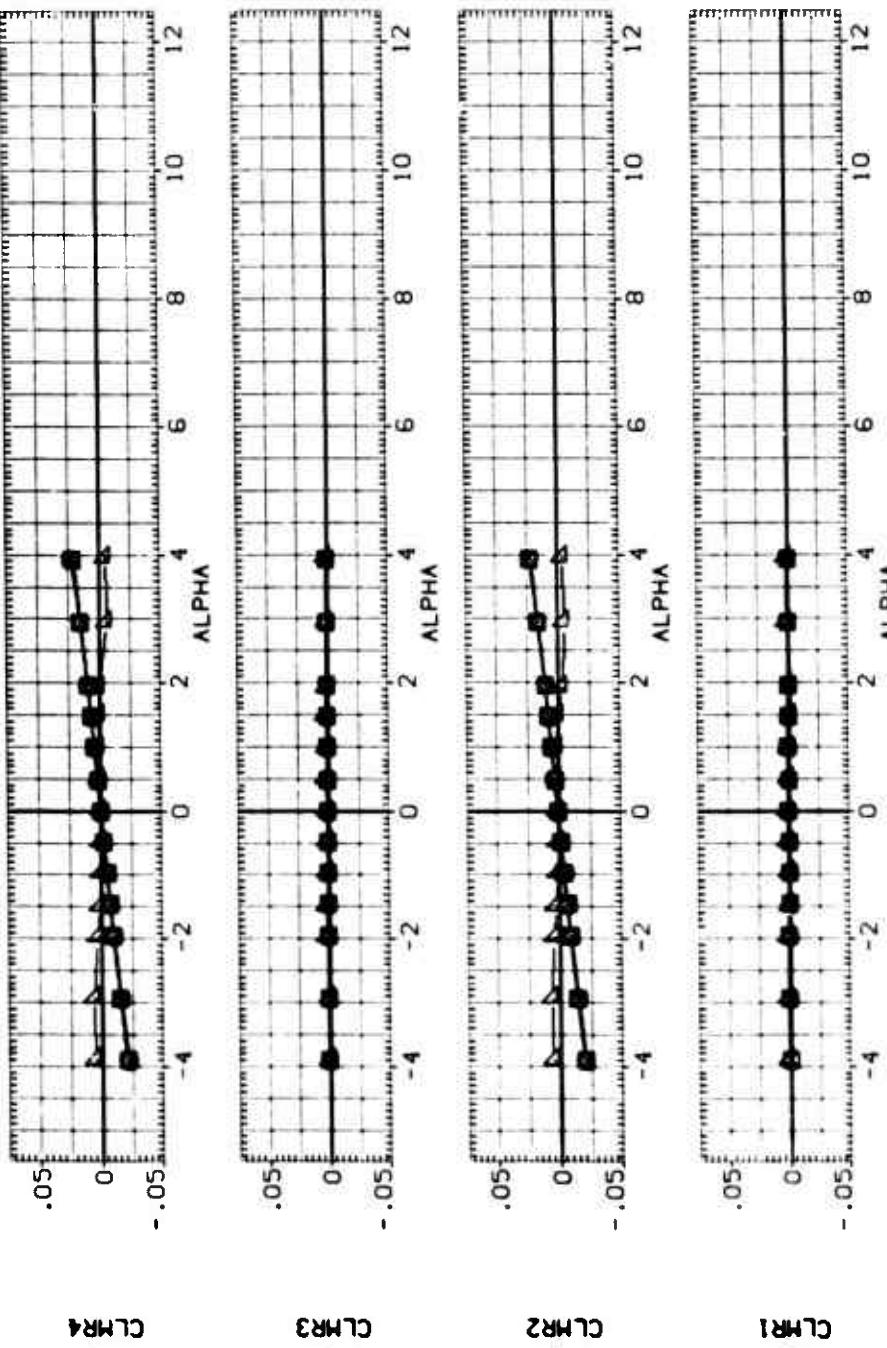


TYPICAL THRUST EFFECT ON FIN ROOT BENDING MOMENT

AEDC TF360 BODY FIN. BF1  
 PARAMETRIC VALUES  
 CRT .010 BETA .000 PHI .000  
 3.042 FINPOS 3.000 MACH 1.250  
 4.014  
 6.006  
 11.926

REFERENCE INFORMATION  
 SQ. IN.  
 LREF 19.6250  
 SREF 5.0000  
 BREF 5.0000  
 XMRP 26.5000  
 YMRP 0.0000  
 ZMRP 0.0000  
 SCALE .0000

(RXE213)

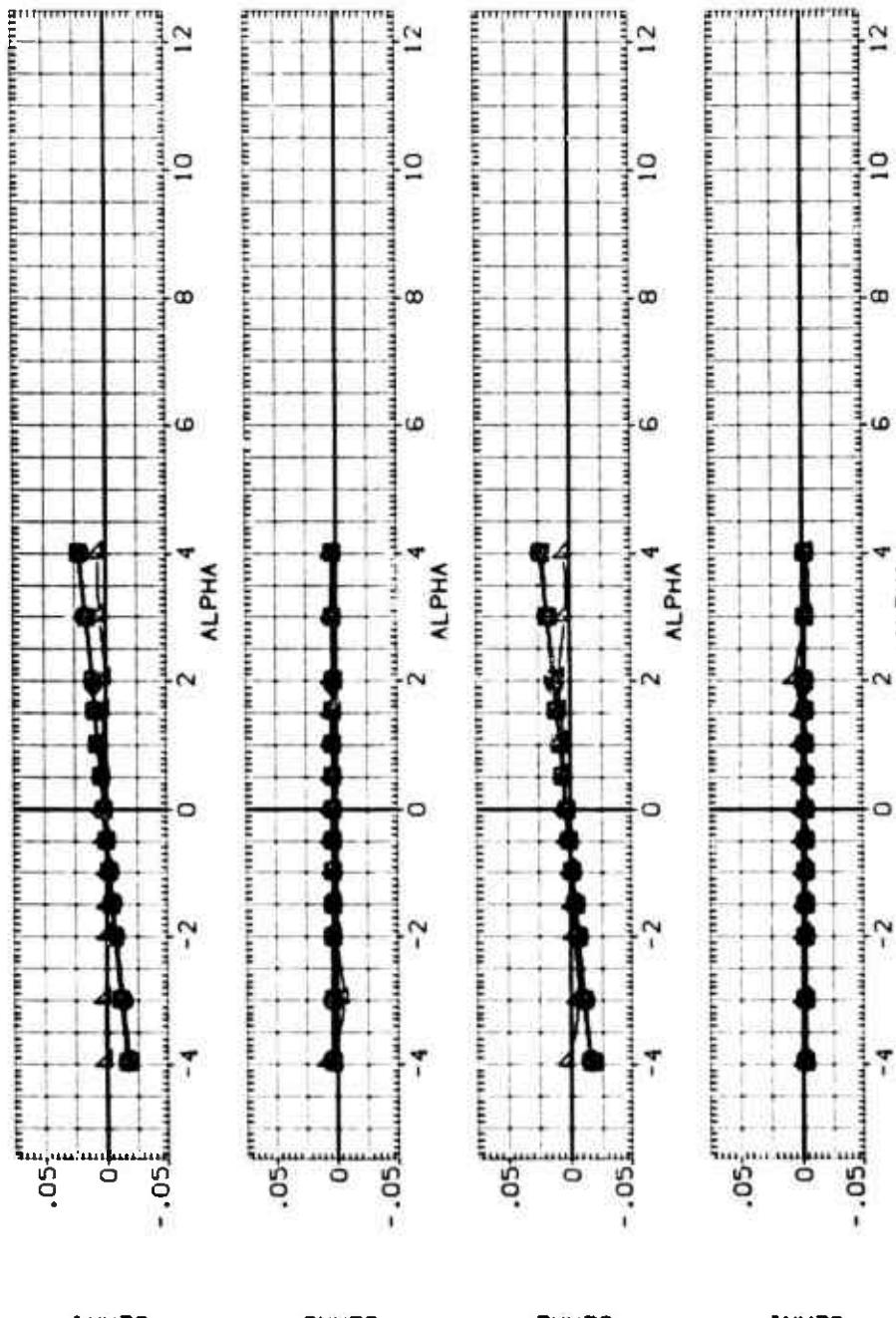


TYPICAL THRUST EFFECT ON FIN ROOT BENDING MOMENT

AEDC SF172 BODY FIN. BF1  
 SYMBOL CPT PARAMETRIC VALUES  
 - .000 BE $\alpha$  .000 PH $\alpha$  .000  
 2.011 FINPOS 3.000 MACH 2.000  
 3.969  
 6.009  
 11.932

(RXE216)

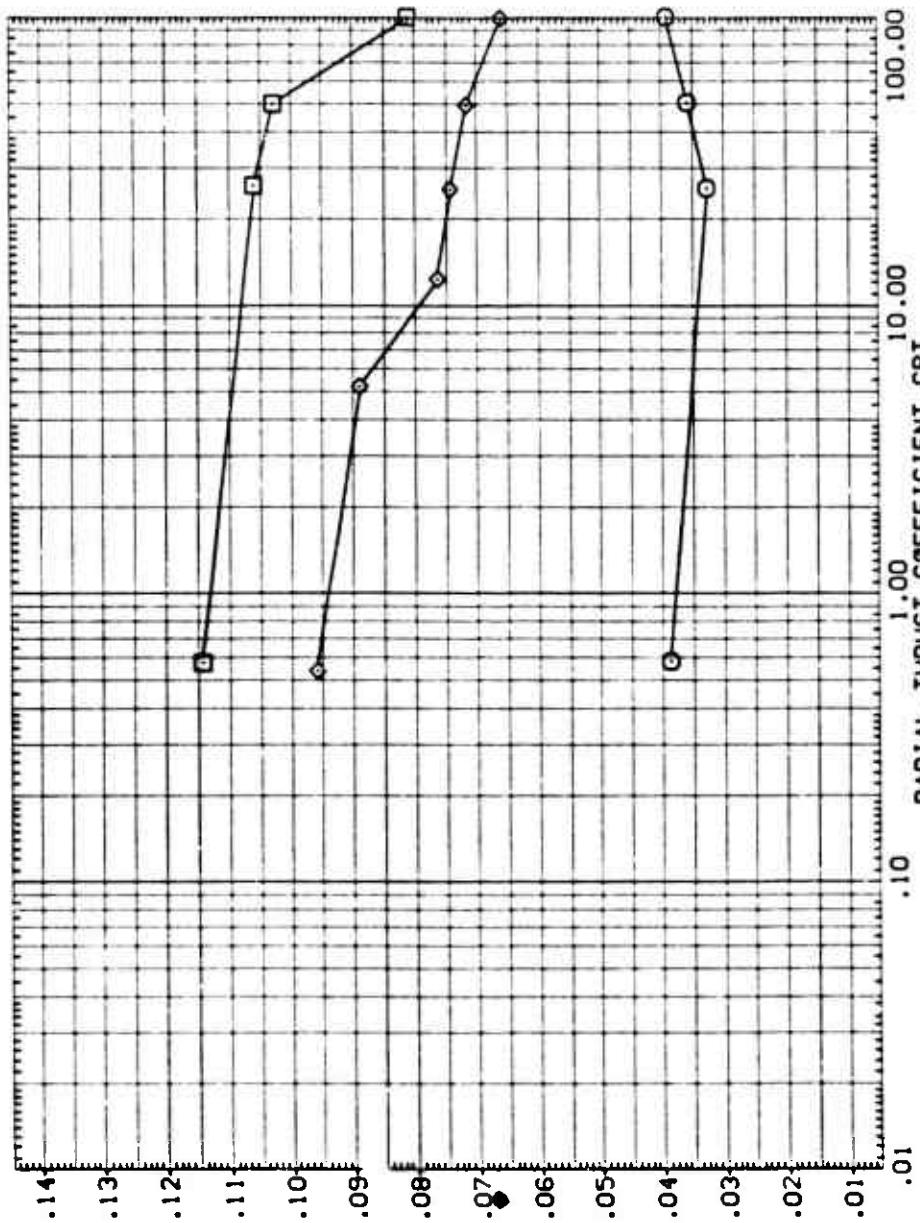
REFERENCE INFORMATION  
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 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XHSP 26.5000 IN.  
 YHSP .0000 IN.  
 ZHSP .0000 IN.  
 SCALE .0000



TYPICAL THRUST EFFECT ON FIN ROOT BENDING MOMENT

DATA SET SYMBOL CONFIGURATION DESCRIPTION  
 (R2E000) ASEC TF360 BODY ALONE B  
 (R2E001) ASEC TF360 BODY FIN. B#1  
 (R2E002) ASEC TF360 BODY FIN. B#2

REFERENCE INFORMATION  
 BETA .000 PHI .000 FINPOS 3.000 MACH .200 SREF 19.6750 SD. IN.  
 .000 .000 3.000 .200 LREF 5.0000 IN.  
 .000 .000 .200 BREF 5.0000 IN.  
 .000 .000 XREF 26.5000 IN.  
 .000 .000 YREF 0.0000 IN.  
 .000 .000 ZREF 0.0000 IN.  
 .000 .000 SCALE -.0000

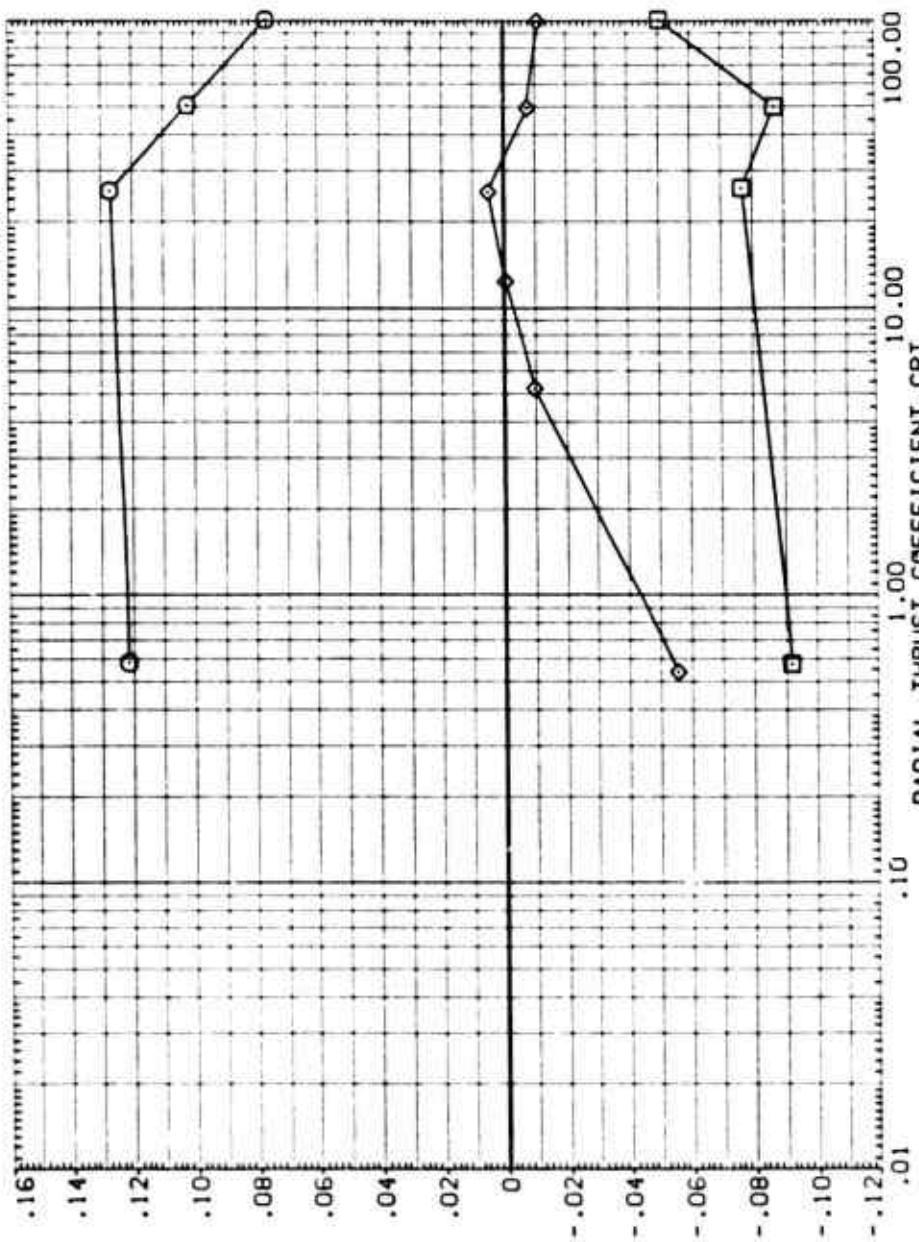


NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHAB, CNALFA, PER DEGREE

EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL CONFIGURATION DESCRIPTION  
 (R0E0007) AEDC BODY ALONE, B  
 (R0E0008) AEDC TF 360 BODY FIN, SF1  
 (R0E0009) AEDC TF 360 BODY FIN, SF2

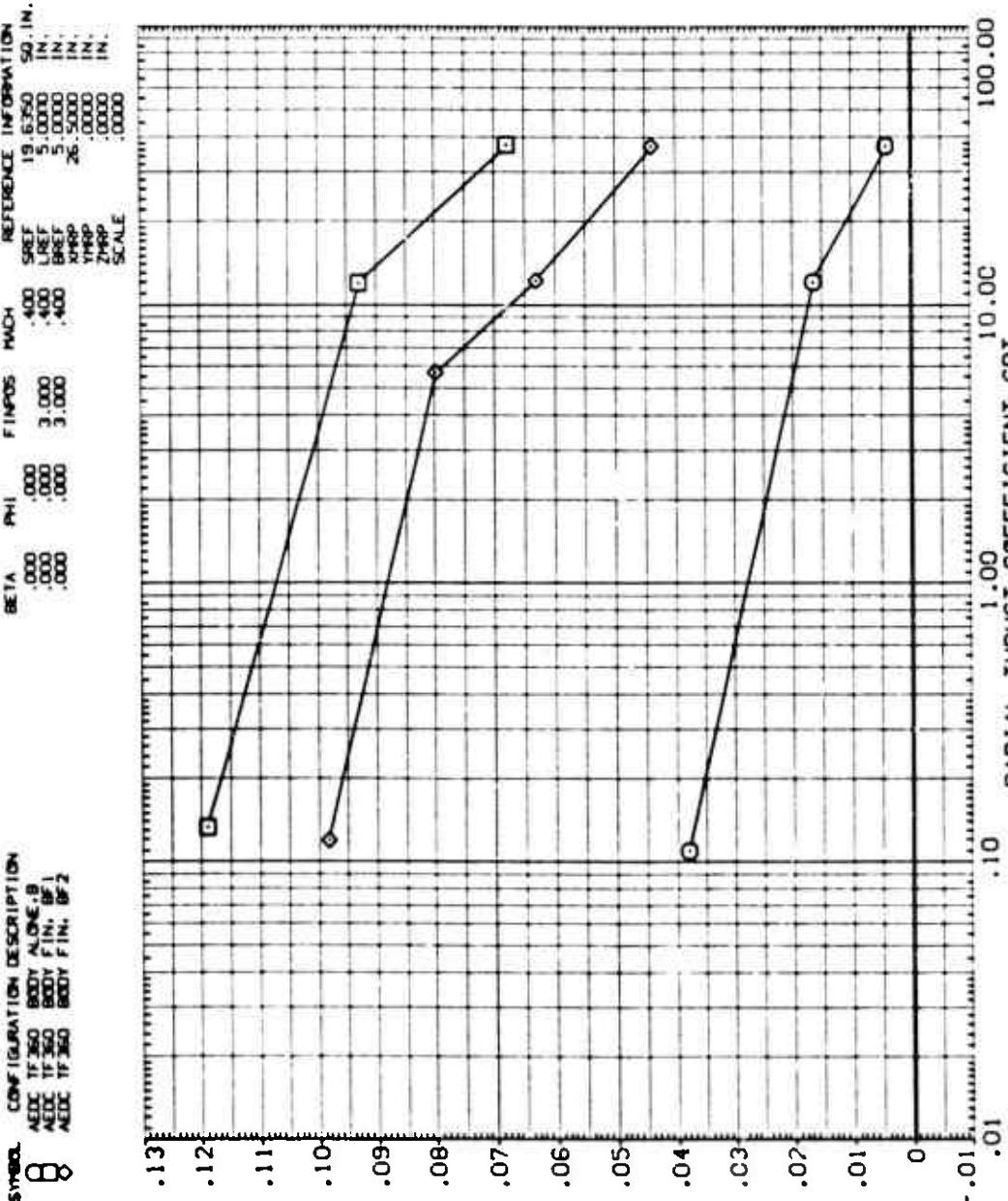
BETA PHI FINPOS MACH REFERENCE INFORMATION  
 .000 .000 3.000 .200 SREF 19.6350 SO, IN.  
 .000 .000 3.000 .200 LREF 5.0000 IN.  
 .000 .000 3.000 .200 SREF 5.0000 IN.  
 .000 .000 3.000 .200 XREF 26.5000 IN.  
 .000 .000 3.000 .200 YREF .0000 IN.  
 .000 .000 3.000 .200 ZREF .0000 IN.  
 SCALE .0000



PITCHING MOMENT COEFFICIENT DERIVATIVE WITH ALPHAB, CLM, L, F, PER DEGREE

### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL: 8  
 CONFIGURATION DESCRIPTION:  
 (CASE001) AEDC TF 350 BODY ALONE, B  
 (CASE011) AEDC TF 350 BODY FIN, BF1  
 (CASE019) AEDC TF 350 BODY FIN, BF2



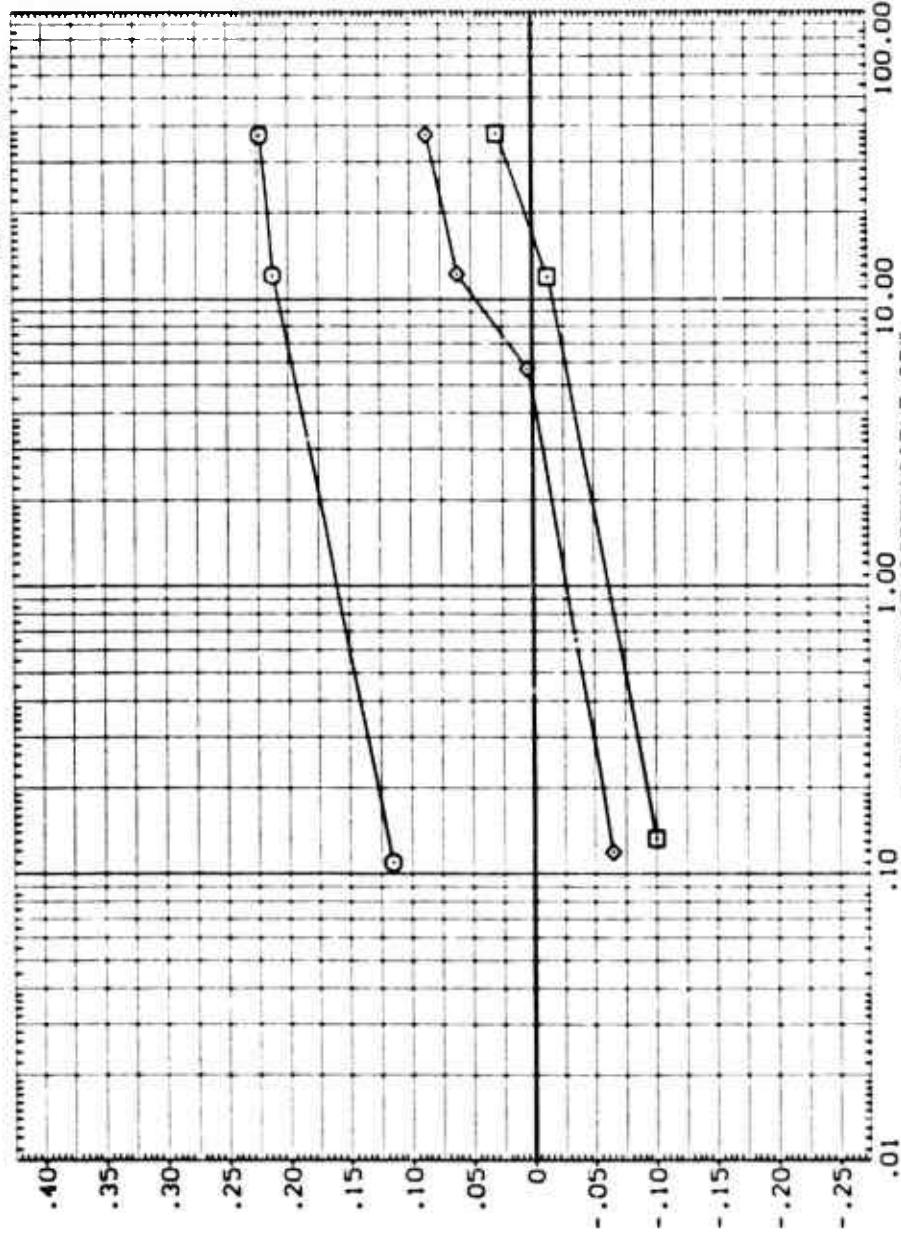
NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHABETIC, CNALFA, PER DEGREE

### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

PITCHING MOMENT COEFFICIENT DERIVATIVE WITH ALPHAS, CLMALS, PER DEGREE

DATA SET STREAM  
 CONFIGURATION DESCRIPTION  
 (A)ELE TF 360 BODY ALONE.  
 (B)ELE TF 360 BODY FIN. 8F-1  
 (C)ELE TF 360 BODY FIN. 8F-2  
 (D)ELE TF 360 BODY FIN. 8F-3

REFERENCE INFORMATION  
 MACH .400 SRREF 19.6350 SQ. IN.  
 MACH .400 LRREF 5.0000 IN.  
 MACH .400 BRREF 5.0000 IN.  
 XHPP 26.5000 IN.  
 THPP 0.0000 IN.  
 ZHPP 0.0000 IN.  
 SCALE .0000

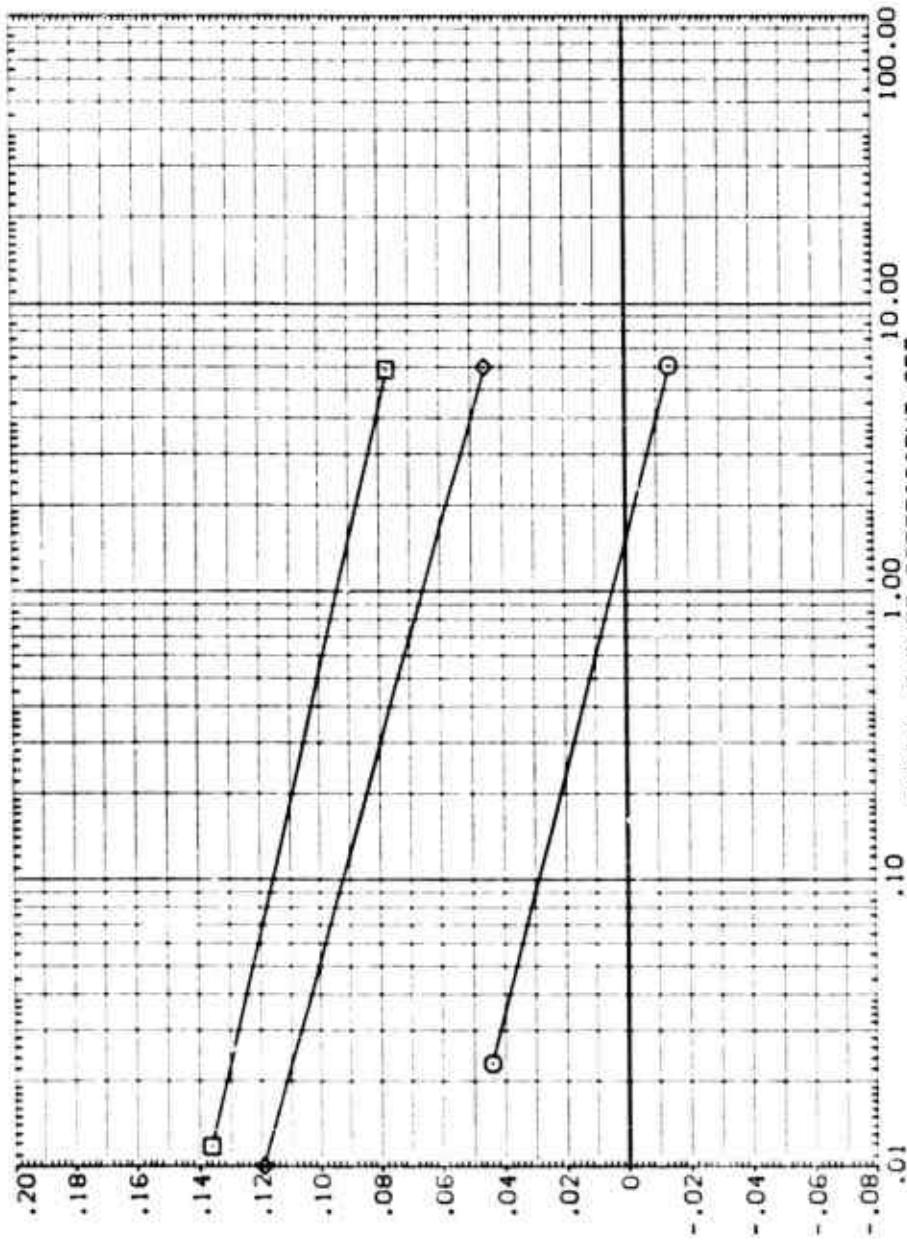


### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL CONFIGURATION DESCRIPTION

RHED04	AELC TF 360 BODY ALONE, B
RHED12	AELC TF 360 BODY FIN, BP <sub>1</sub>
RHED20	AELC TF 360 BODY FIN, BP <sub>2</sub>

BETA PHI FINPOS MACH REFERENCE INFORMATION  
 .000 .000 1.000 SOFT 19.6750 50. IN.  
 .000 .000 3.000 1.000 LBDF 5.0000 IN.  
 .000 .000 3.000 1.000 BDF 5.0000 IN.  
 .000 .000 26.5000 IN.  
 THDP .000000 IN.  
 ZHDP .000000 IN.  
 SCALE .0000



NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHA, CNLFA, PER DEGREE

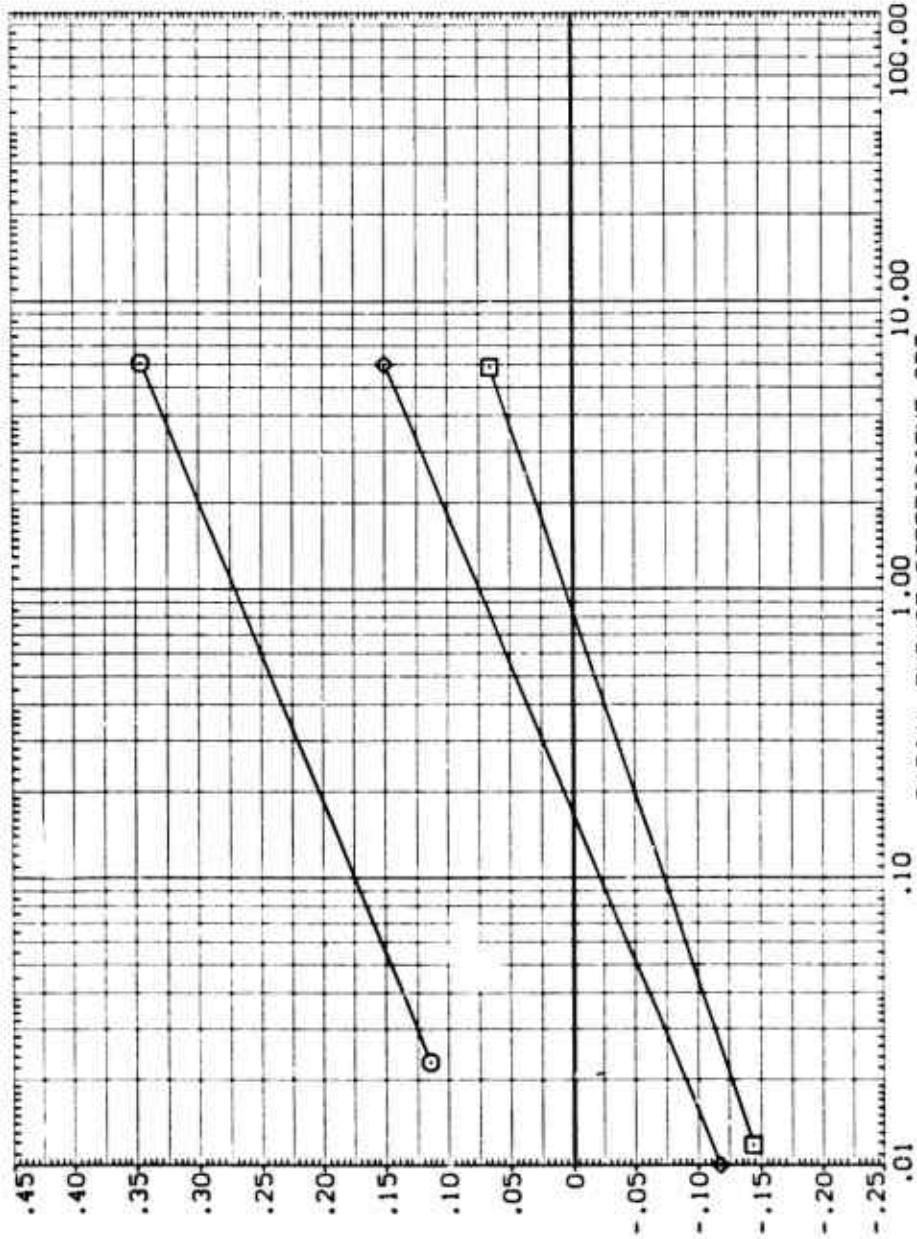
EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

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PITCHING MOMENT COEFFICIENT DERIVATIVE WITH ALPHAS, CLHALF, PER DEGREE

DATA SET SYMBOL CONFIGURATION DESCRIPTION  
 (ROE004) AEDC TF 360 BODY ALONE, B  
 (ROE012) AEDC TF 360 BODY FIN, BF<sub>1</sub>  
 (ROE020) AEDC TF 360 BODY FIN, BF<sub>2</sub>

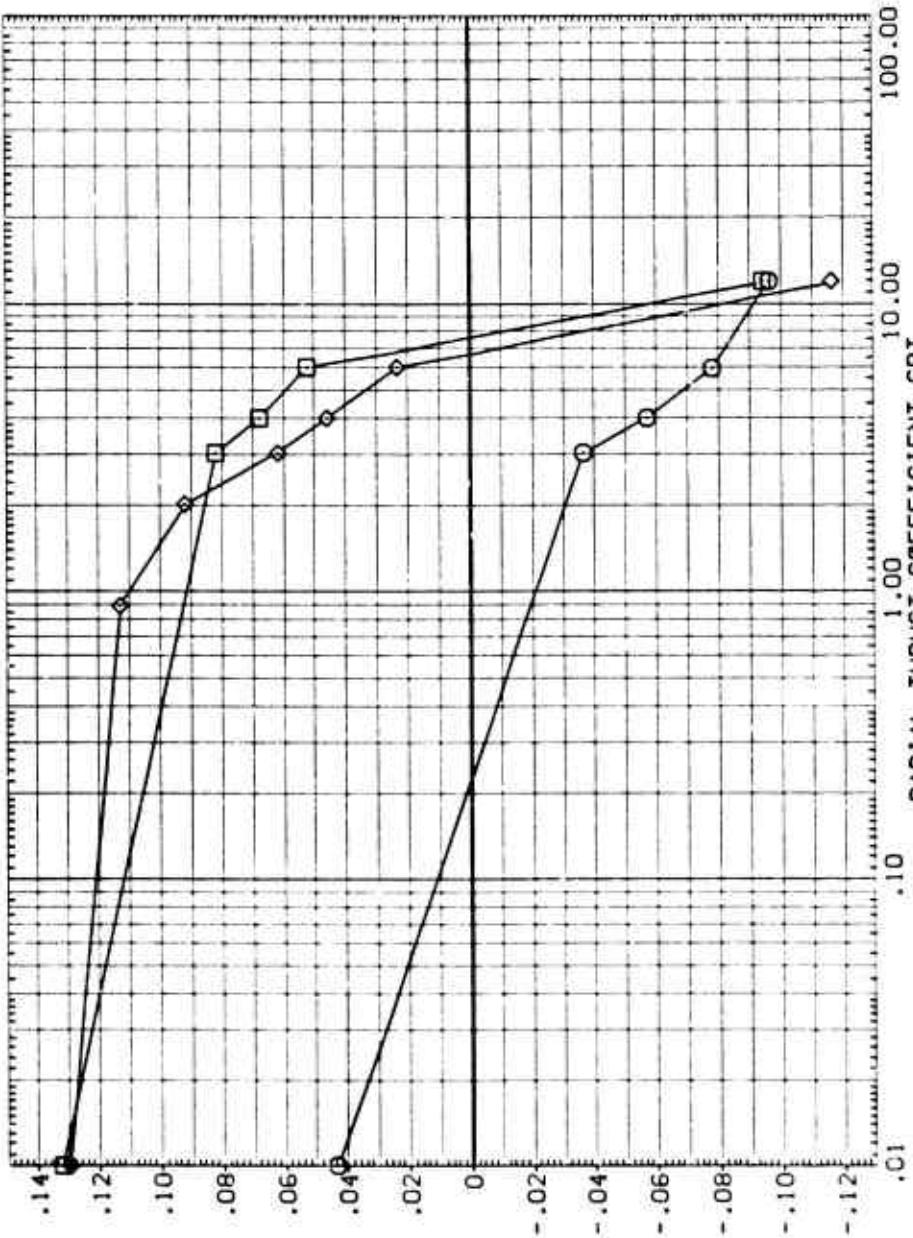
REFERENCE INFORMATION  
 BETA PHI FINPOS MACH  
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 .0000 .0000 3.0000 1.0000  
 .0000 .0000 3.0000 1.0000  
 .0000 .0000 19.6750 50. IN.  
 LREF 5.0000 IN.  
 BREF 5.0000 IN.  
 XMP 26.5000 IN.  
 YSP 0.0000 IN.  
 ZRP 0.0000 IN.  
 SCALE .0000



EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL  
 CONFIGURATION DESCRIPTION  
 (AEDC) AEDC TF 360 BODY ALONE, .9  
 (AEDC013) AEDC TF 360 BODY FIN, BF 1  
 (AEDC02) AEDC TF 360 BODY FIN, BF 2

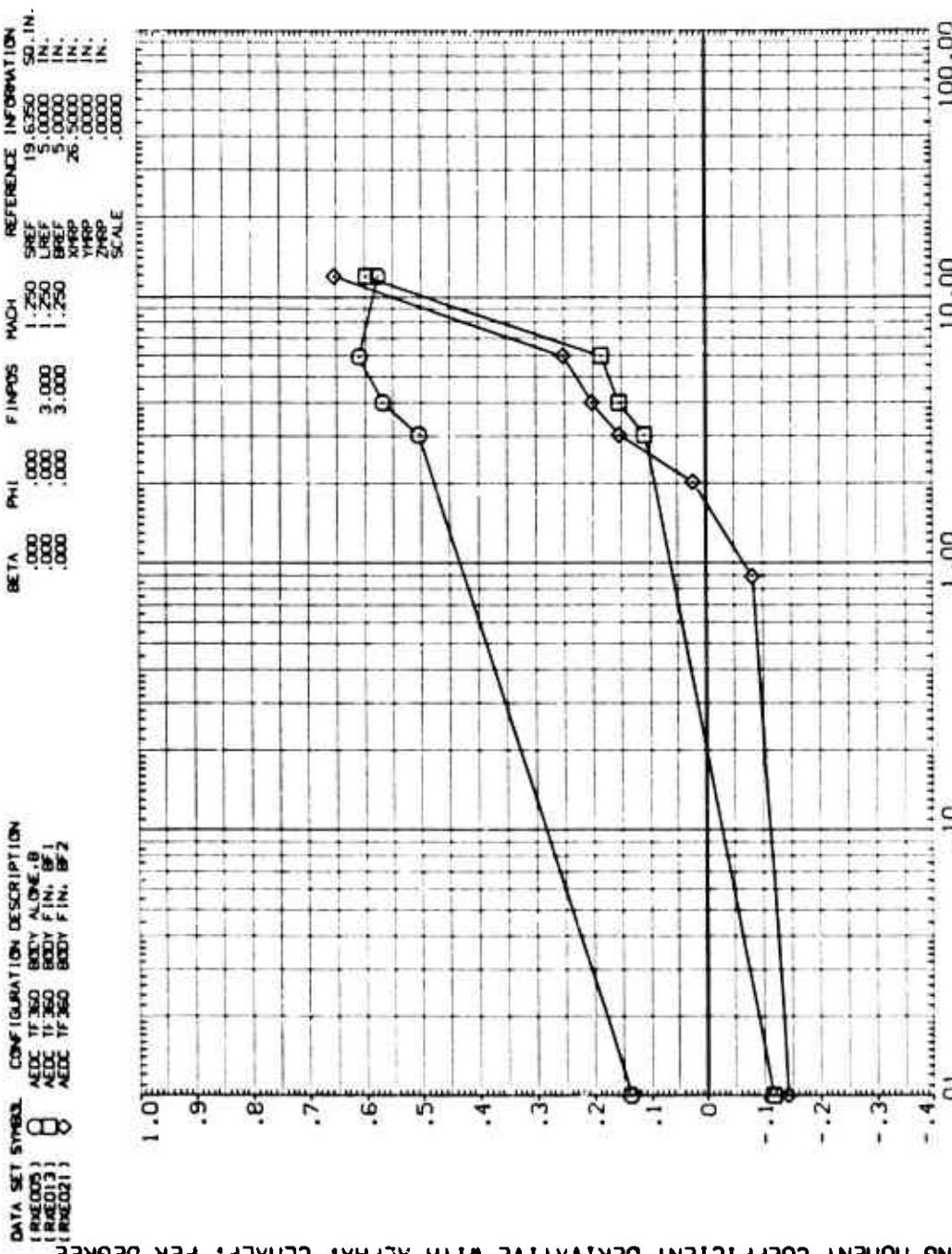
REFERENCE INFORMATION  
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 FINPOS 3.000 3.000 3.000 LREF 5.000 IN.  
 .000 .000 .000 BREF 5.000 IN.  
 .000 .000 .000 XHMP 26.5000 IN.  
 .000 .000 .000 YHMP .0000 IN.  
 .000 .000 .000 ZHMP .0000 IN.  
 .000 .000 .000 SCALE



NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHA, CNALFA, PER DEGREE

### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL      CONFIGURATION DESCRIPTION  
 (RHO013)      AEDC TF 360 BODY ALONE, B  
 (RHO013)      AEDC TF 360 BODY FIN, B<sup>1</sup>  
 (RHO021)      AEDC TF 360 BODY FIN, B<sup>2</sup>



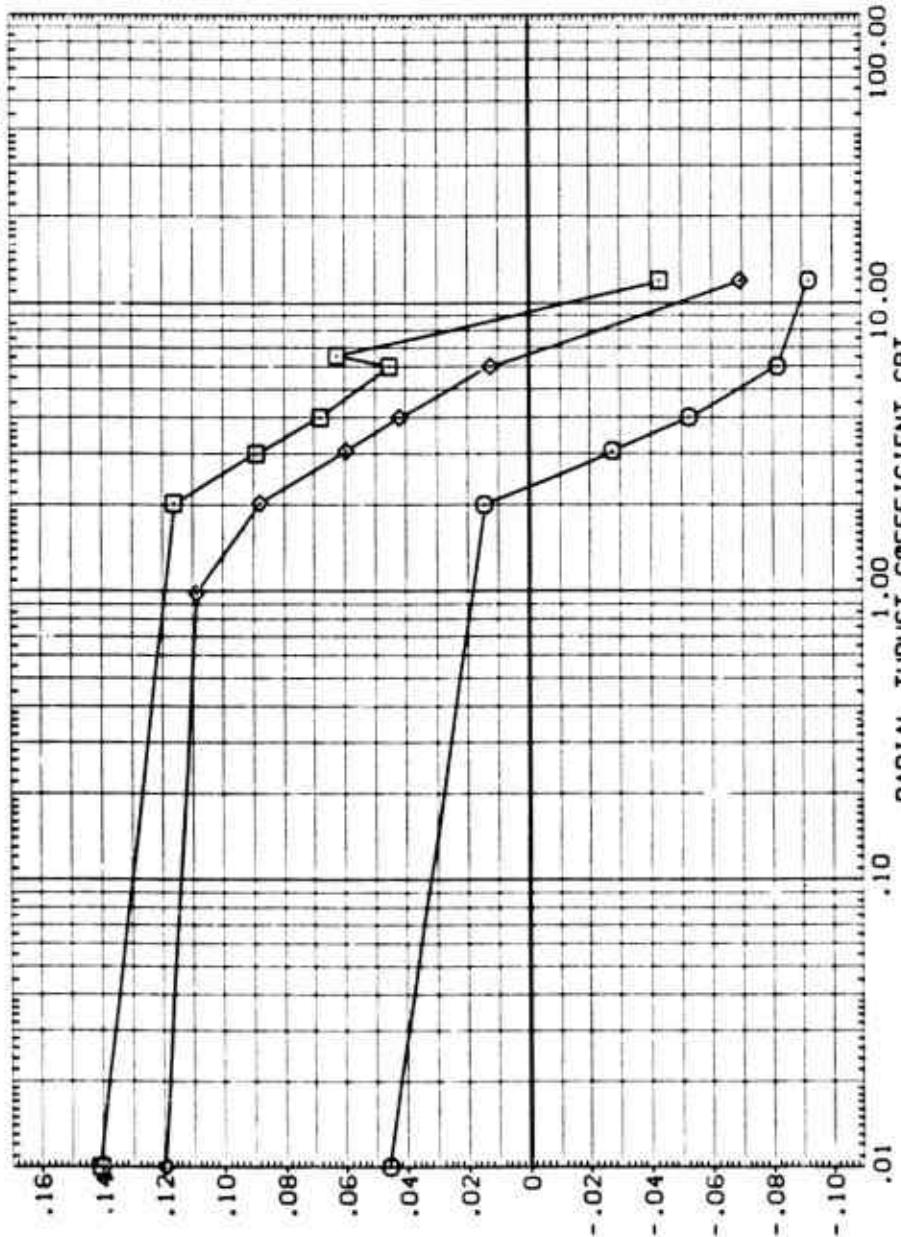
PITCHING MOMENT COEFFICIENT DERIVATIVE WITH ALPHABETIC, CLM(L.F.), PER DEGREE

### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

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DATA SET SYMBOL      CONFIGURATION DESCRIPTION  
 (REF000)      AEDC TF 360 BODY ALONE, B  
 (REF014)      AEDC TF 360 BODY FIN, BF1  
 (REF022)      AEDC TF 360 BODY FIN, BF2

	BETA	PHI	FINPOS	MACH	REFERENCE INFORMATION
(REF000)	.000	.000	3.000	1.500	SREF 19.6350 SQ. IN.
(REF000)	.000	.000	3.000	1.500	LREF .500000 IN.
(REF000)	.000	.000	3.000	1.500	BREF .500000 IN.
(REF000)	.000	.000	3.000	1.500	XHGP .000000 IN.
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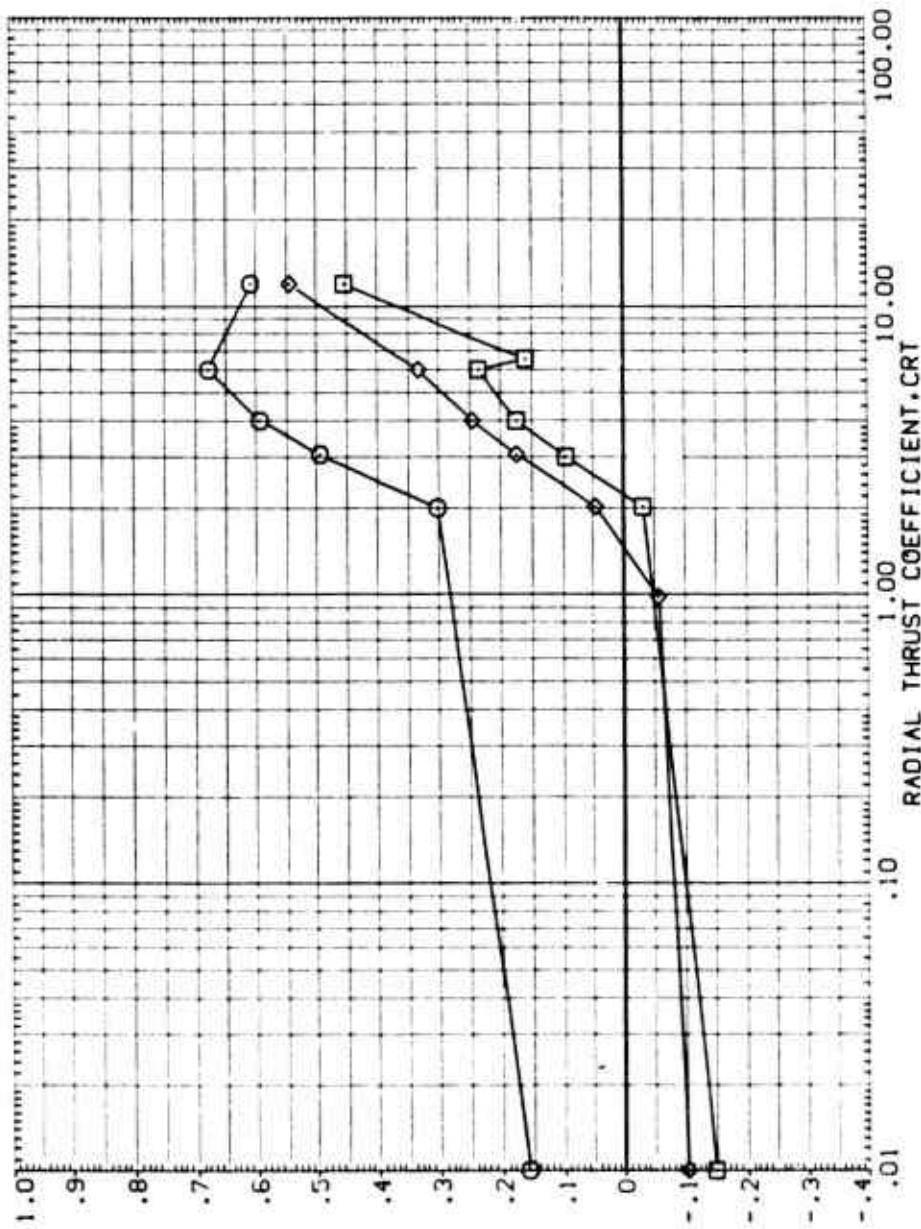


NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHAB, CNLFA, PER DEGREE

### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL: CONFIGURATION DESCRIPTION  
 RAE003 BODY ALONE, B  
 RAE014 BODY FIN, BF1  
 RAE022 BODY FIN, BF2

REFERENCE INFORMATION  
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 FINPOS 3.000  
 PHI .000  
 BETA .000  
 REF 19.6350 IN.  
 BREF 5.0000 IN.  
 XHREF 26.5000 IN.  
 YHREF .0000 IN.  
 ZHREF .0000 IN.  
 SCALE .0000



PITCHING MOMENT COEFFICIENT DERIVATIVE WITH ALPHA, CLMALF, PER DEGREE

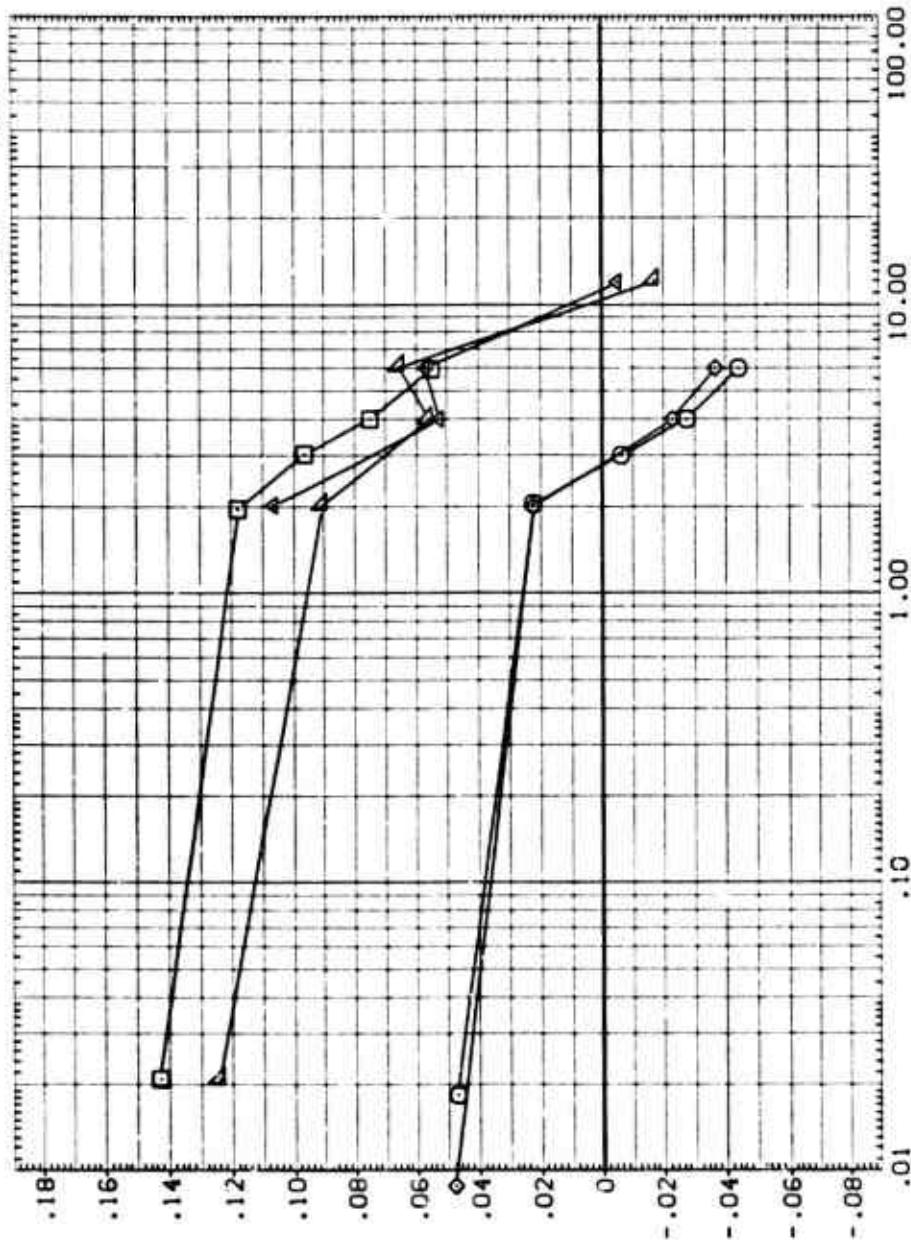
EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOLS CONFIGURATION DESCRIPTION

PROE017	NEDE SF172	BODY ALONE, B
PROE018	NEDE SF172	BODY FIN, Bf
PROE019	NEDE SF172	BODY ALONE, Bf
PROE016	NEDE SF172	BODY FIN, Bf
PROE017	NEDE SF172	BODY FIN, Bf

REFERENCE INFORMATION

BETA	.000	FINPOS	1.700	MACH	19.6350	SD. IN.
PHI	.000		1.700	LREF	5.0000	IN.
	.000		2.000	BREF	5.0000	IN.
	.000		2.000	HRP	26.5000	IN.
	.000		2.000	ZRP	.0000	IN.
	.000		2.000	SCALE	.0000	IN.



NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHABETIC CNLFA, PER DEGREE

### EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

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CME / CREDIT / DESCRIPTION

DATA SET NAME	CONFIGURATION DESCRIPTION
R001007	ADIC SF BODY ALONE-B
R001015	ADIC SF BODY FIN. B/F
R001009	ADIC SF BODY ALONE-B
R001016	ADIC SF BODY FIN. B/F
R001017	ADIC SF BODY FIN. B/F

BETA PHI FRATERNAL REFERENCE INFORMATION

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INFORMATION

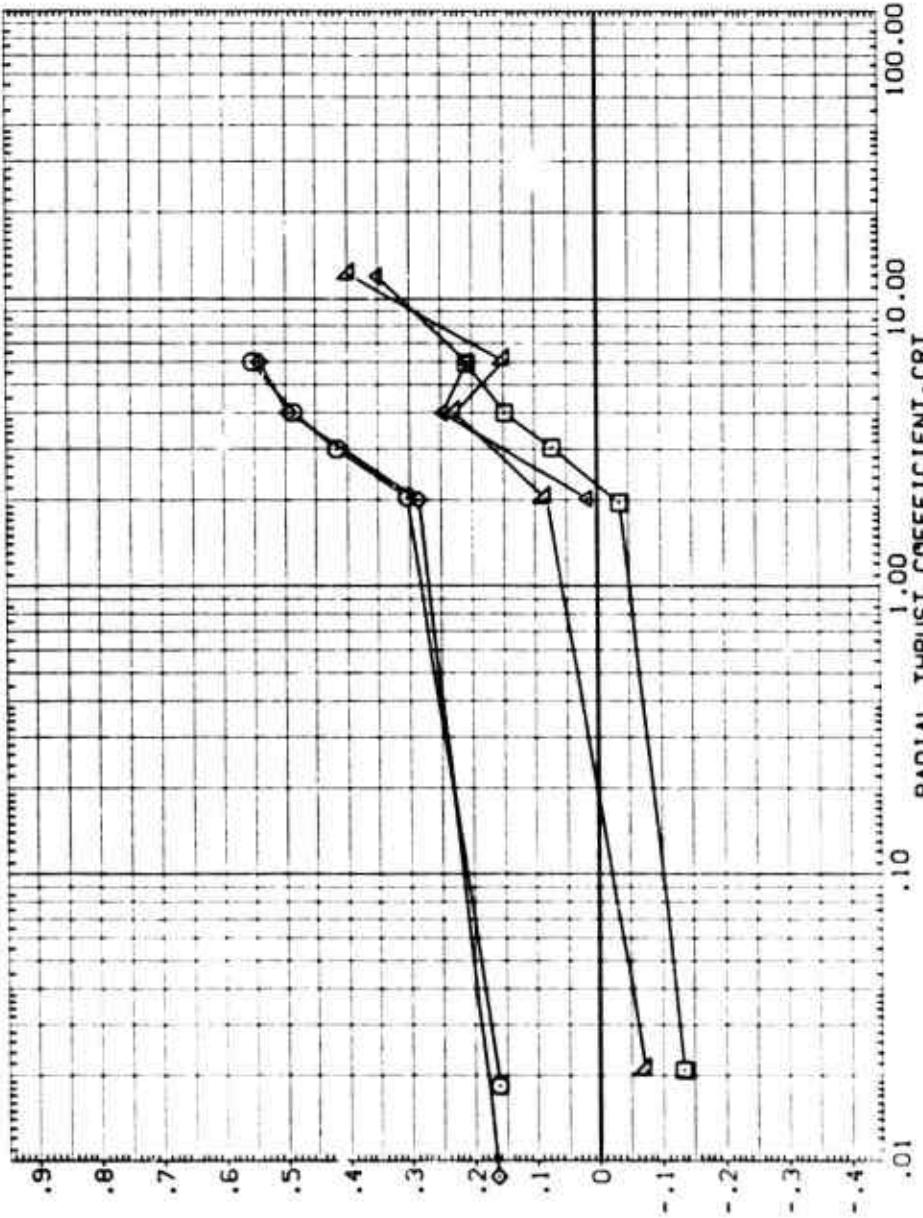
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PITCHING MOMENT COEFFICIENT DERIVATIVE WITH ALPHABETIC CHARGE. PER DEGREE

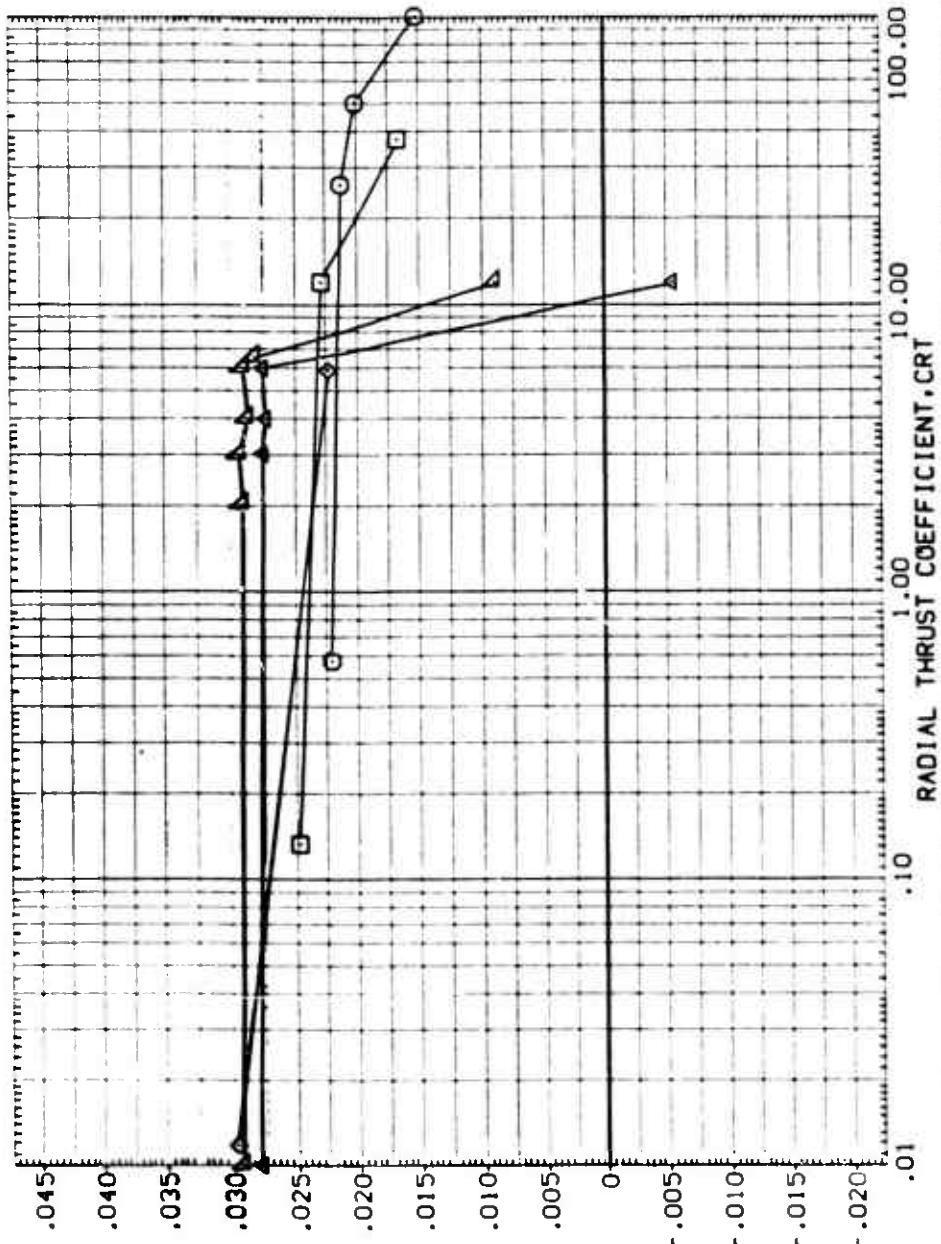
EFFECT OF RADIAL THRUST COEFFICIENT ON LONGITUDINAL DERIVATIVES

DATA SET SYMBOL      CONFIGURATION DESCRIPTION

RDE109	AEDC	TF 360	BODY FIN.	35
RDE110	AEDC	TF 360	BODY FIN.	35
RDE111	AEDC	TF 360	BODY FIN.	35
RDE112	AEDC	TF 360	BODY FIN.	35
RDE113	AEDC	TF 360	BODY FIN.	35
RDE114	AEDC	TF 360	BODY FIN.	35

DATA SET SYMBOL      CONFIGURATION DESCRIPTION

FIN2ALFA	AEDC	TF 360	BODY FIN.	35
FIN2ALFB	AEDC	TF 360	BODY FIN.	35
FIN2ALFC	AEDC	TF 360	BODY FIN.	35
FIN2ALFD	AEDC	TF 360	BODY FIN.	35
FIN2ALFE	AEDC	TF 360	BODY FIN.	35



FIN NO. 2 NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHAS. CNF2ALFA

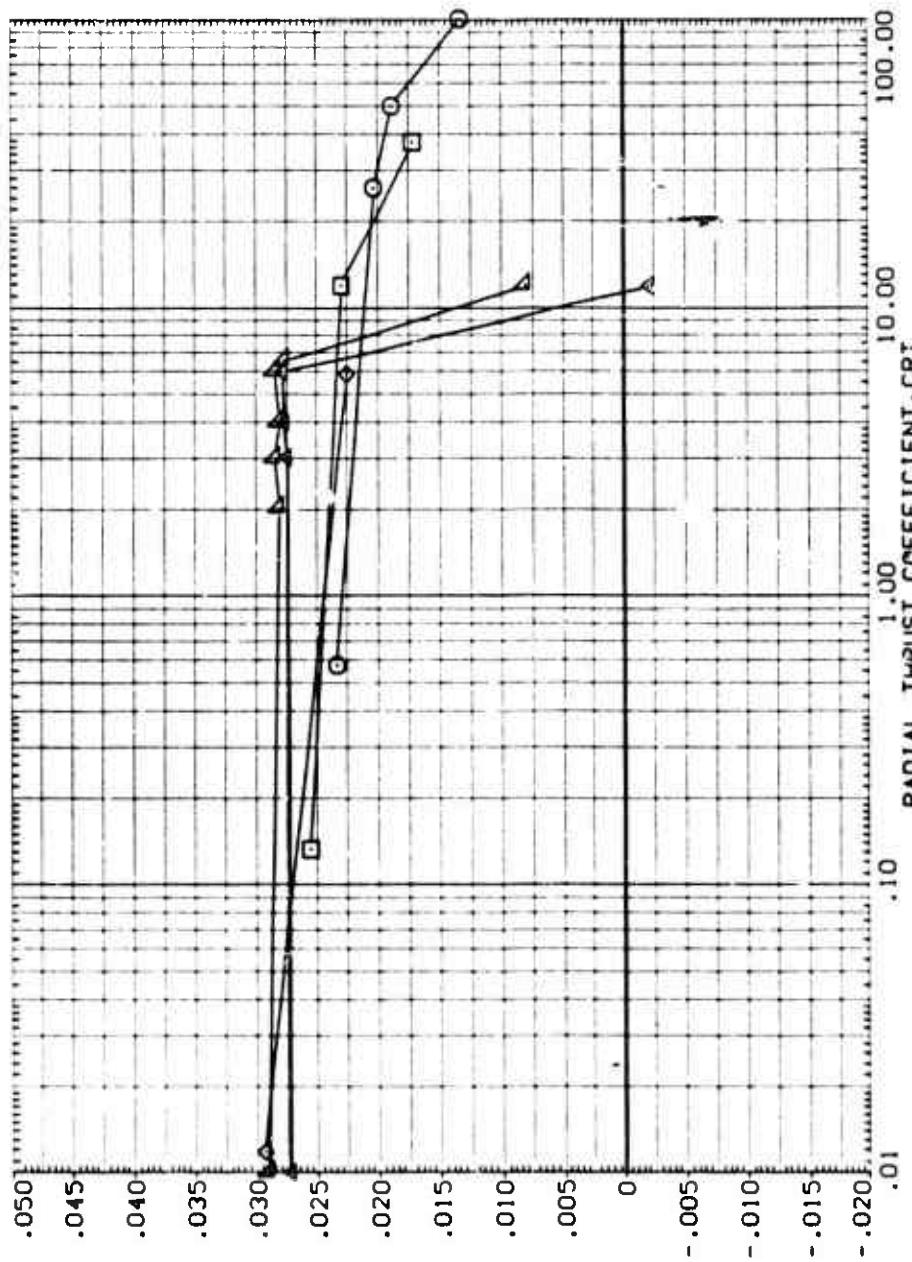
THRUST EFFECTS ON FIN NO. 2 NORMAL FORCE CHARACTERISTICS-FIN IN FORWARD POSITION

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DATA SET SYMBOL CONFIGURATION DESCRIPTION

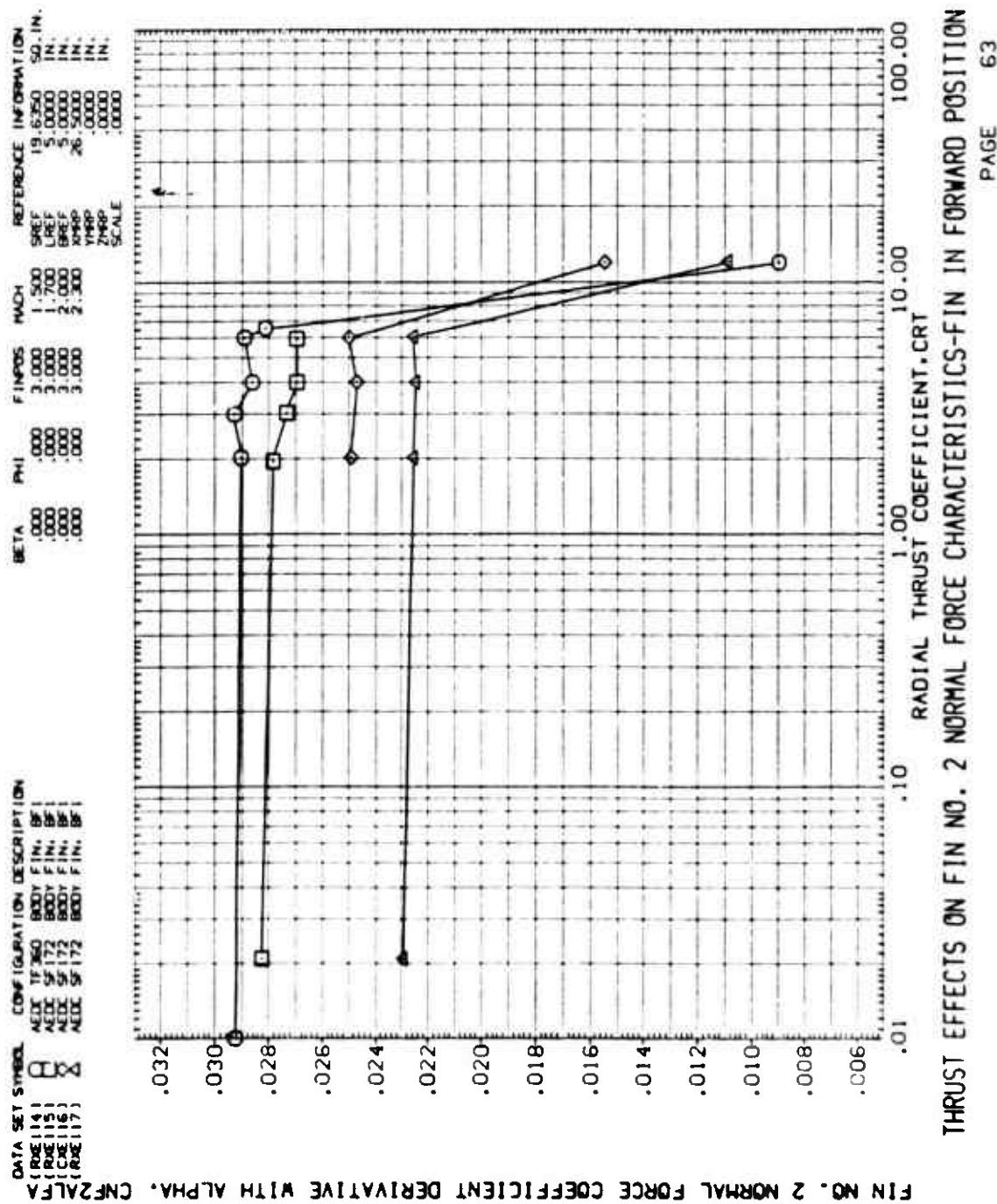
1	AEDC	TF360	BODY FIN, BF
2	AEDC	TF360	BODY FIN, SF
3	AEDC	TF360	BODY FIN, SF
4	AEDC	TF360	BODY FIN, SF
5	AEDC	TF360	BODY FIN, SF
6	AEDC	TF360	BODY FIN, SF
7	AEDC	TF360	BODY FIN, SF
8	AEDC	TF360	BODY FIN, SF

REFERENCE INFORMATION  
 MACH .200  
 FINPOS 3.000  
 PHI .000  
 BETA .000  
 REF 19.8350 IN.  
 DREF 5.0000 IN.  
 SREF 5.0000 IN.  
 XREF 26.5000 IN.  
 YREF 0.0000 IN.  
 ZREF 0.0000 IN.  
 SCALE .0000



FIN NO. 4 NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHAS. CNF4A1.FIN

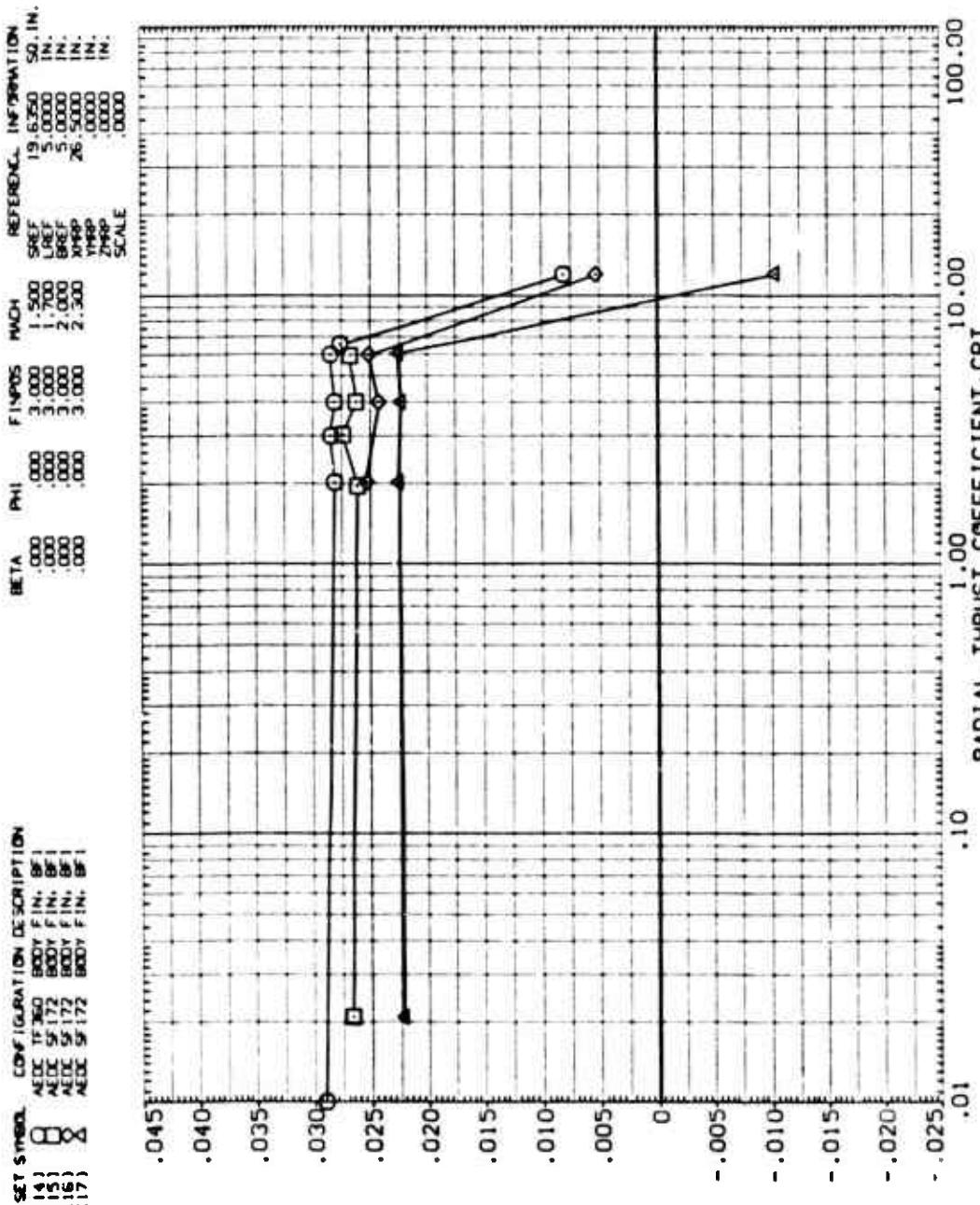
THRUST EFFECTS ON FIN NO. 4 NORMAL FORCE CHARACTERISTICS-FIN IN FORWARD POSITION



THRUST EFFECTS ON FIN NO. 2 NORMAL FORCE CHARACTERISTICS-FIN IN FORWARD POSITION  
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THRUST EFFECTS ON FIN NO. 4 NORMAL FORCE CHARACTERISTICS-FIN IN FORWARD POSITION

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FIN NO. 4 NORMAL FORCE COEFFICIENT DERIVATIVE WITH ALPHA, CNF4ALFA

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